

AFWL-TR-78-158, Pt. 3

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AFWL-TR-
78-158
Pt. 3

Aug 31 1979
AC 71 522

DA071523

SIMULATION DEVELOPMENT FOR TARGET ASSESSMENT

Part 3 of 3

J. A. Earickson

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Albuquerque, NM 87131

March 1979

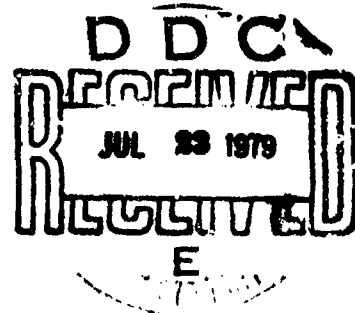
Final Report

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AIR FORCE WEAPONS LABORATORY
Air Force Systems Command
Kirtland Air Force Base, NM 87117




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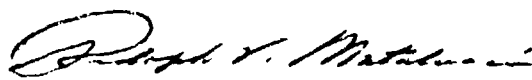
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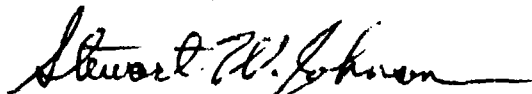
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Division

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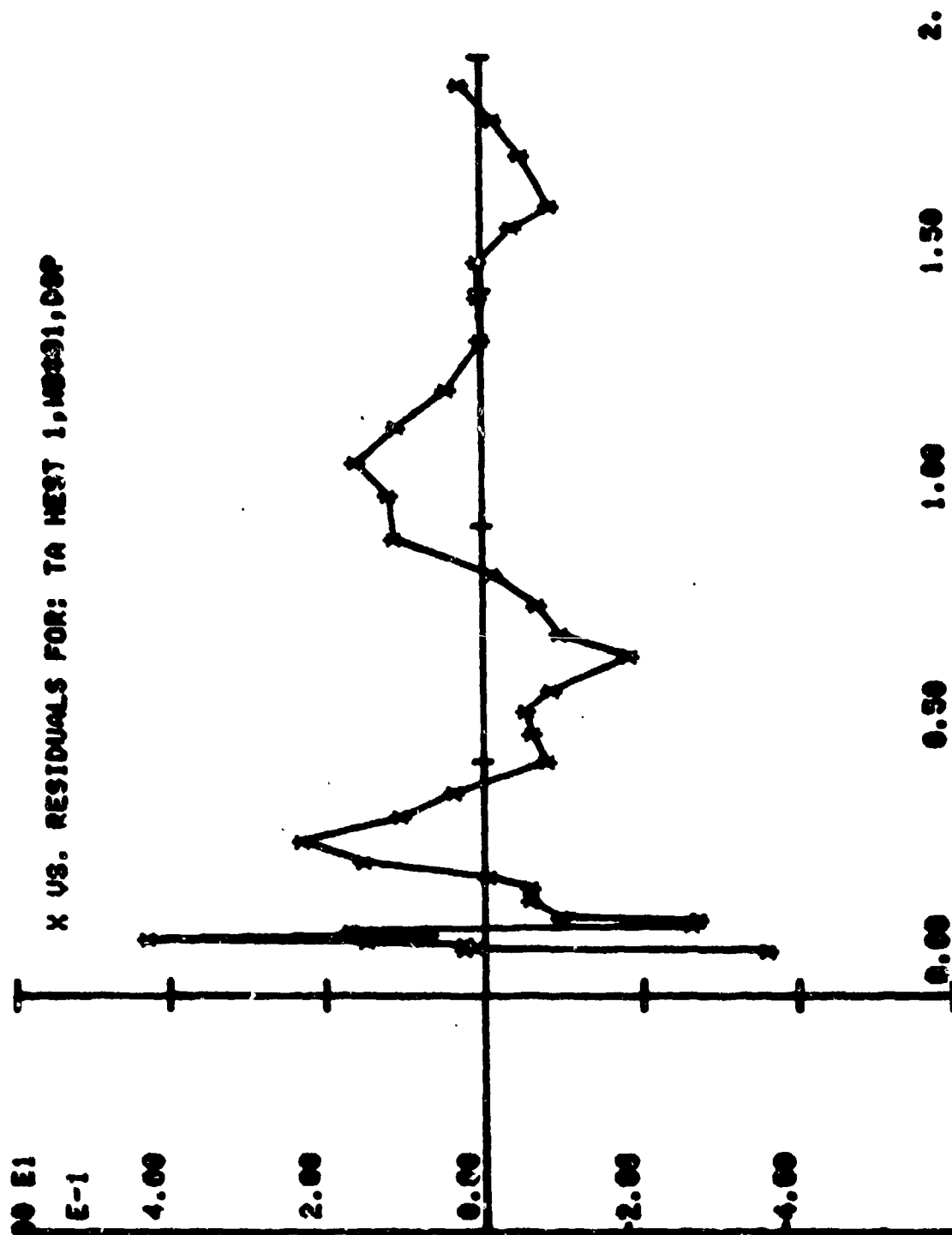
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4. TITLE (and Subtitle) SIMULATION DEVELOPMENT FOR TARGET ASSESSMENT		5. TYPE OF REPORT & PERIOD COVERED Final Report
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) J. A. Earickson		8. CONTRACT OR GRANT NUMBER(s) F29601-76-C-0015
9. PERFORMING ORGANIZATION NAME AND ADDRESS Eric H. Wang Civil Engineering Research Facility University of New Mexico Albuquerque, NM 87117		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 62601F 88091323
11. CONTROLLING OFFICE NAME AND ADDRESS Air Force Weapons Laboratory (DED) Kirtland Air Force Base, NM 87117		12. REPORT DATE March 1979
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		13. NUMBER OF PAGES 166
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES This report consists of 3 parts. Part 1 contains the front matter and pages 1 to 178. Part 2 contains pages 179 to 364- Part 3 contains pages 365 to 530.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Simulator HEST (High Explosive Simulation Technique) Target Assessment Air Shock		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This effort produced design information and experiment data for improving high explosive simulation of nuclear airblasts. Specifically, a peak pressure versus charge density relationship for Iremits in 100 percent foam cavities was obtained for pressure up to 68 MPa. The results of this effort were transmitted to USAE Waterways Experiment Station. WES is conducting tests on generic silos as part of a DNA targeting research and test program.		

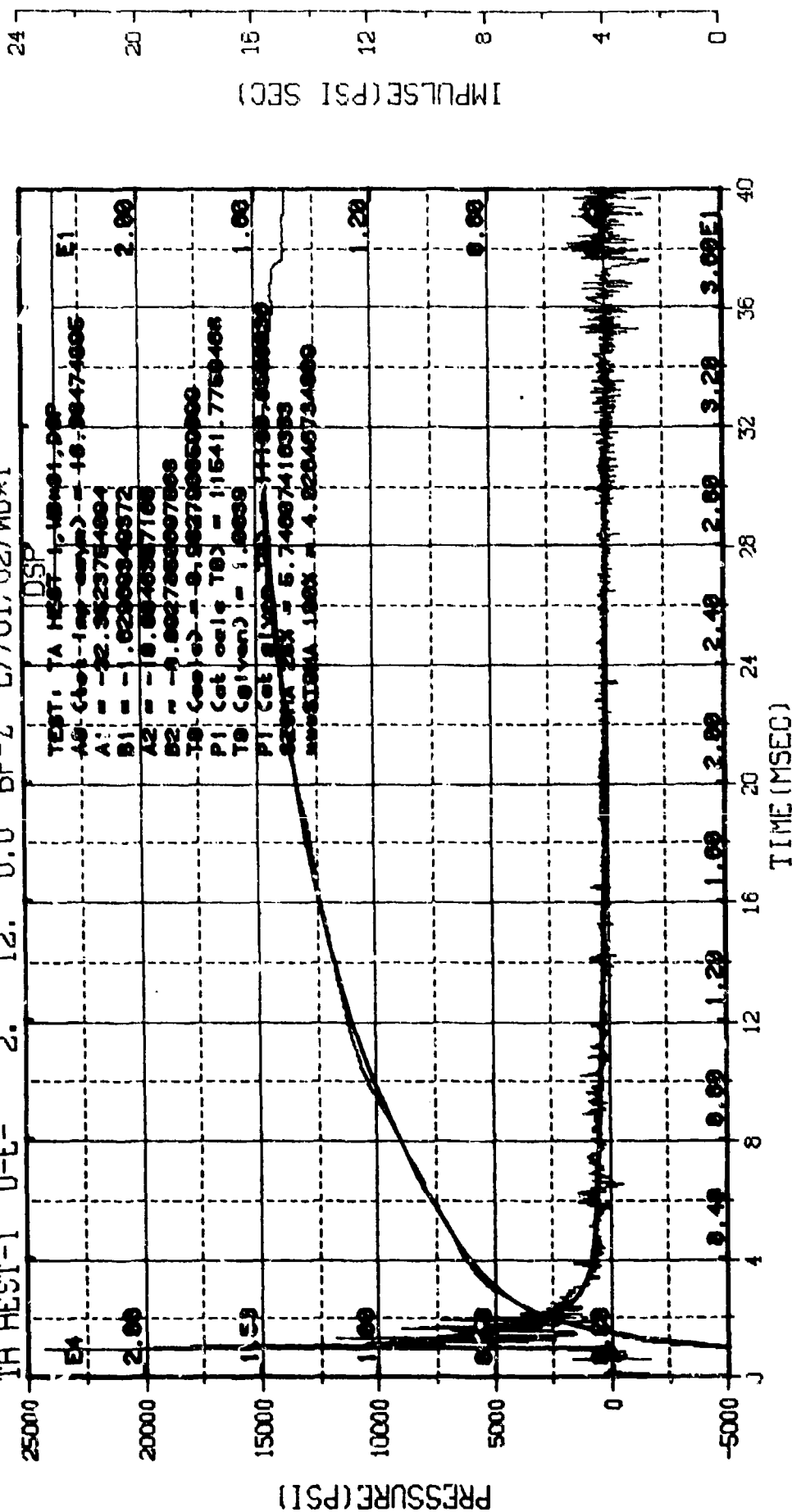
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APPENDIX B
DOUBLE-EXPONENTIAL PEAK PRESSURE OVERLAY PLOTS AND
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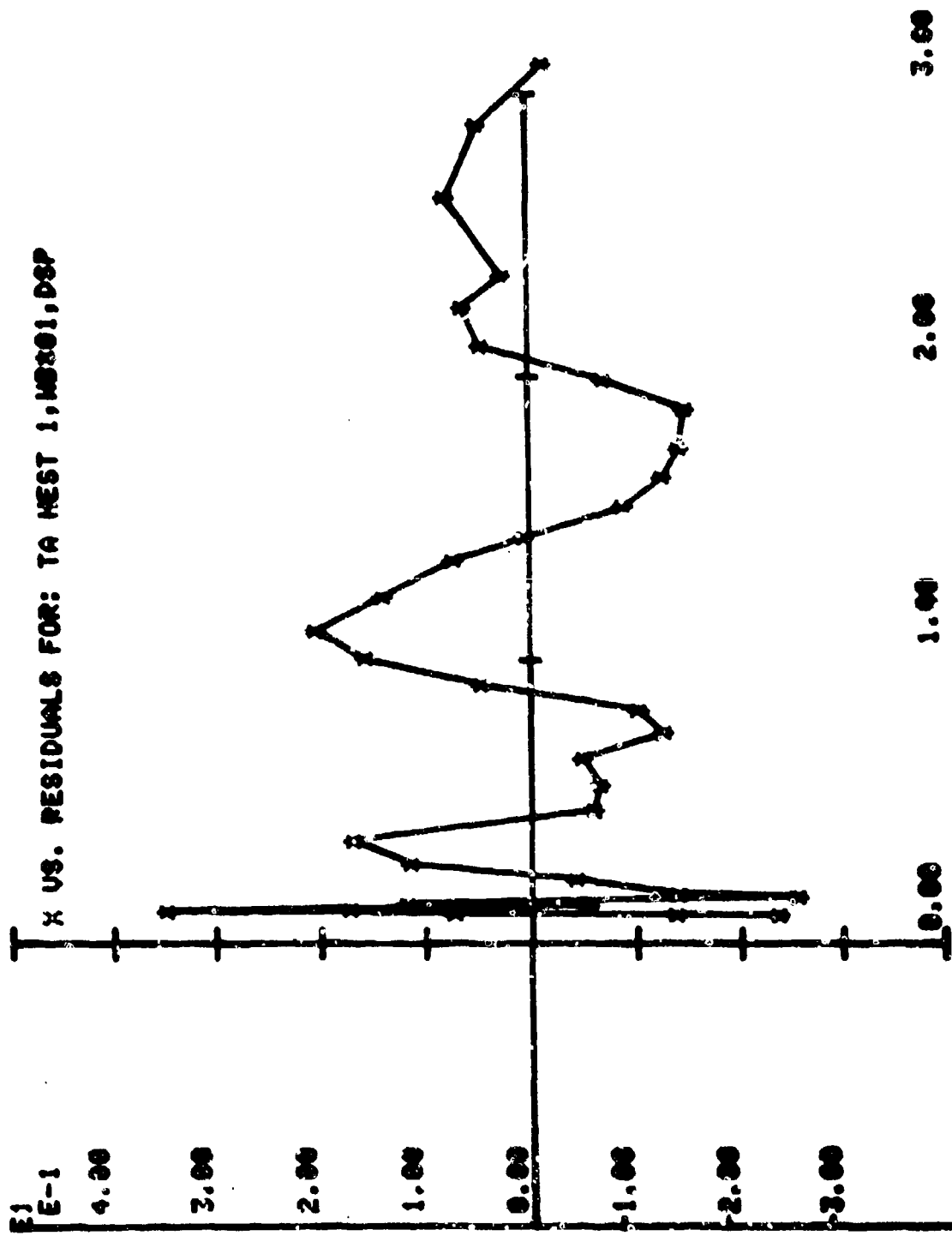
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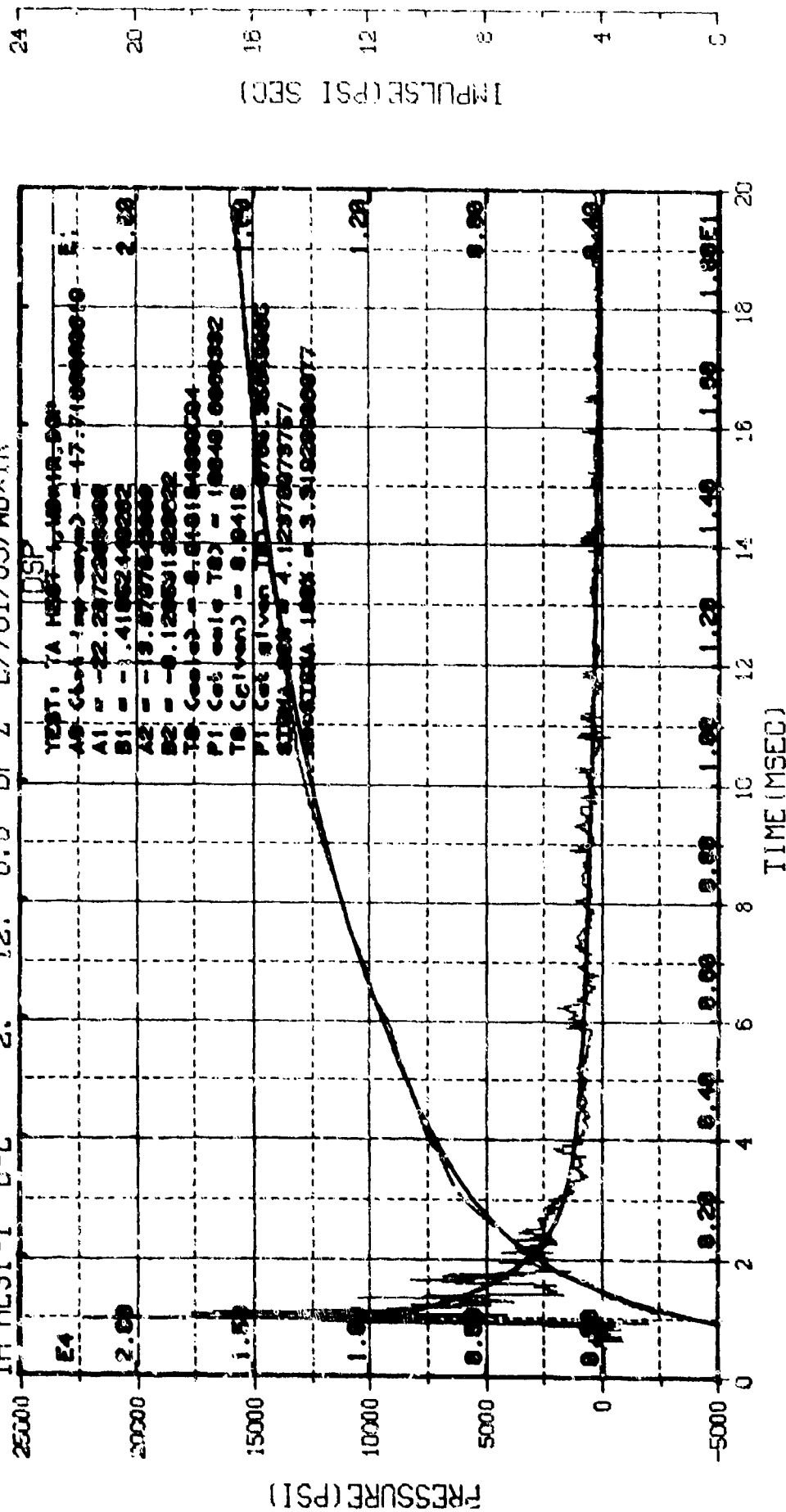
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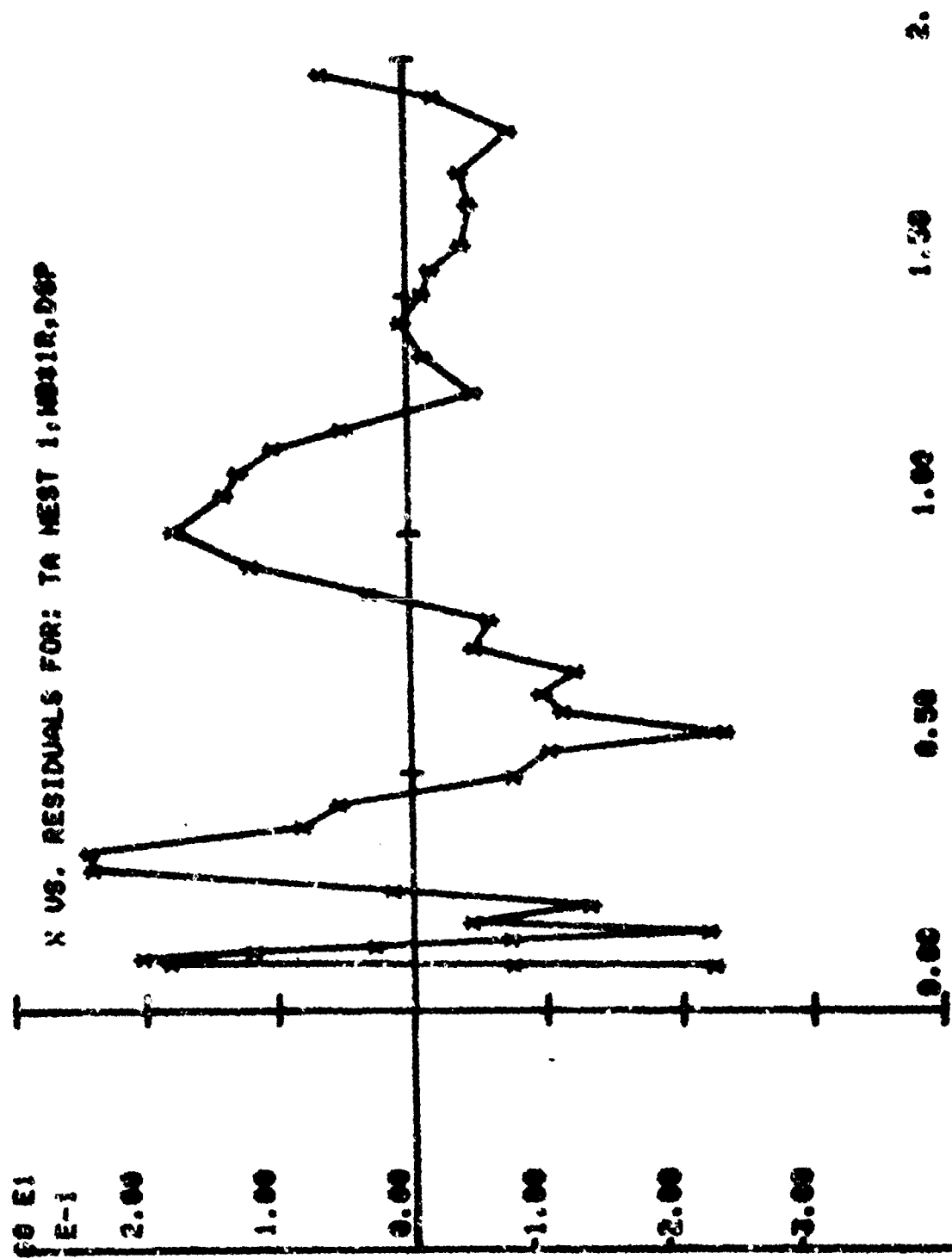


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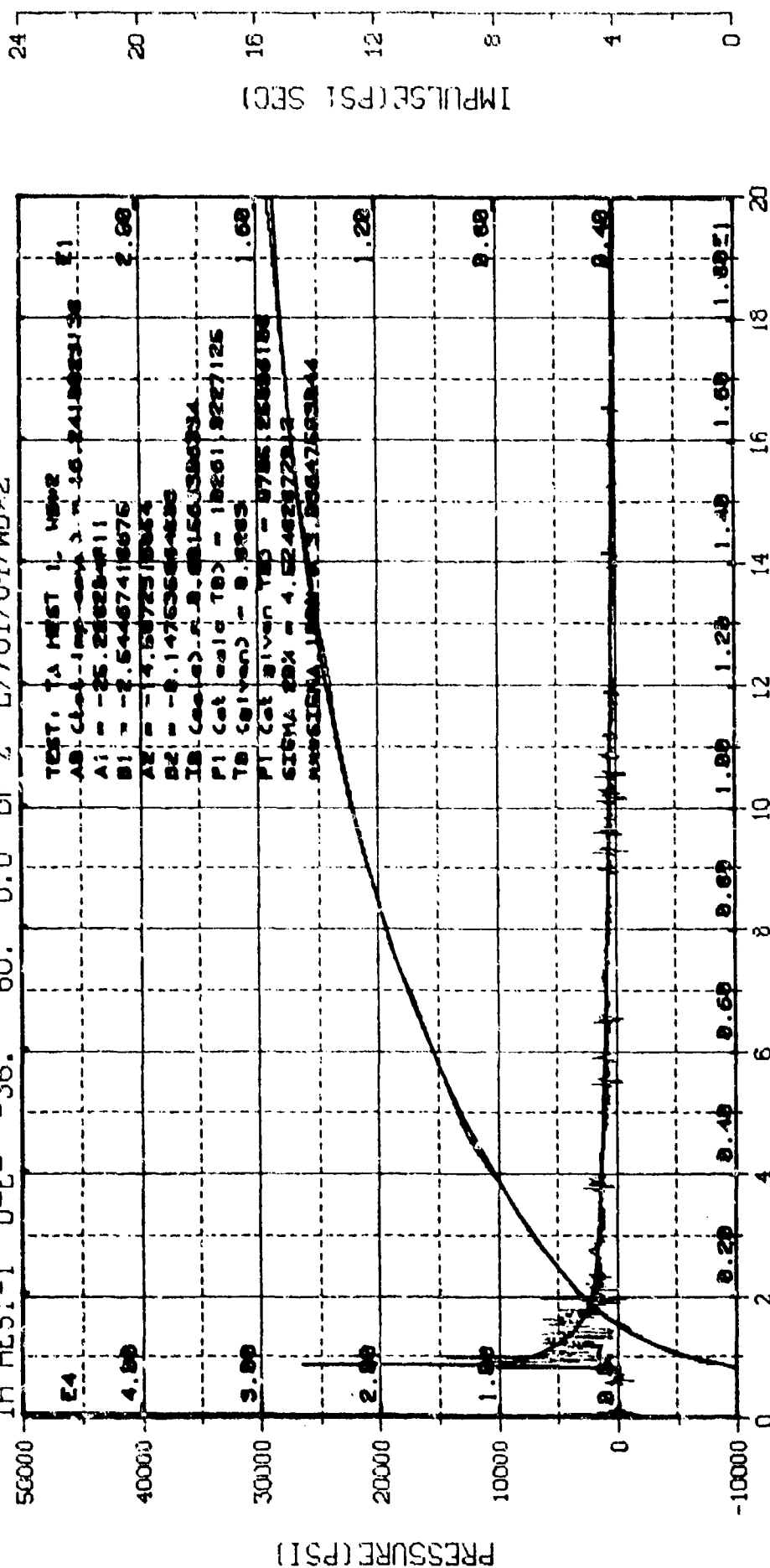




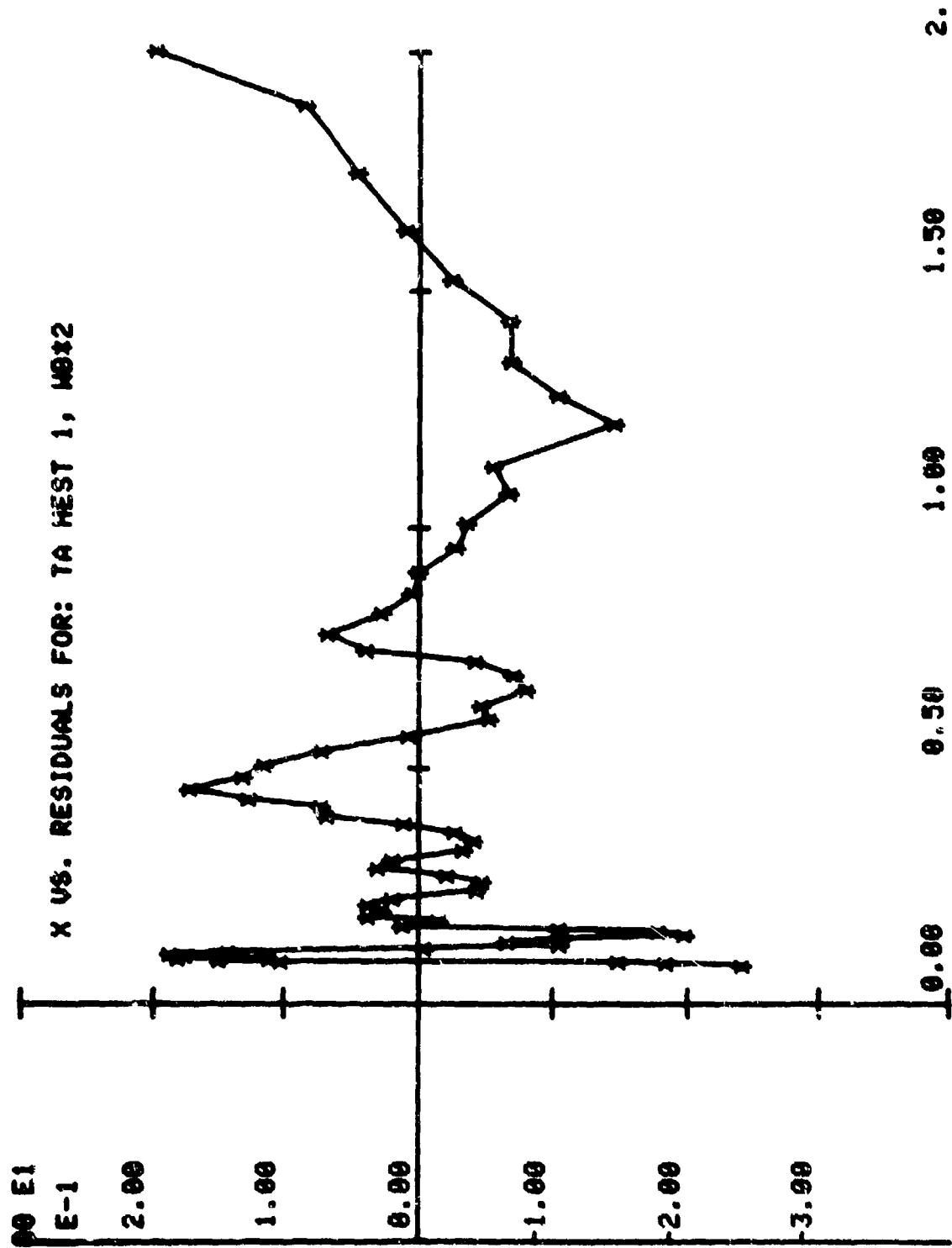
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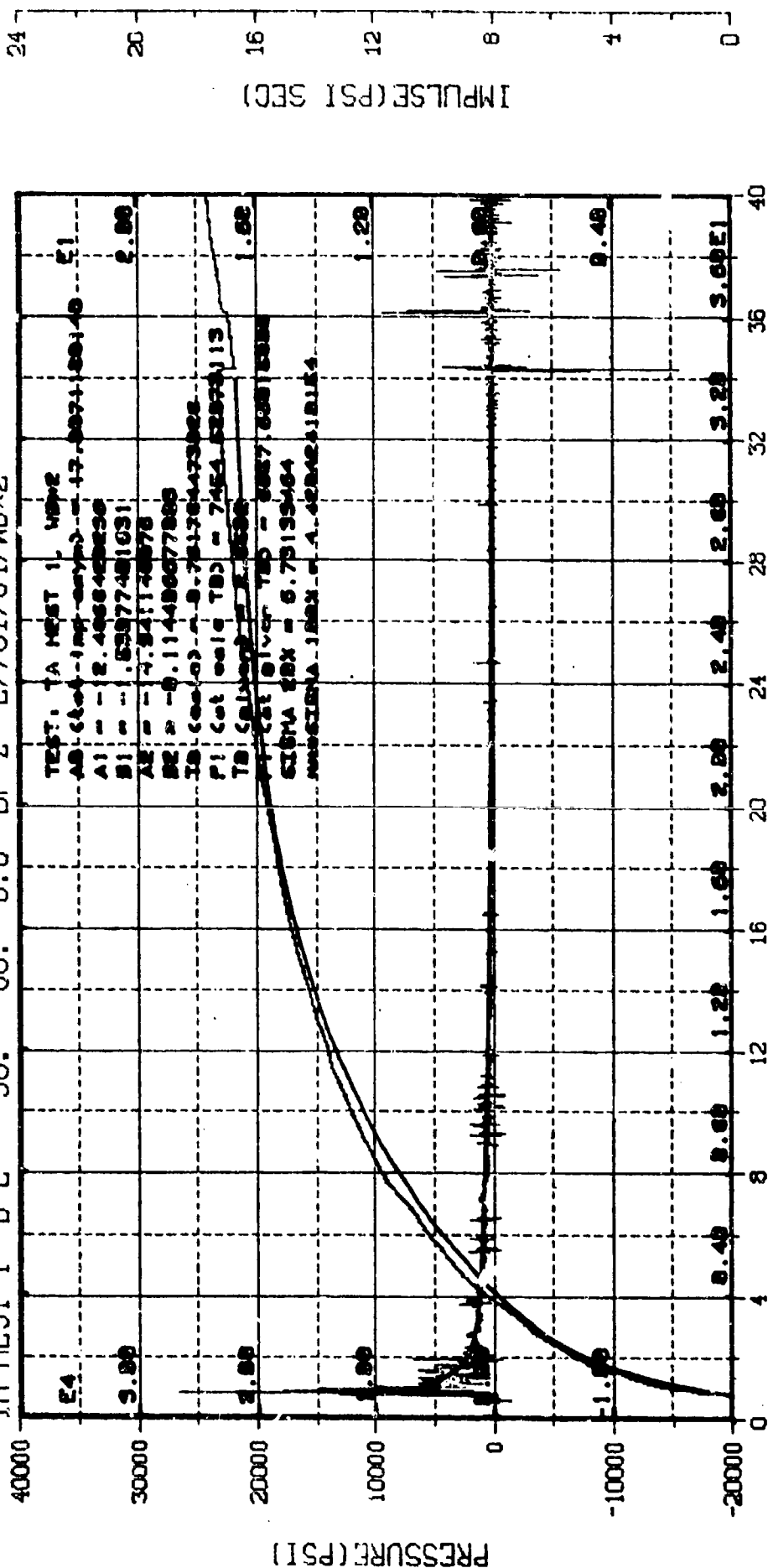
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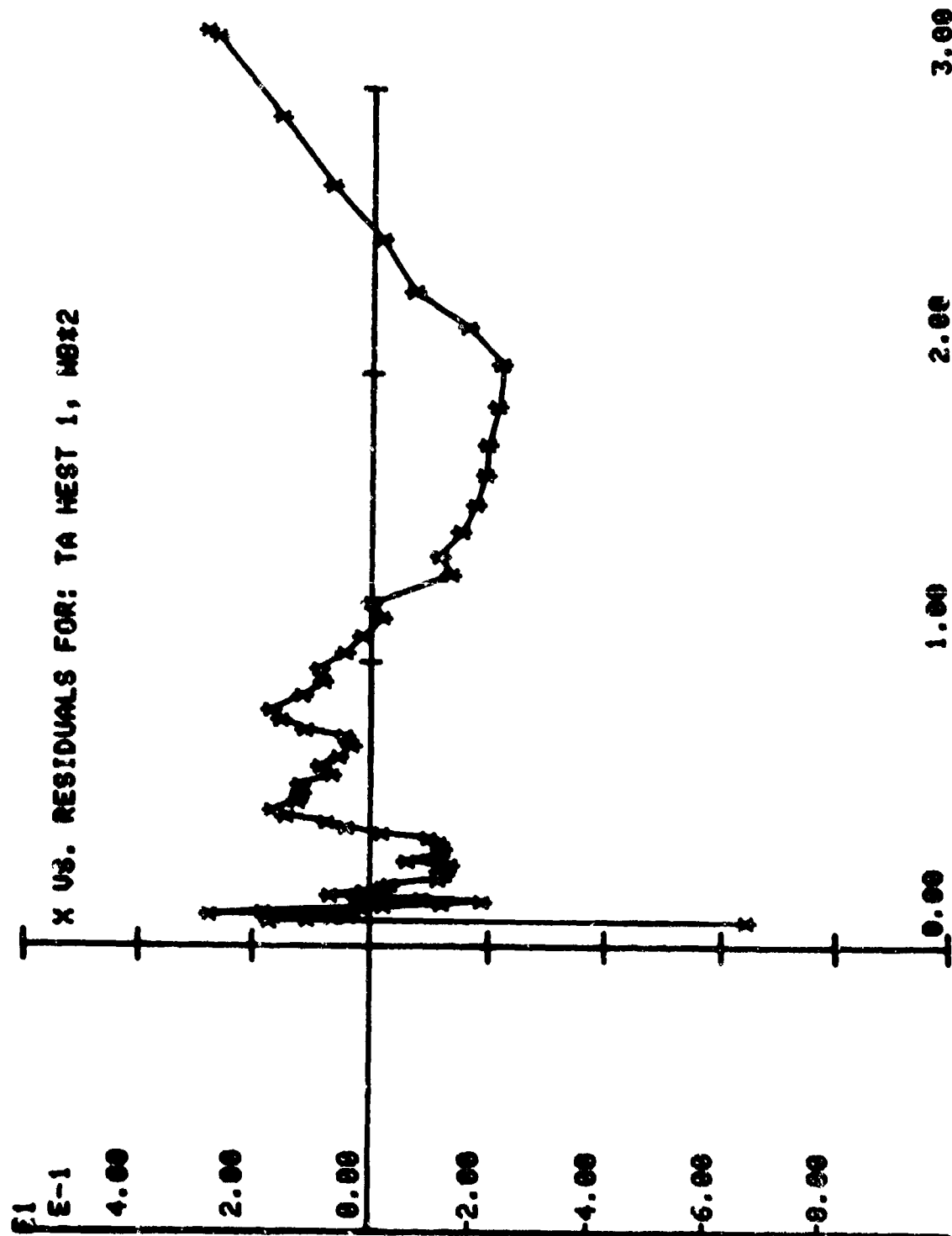
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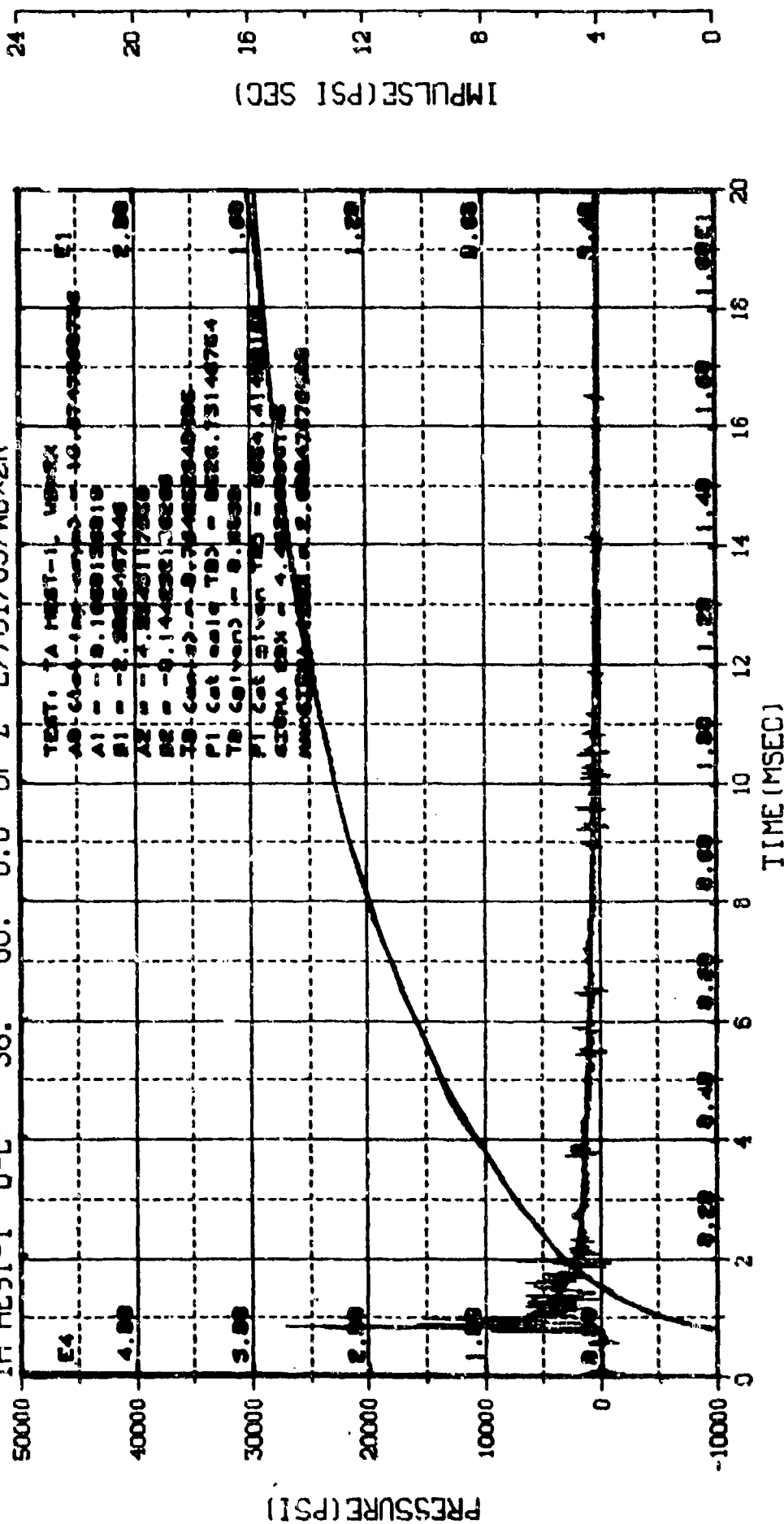
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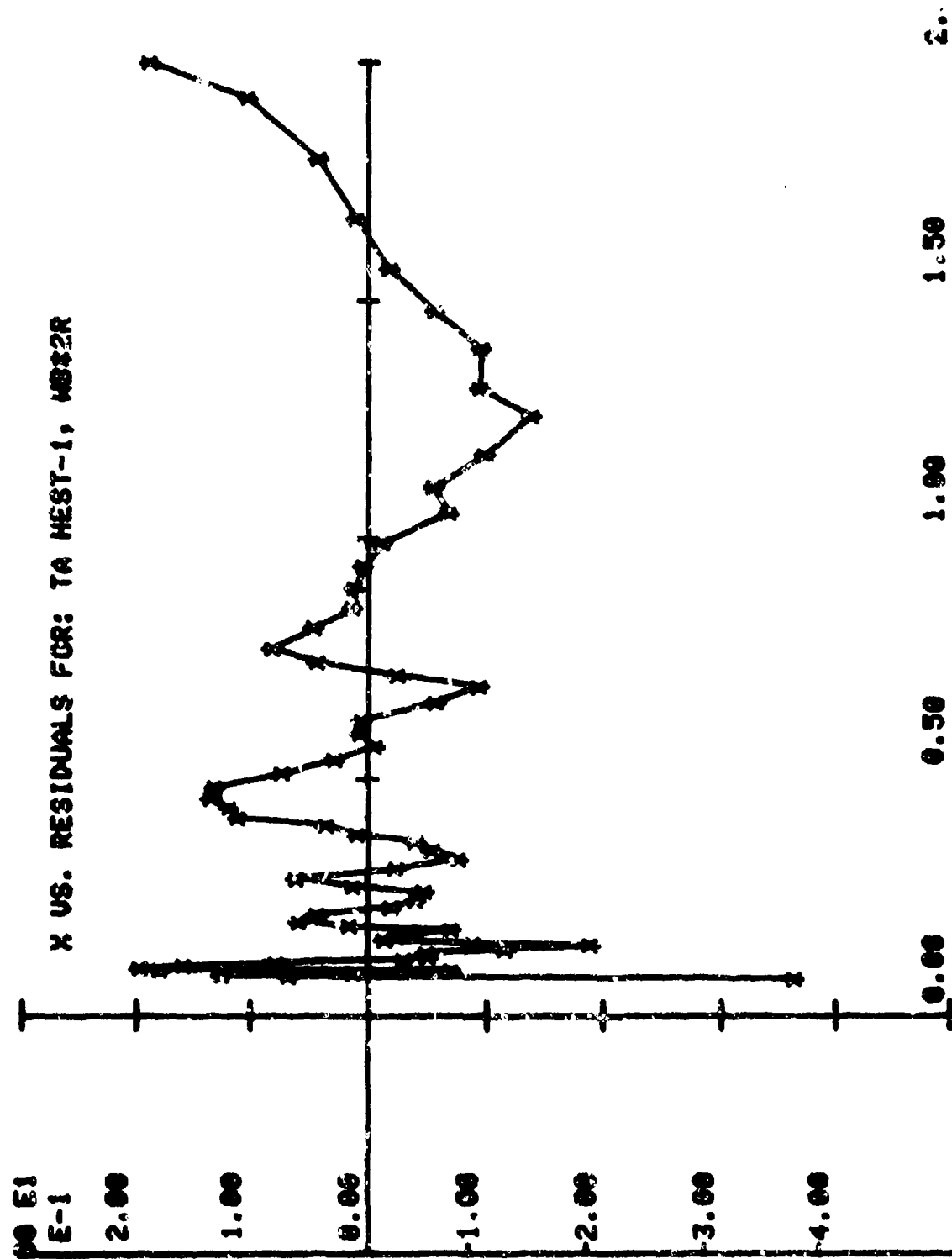
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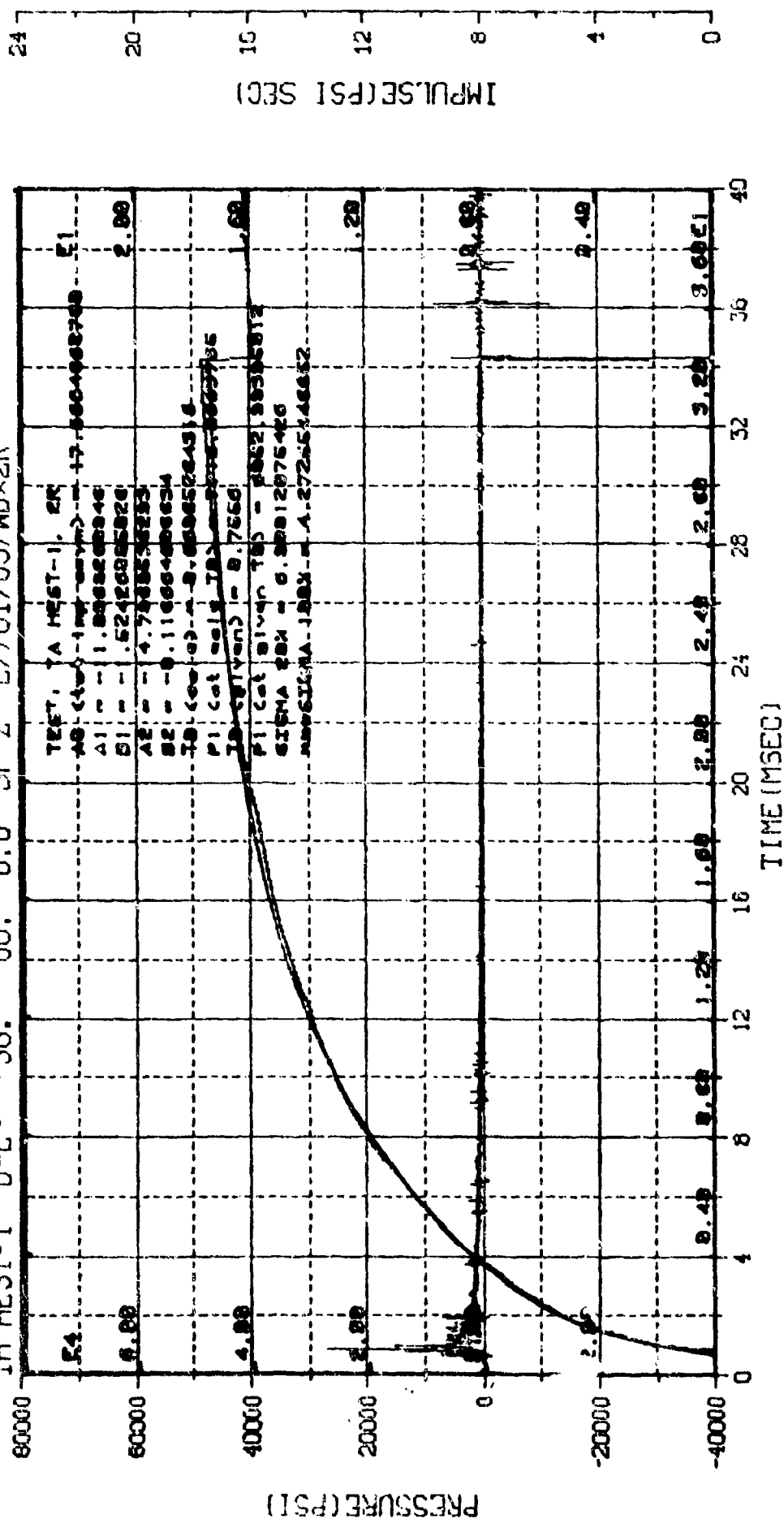
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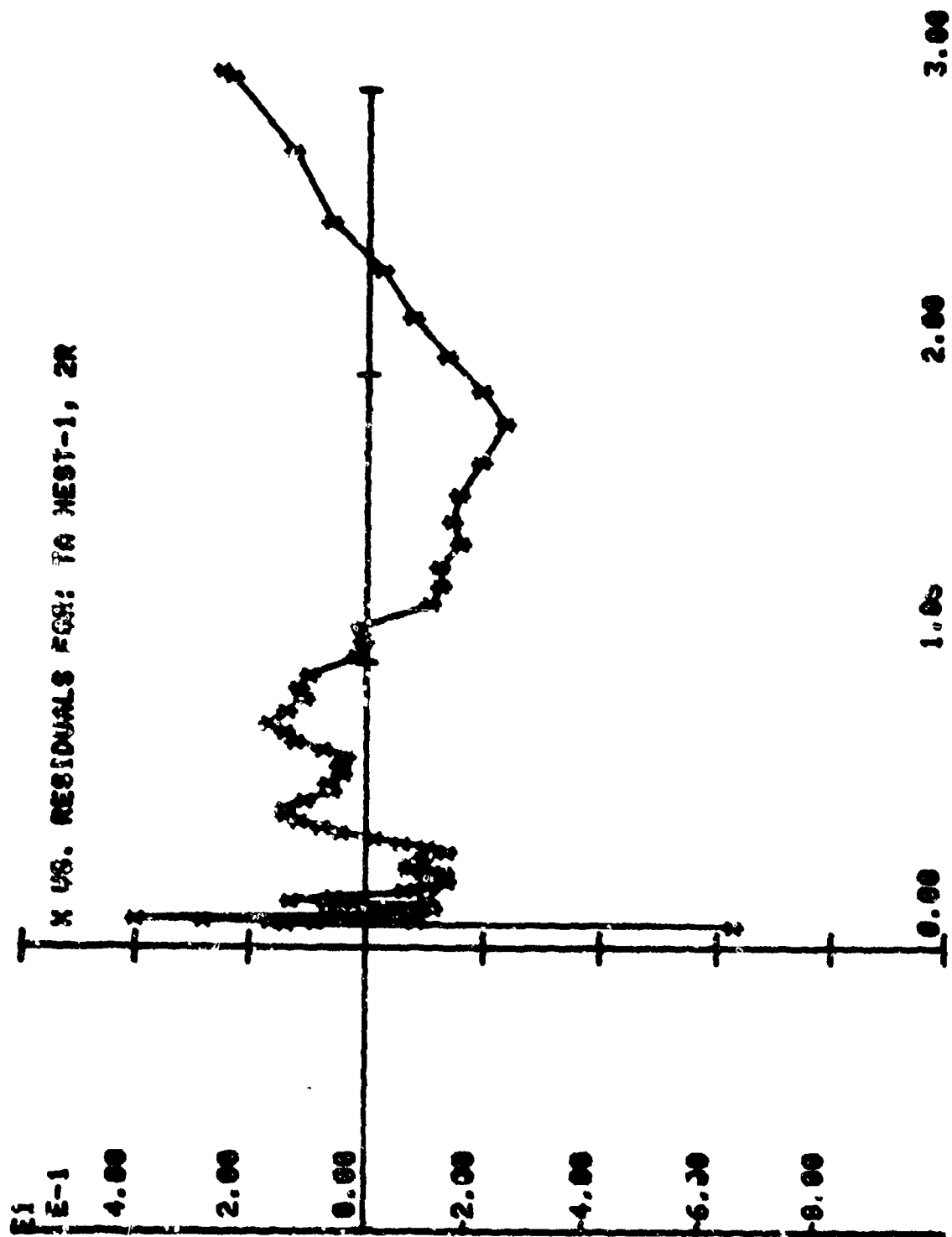
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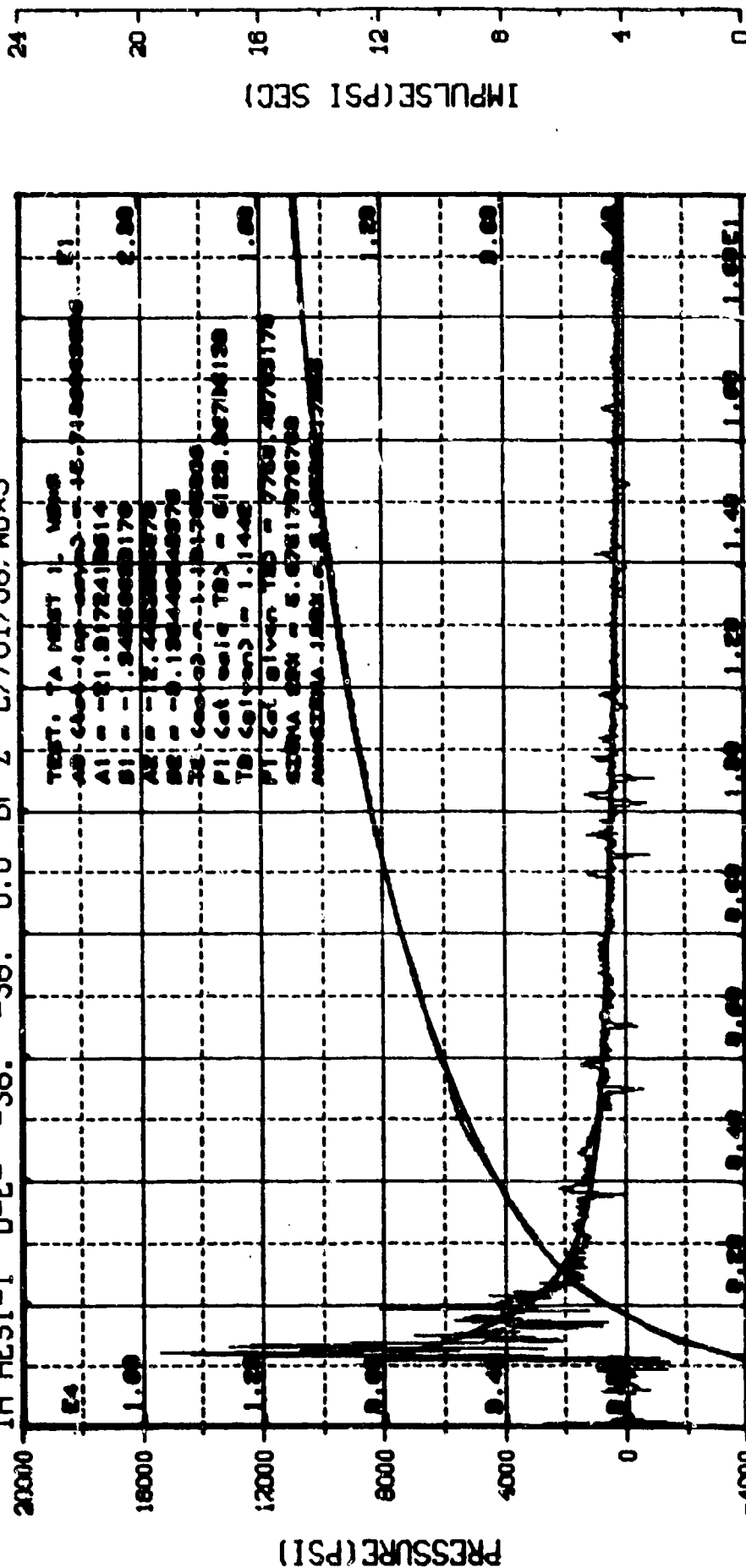


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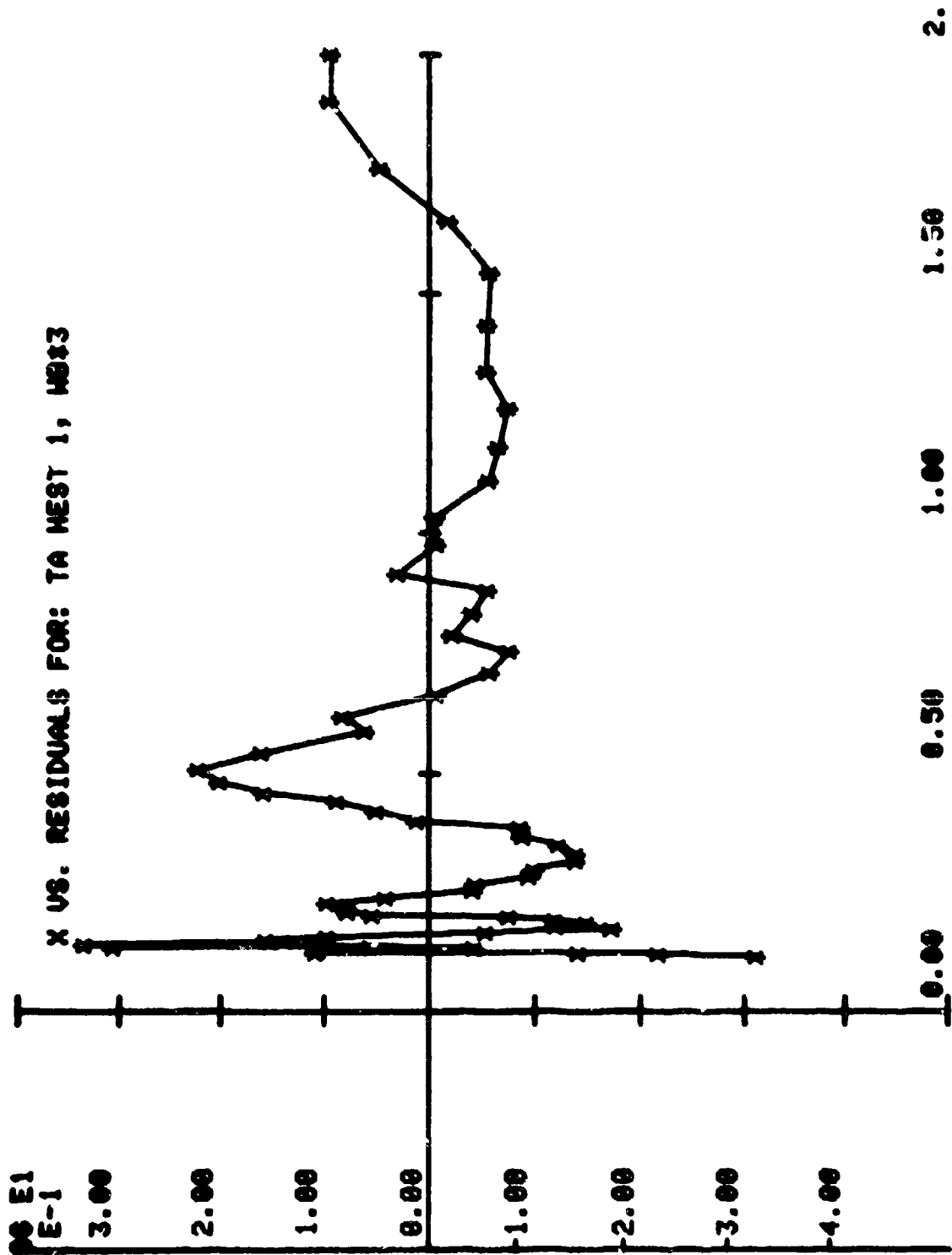


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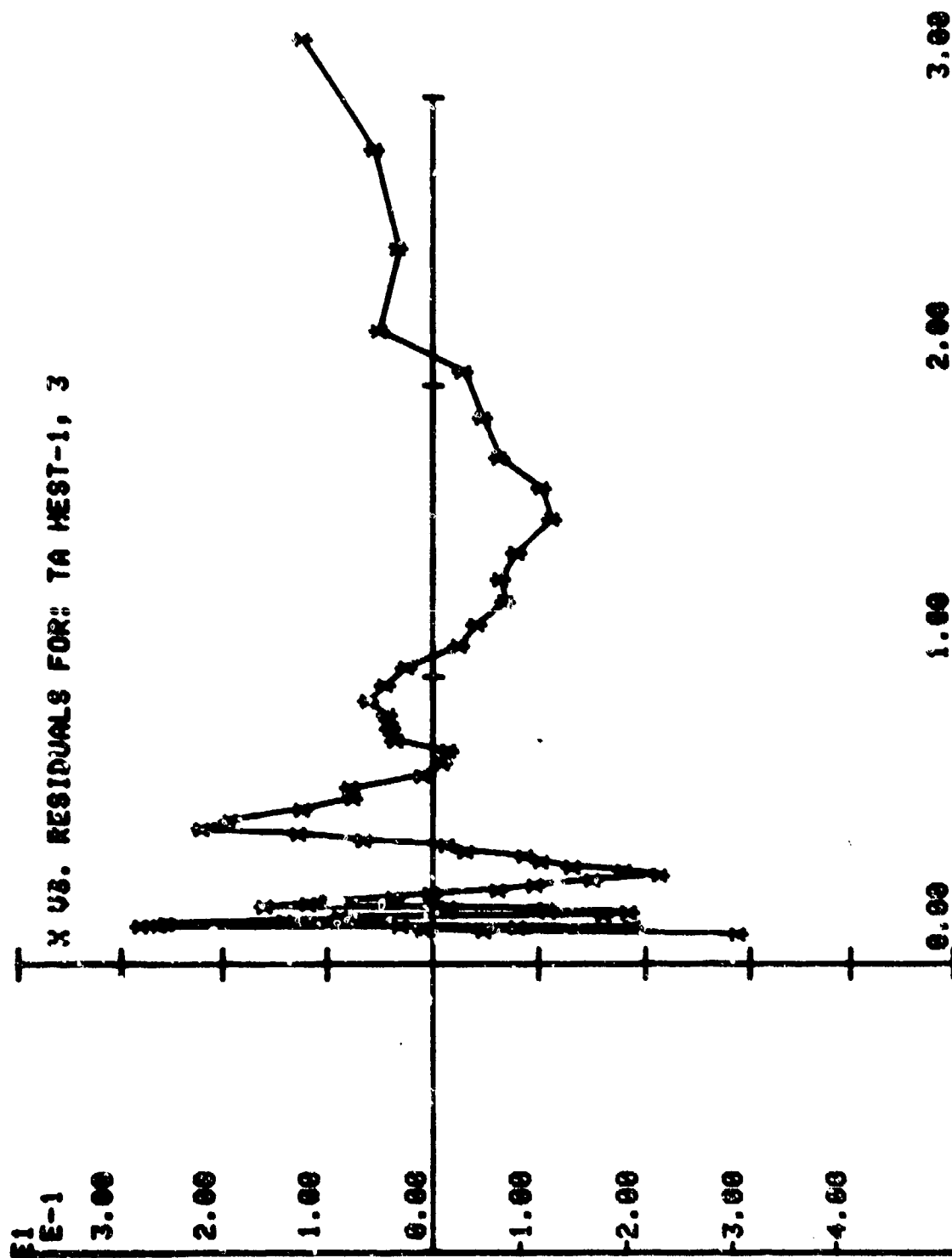


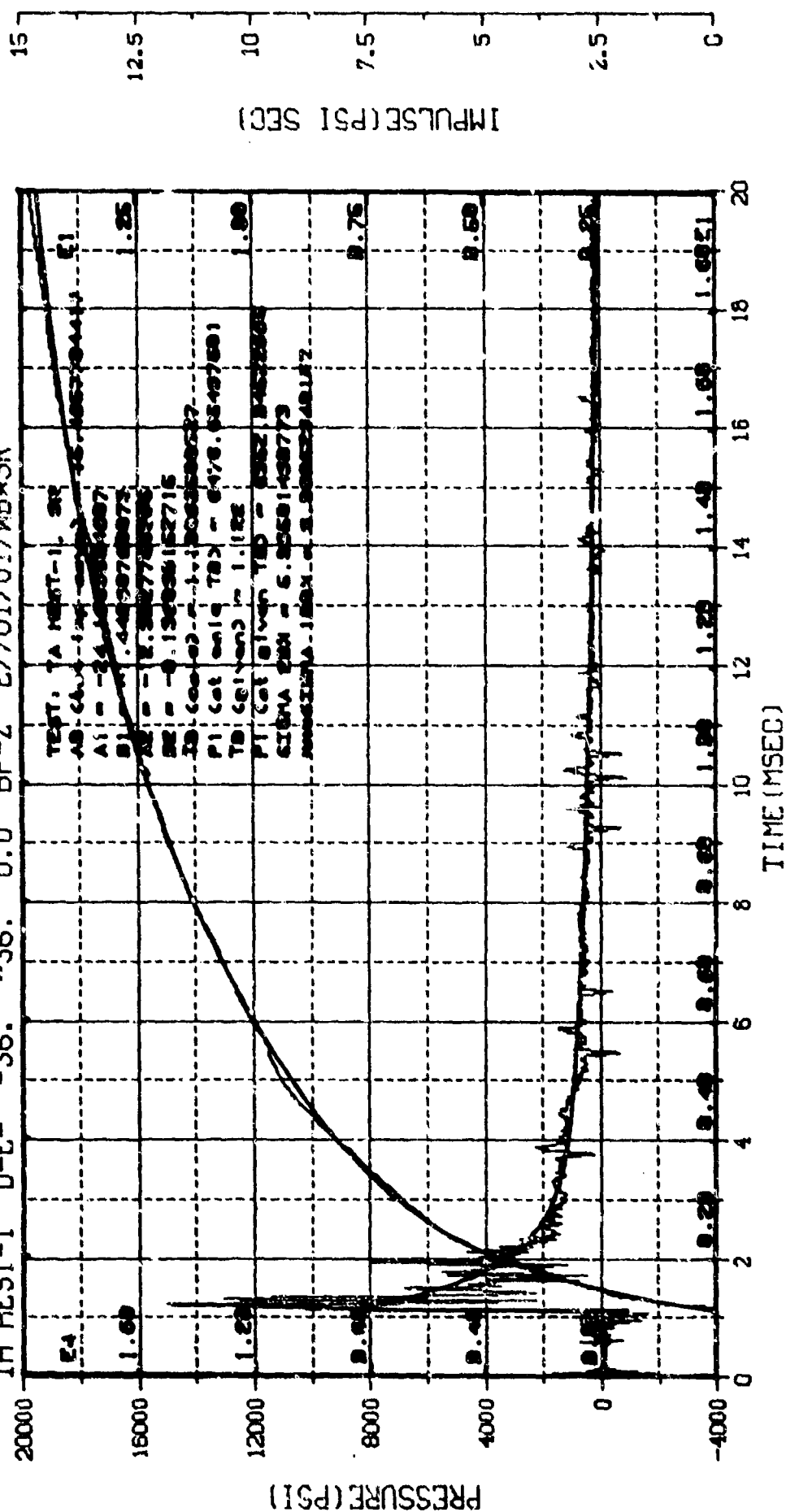
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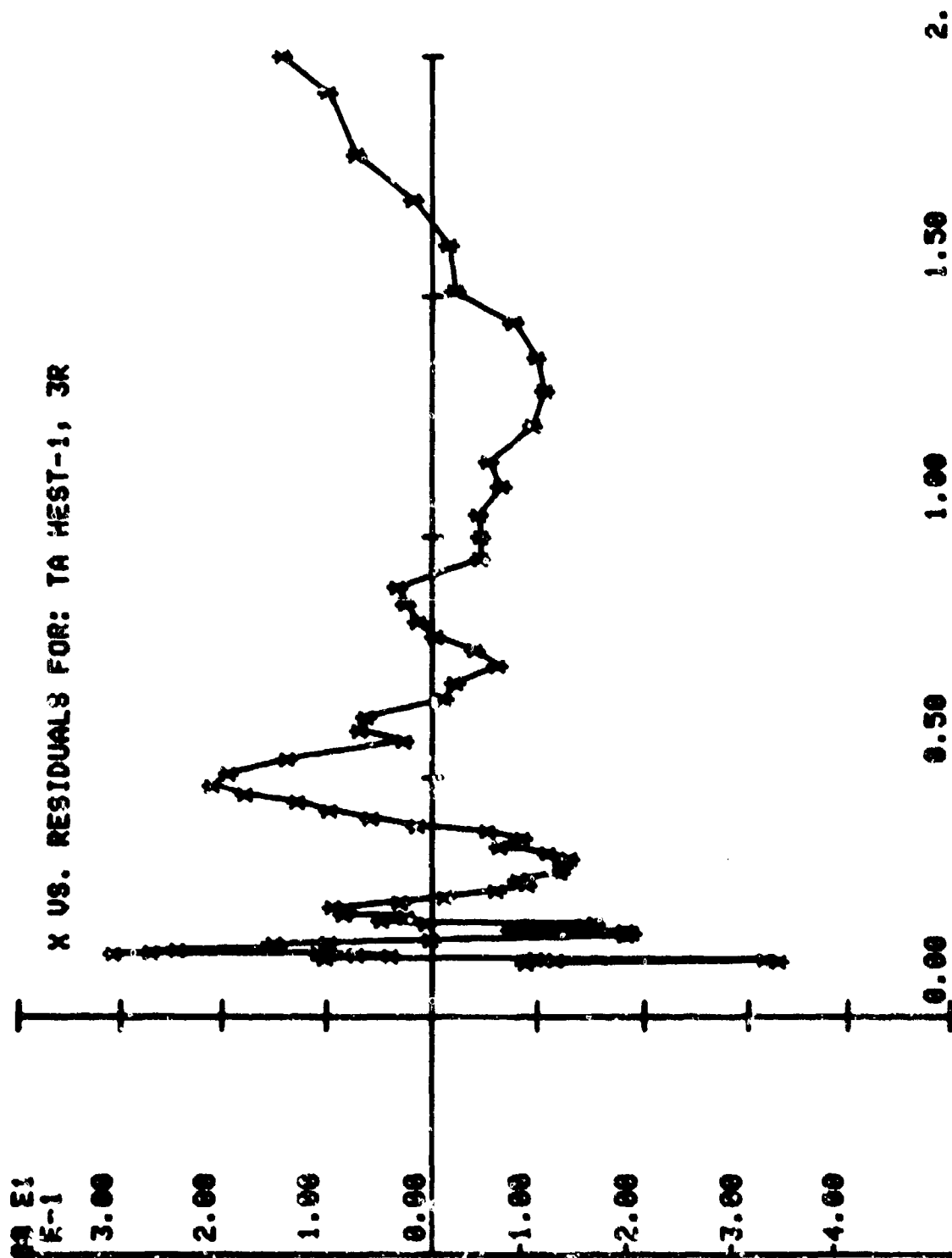
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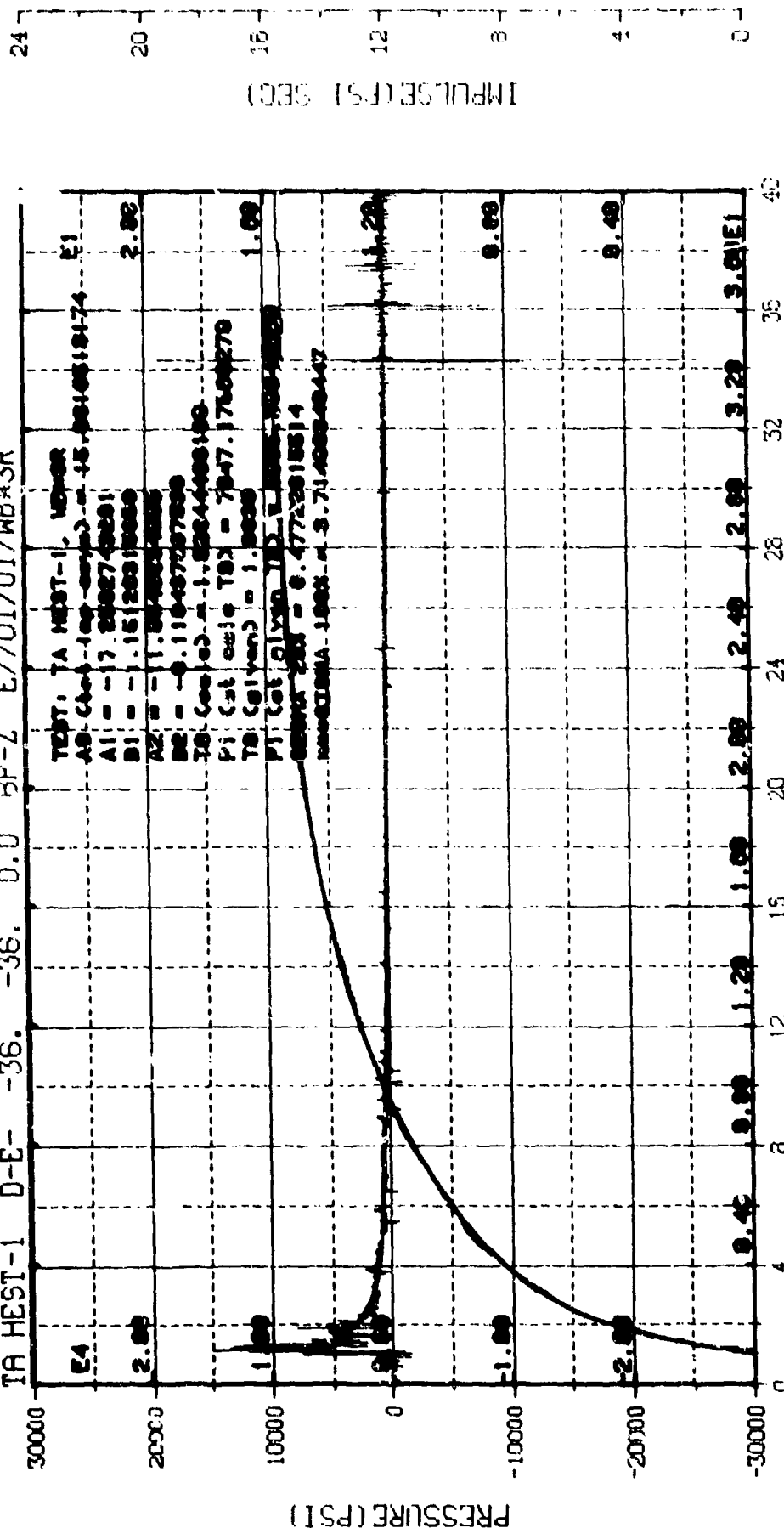




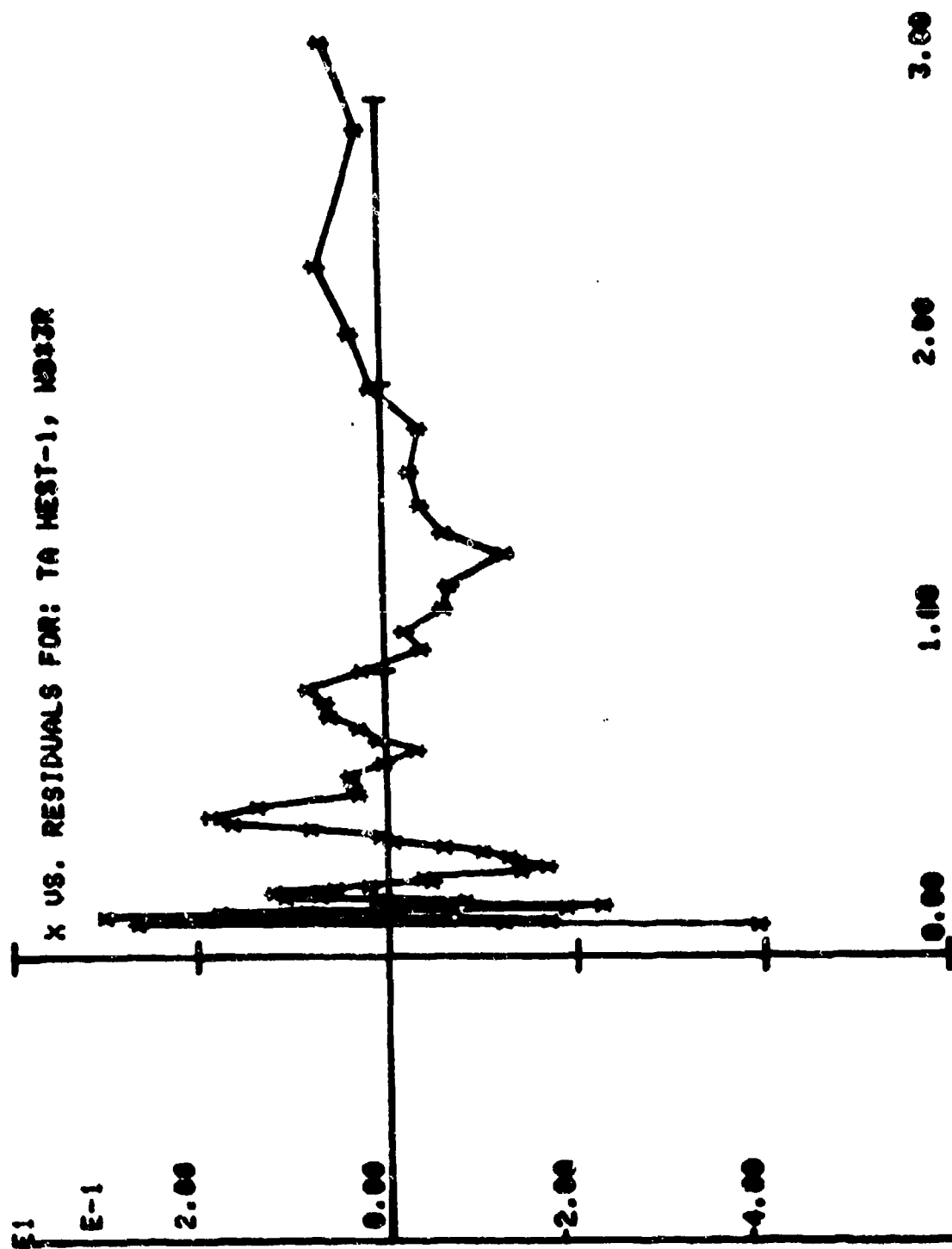
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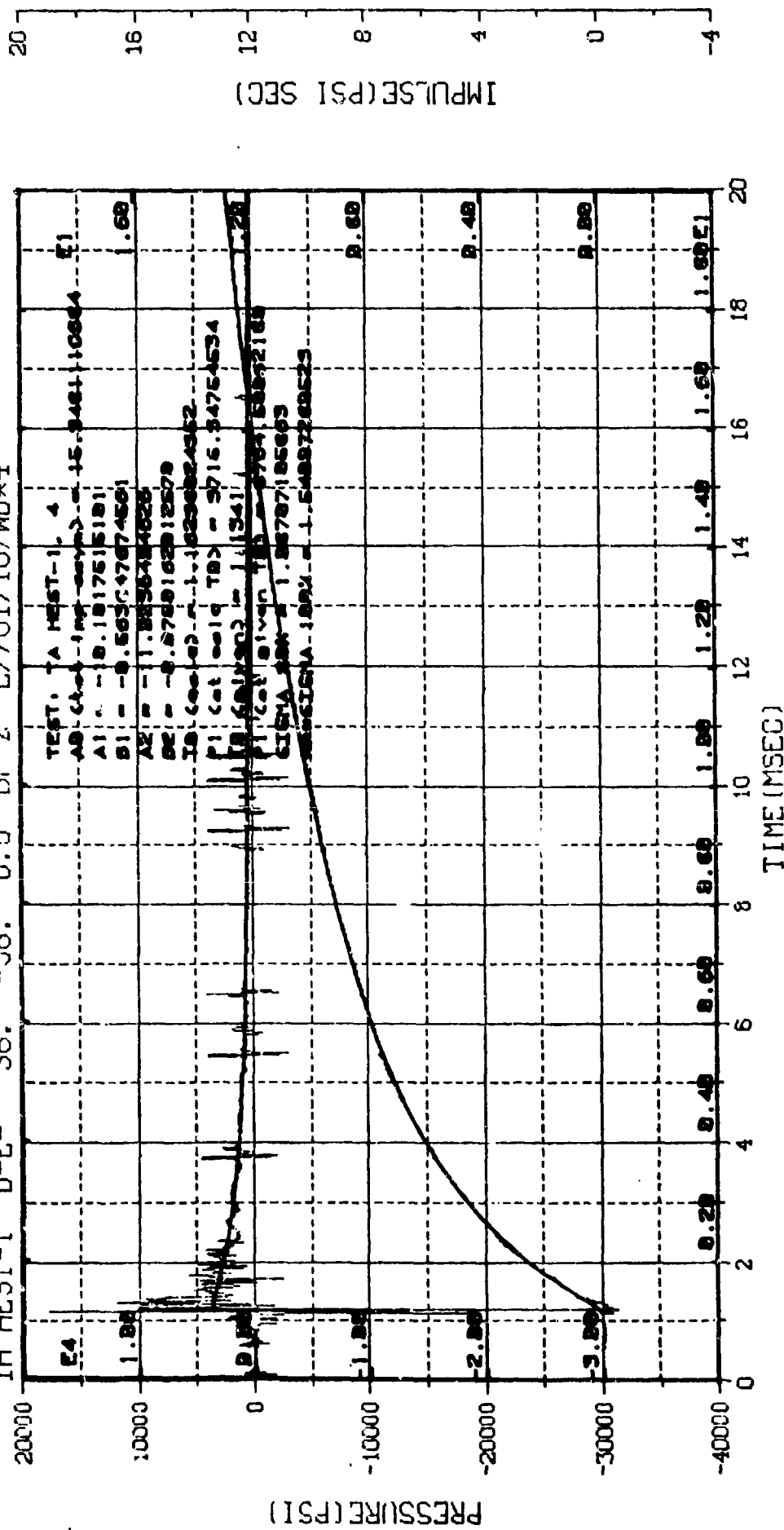


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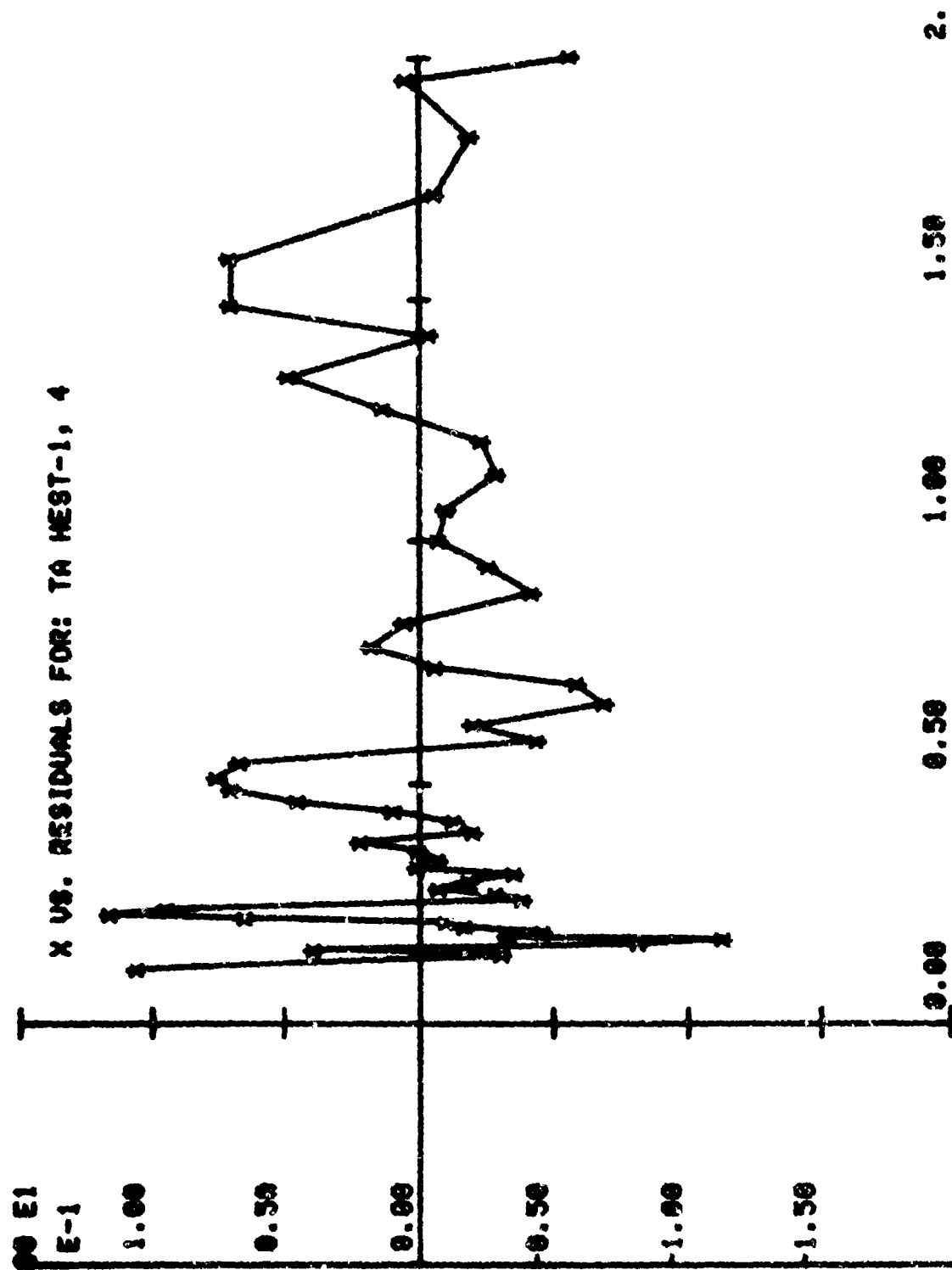


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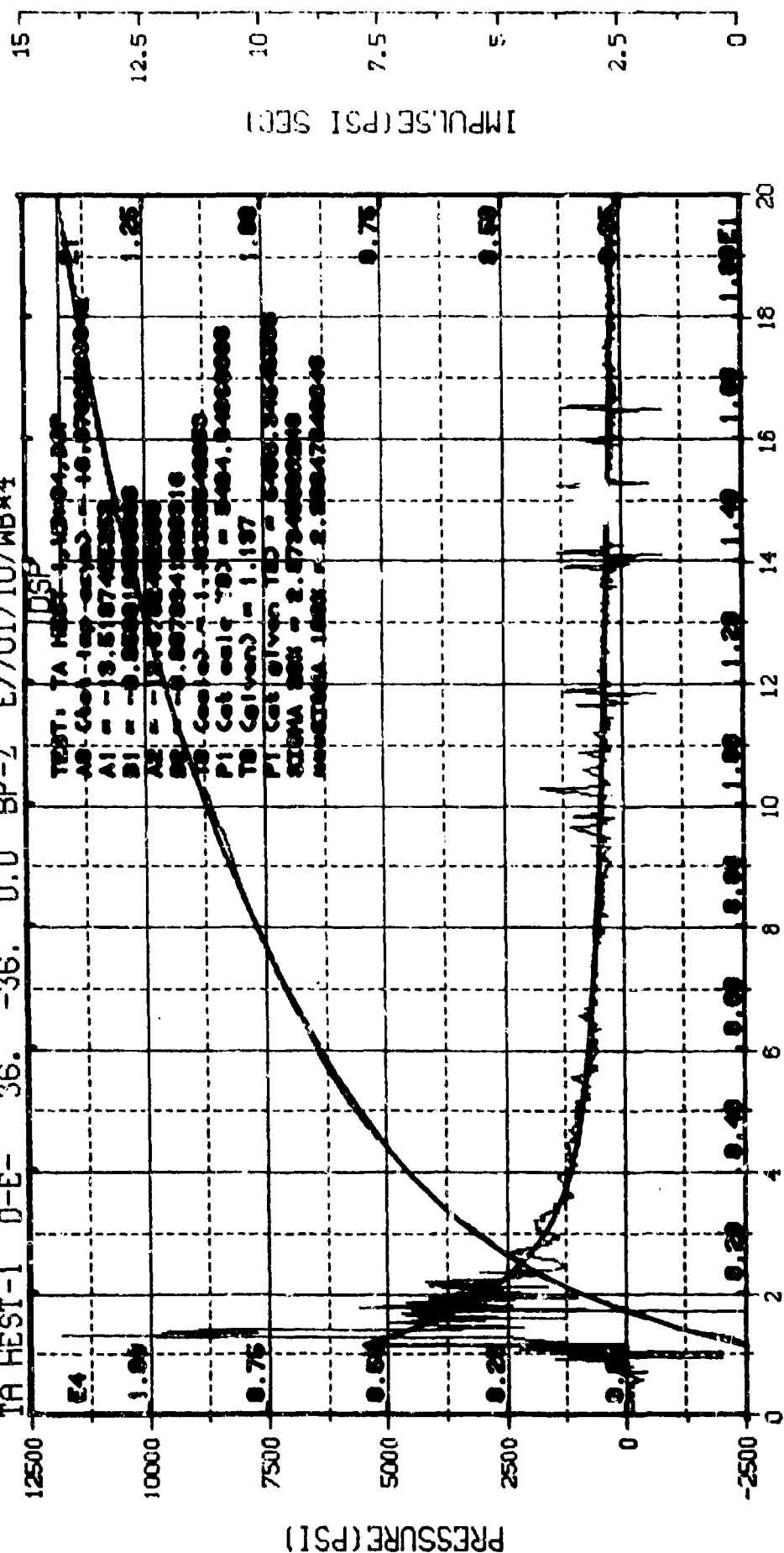




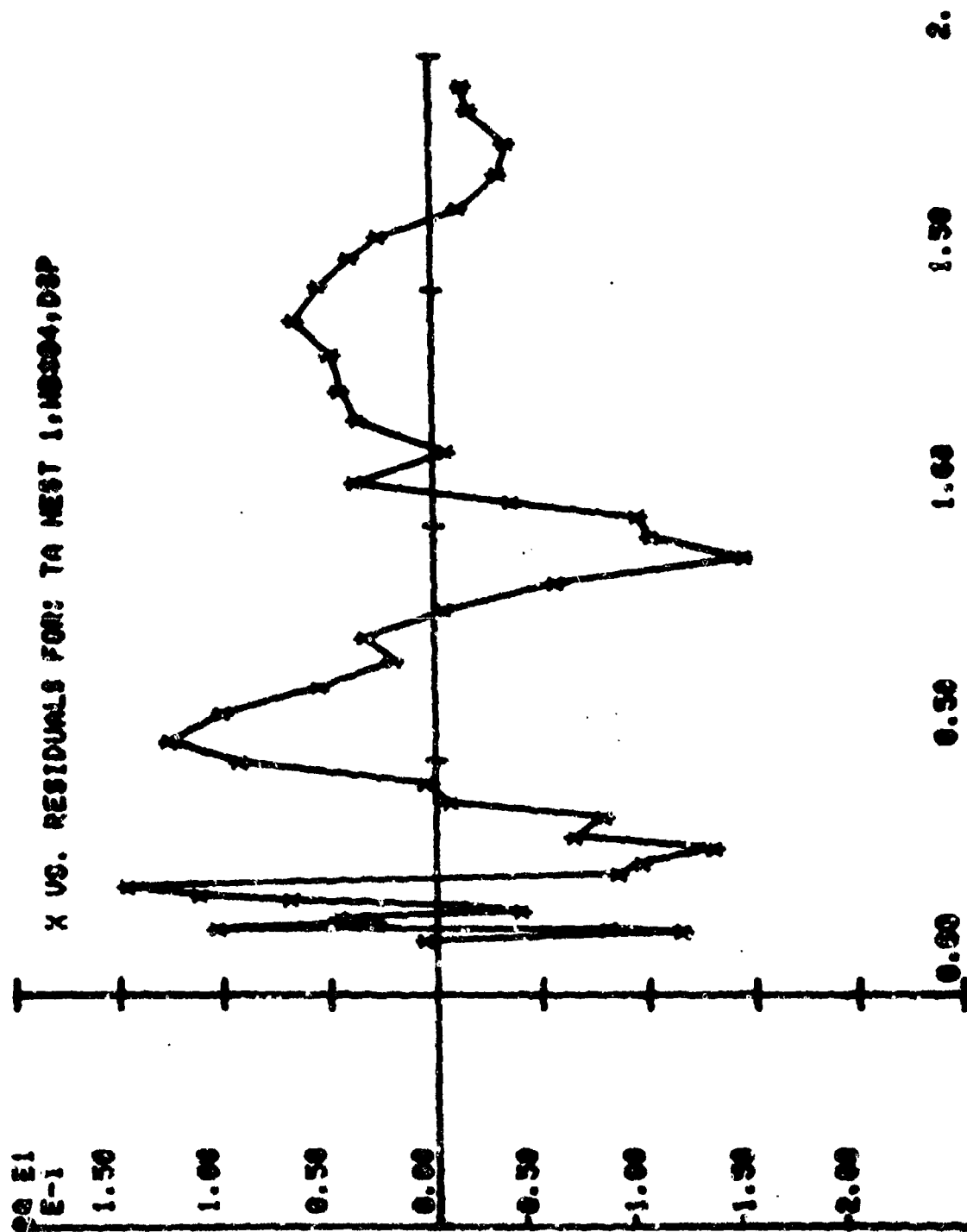
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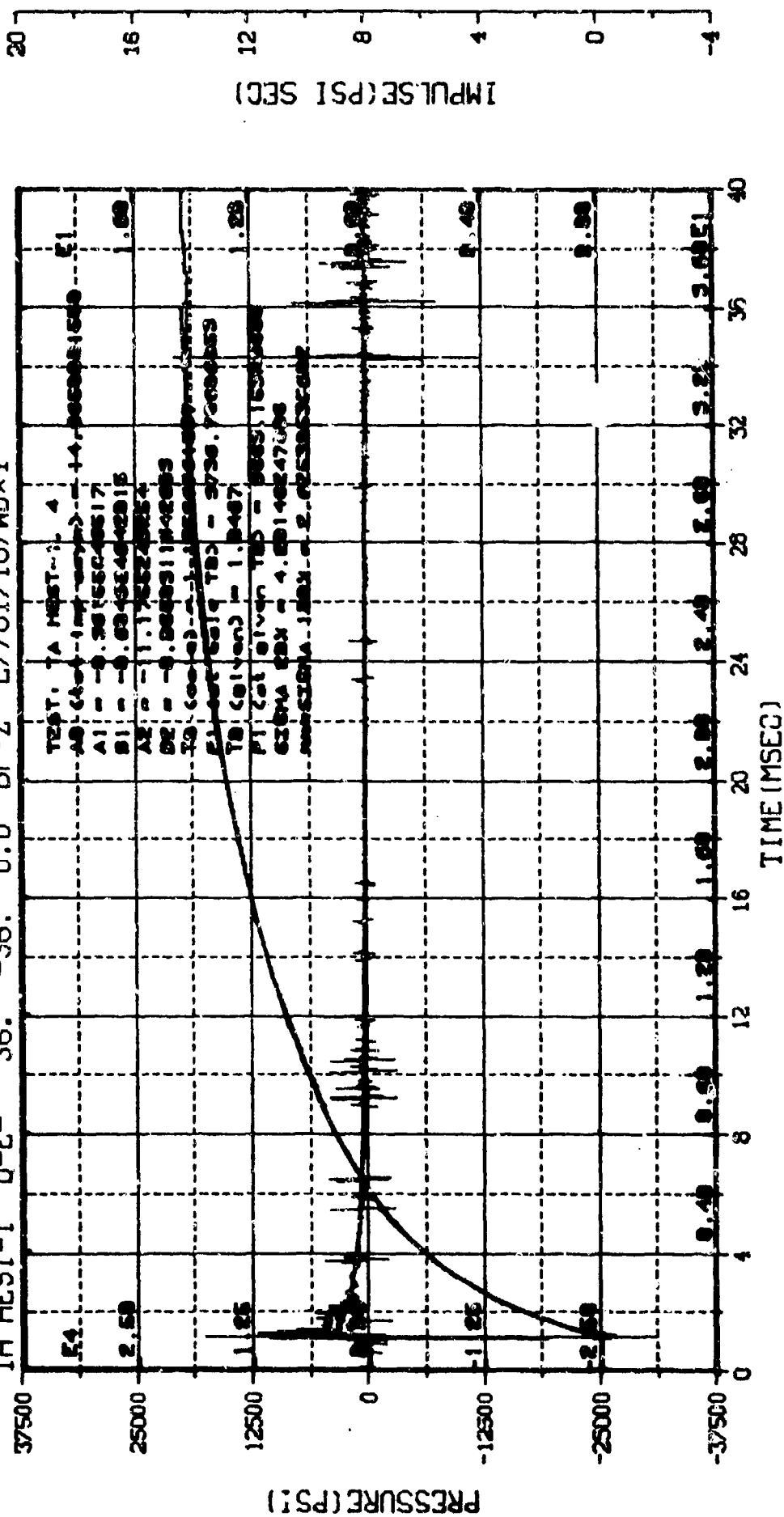


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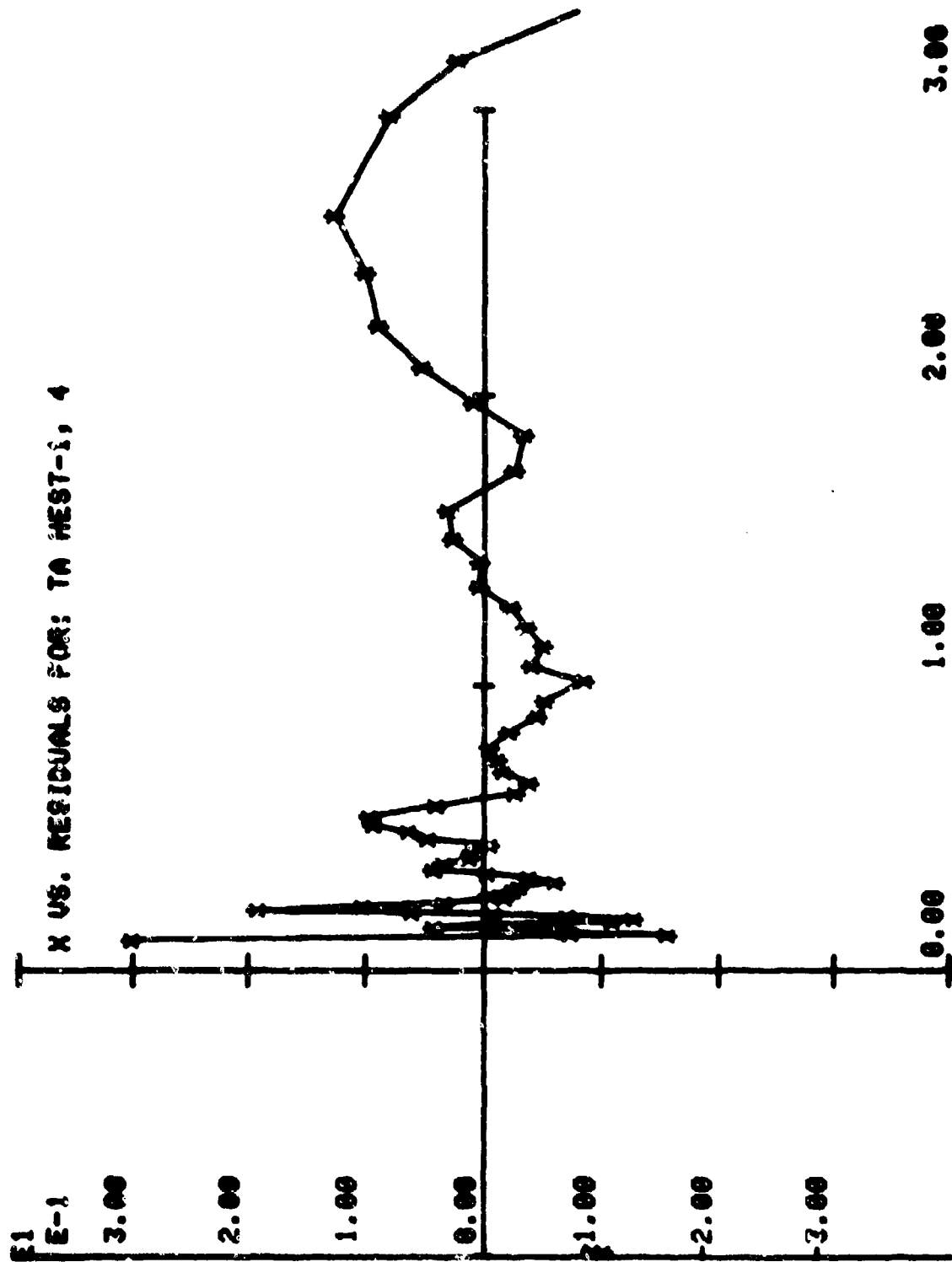


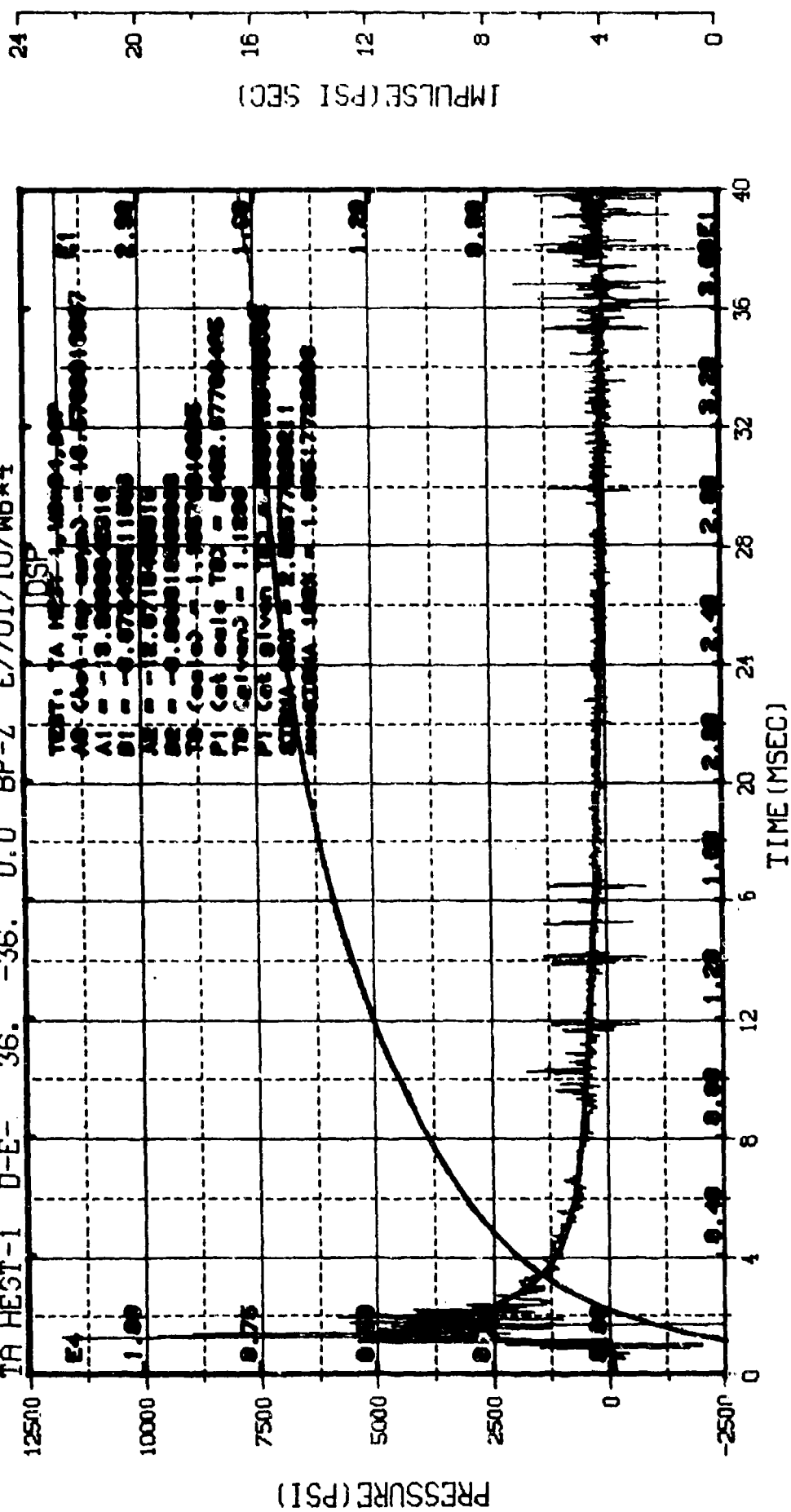
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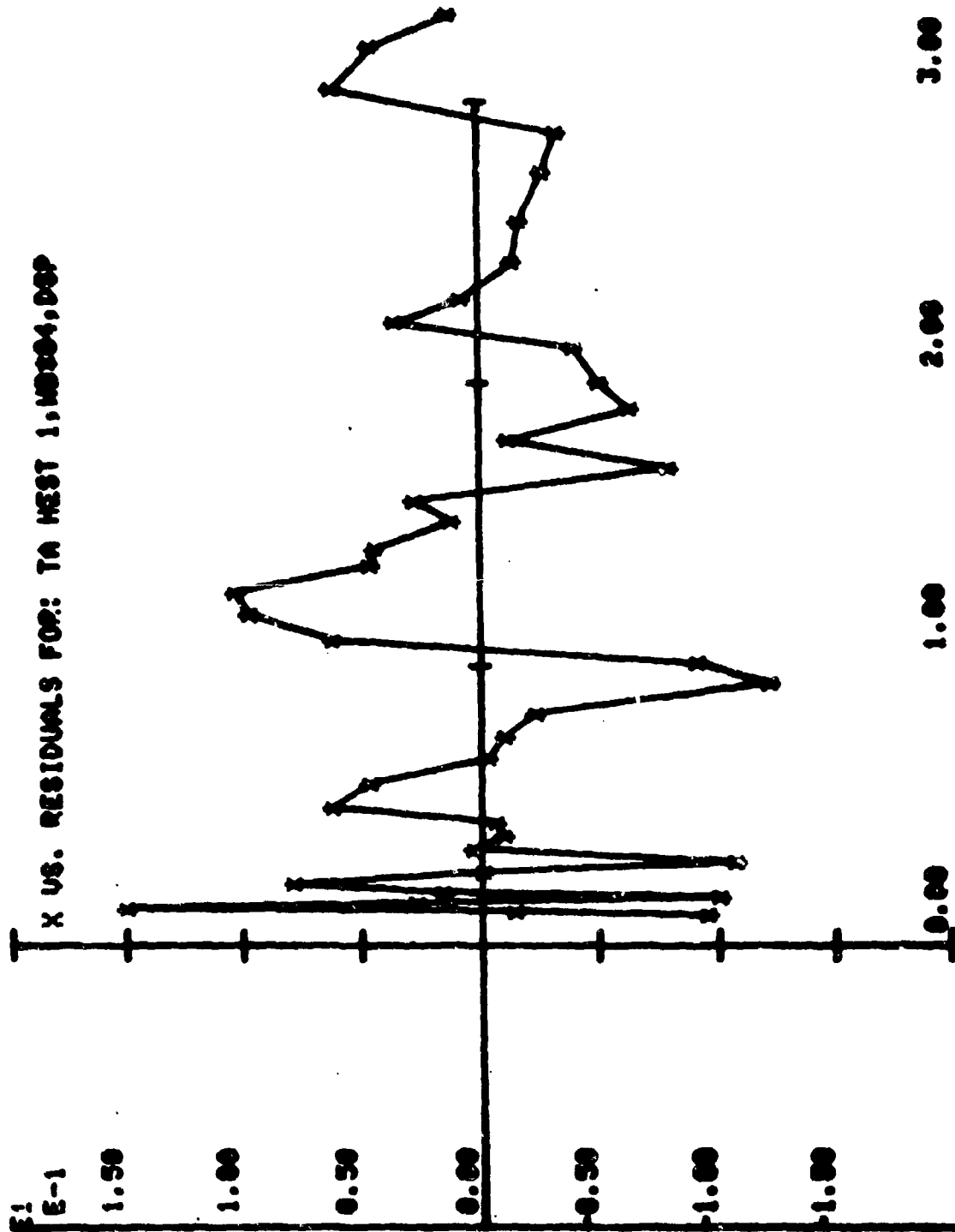


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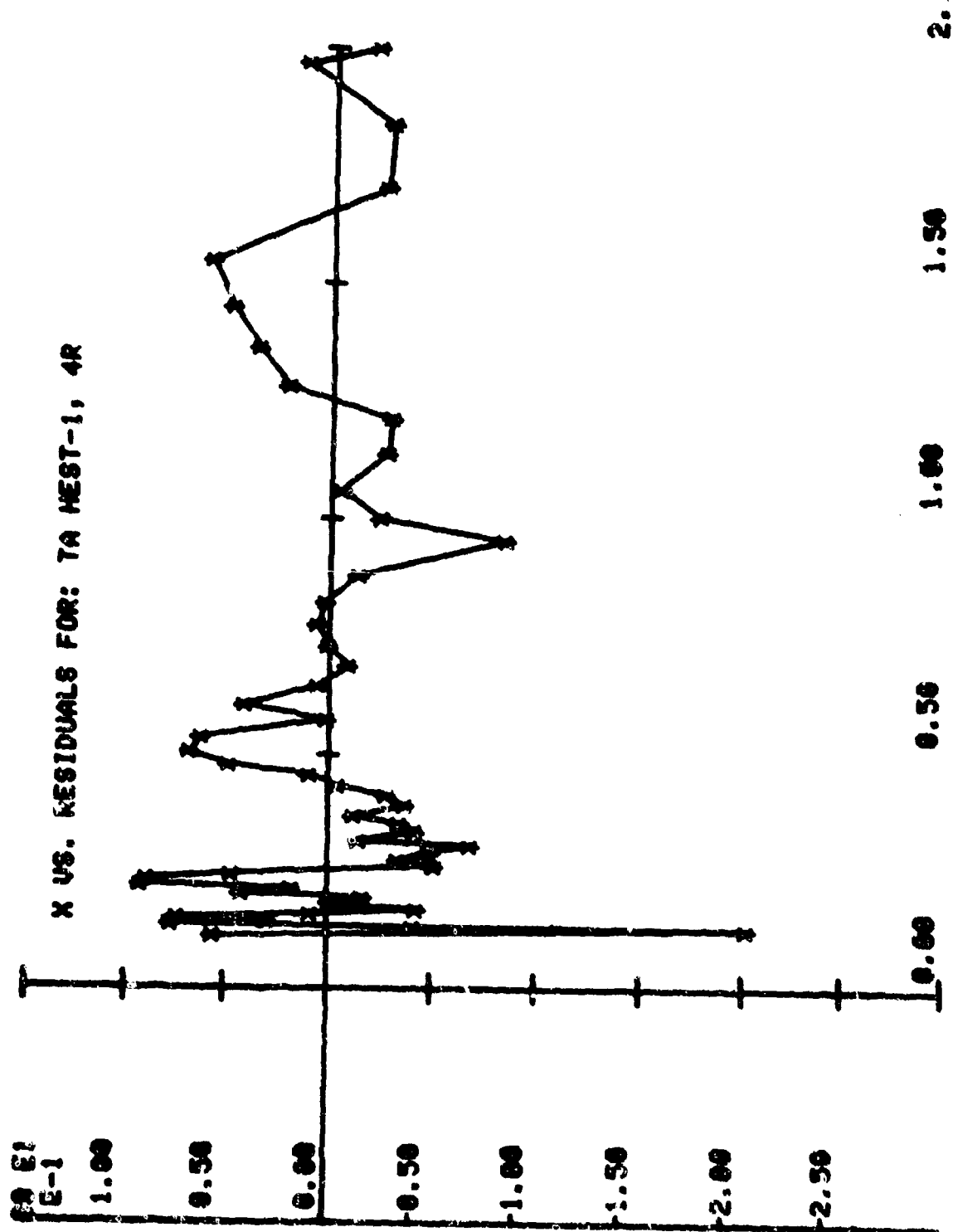




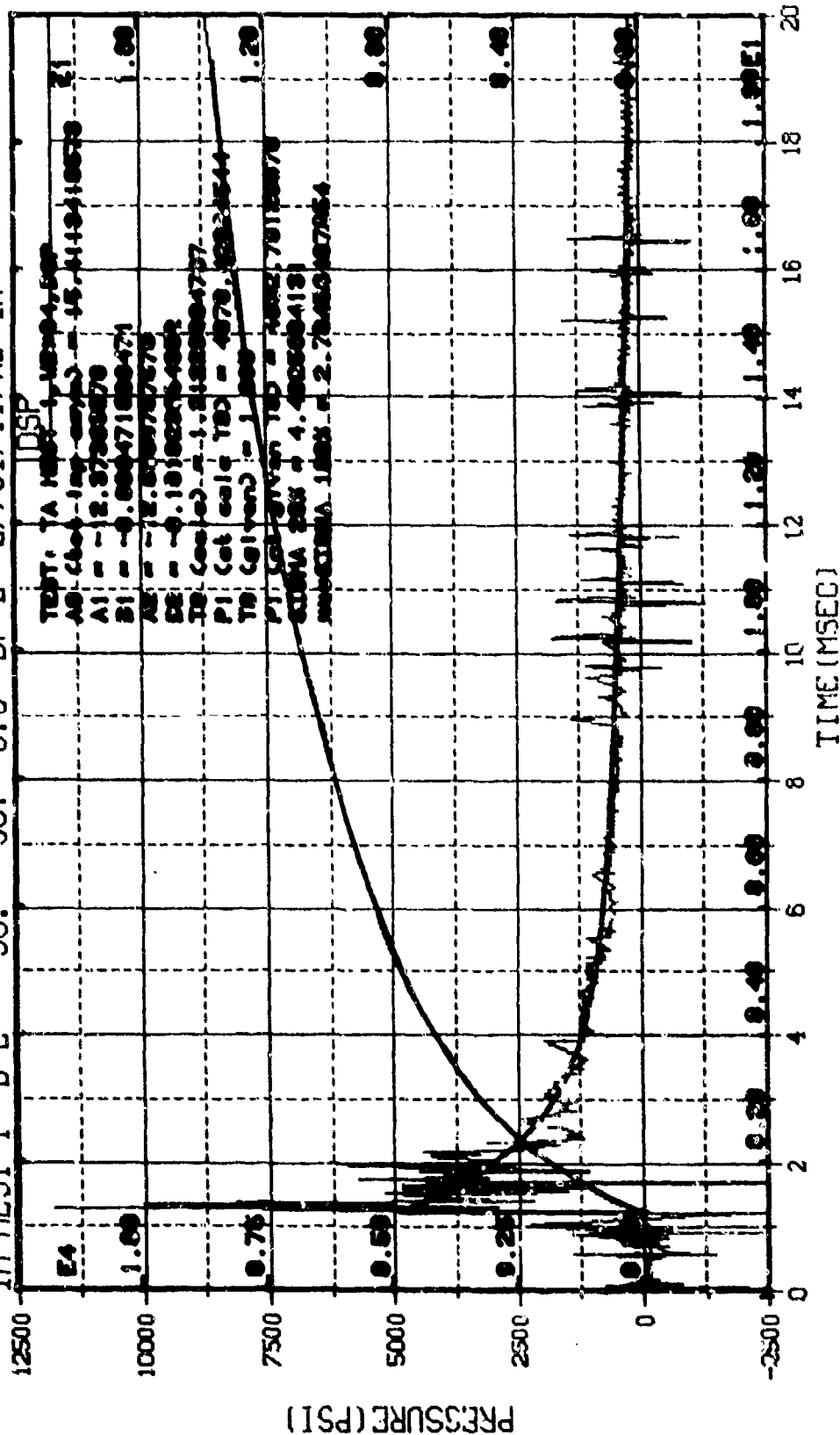
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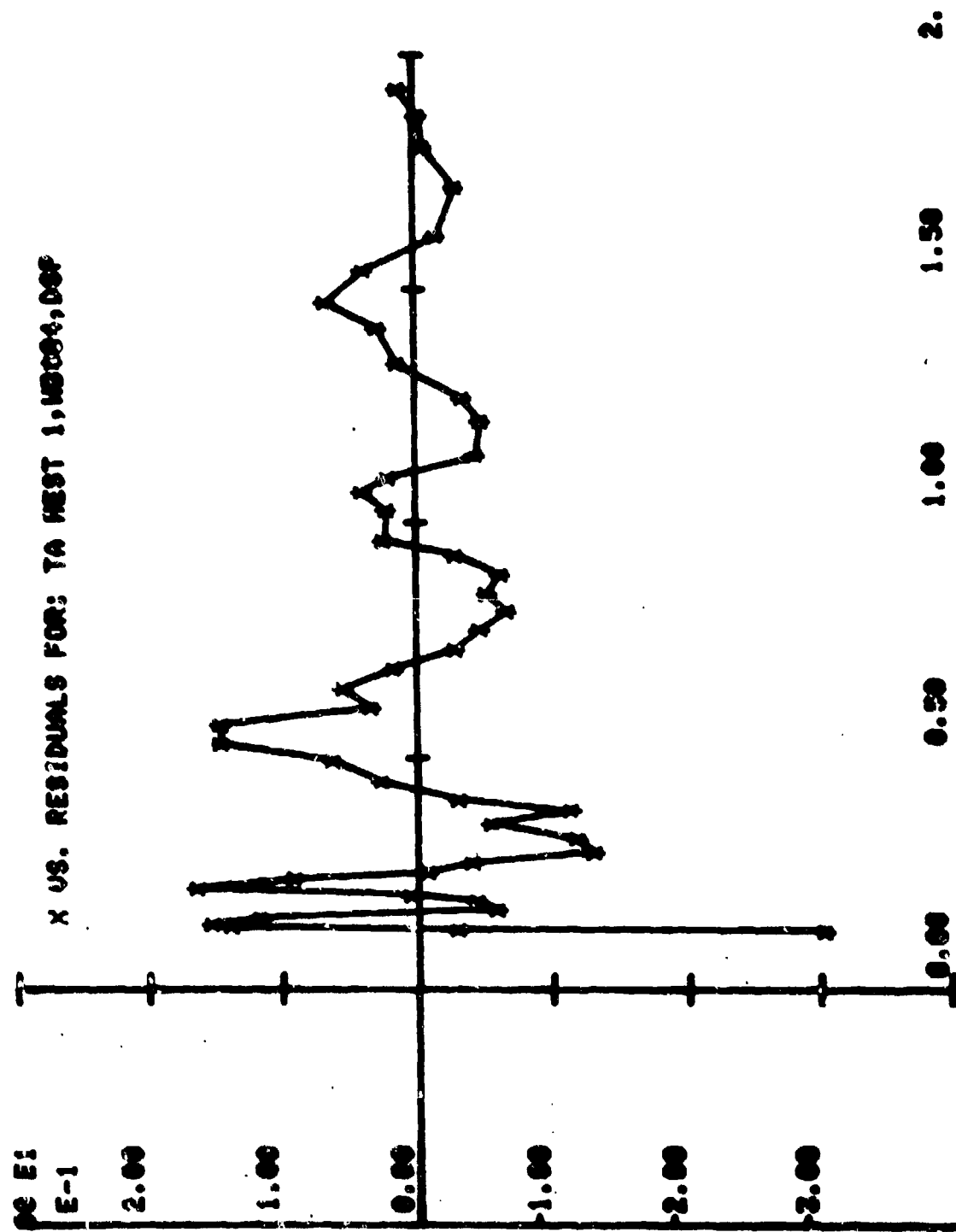
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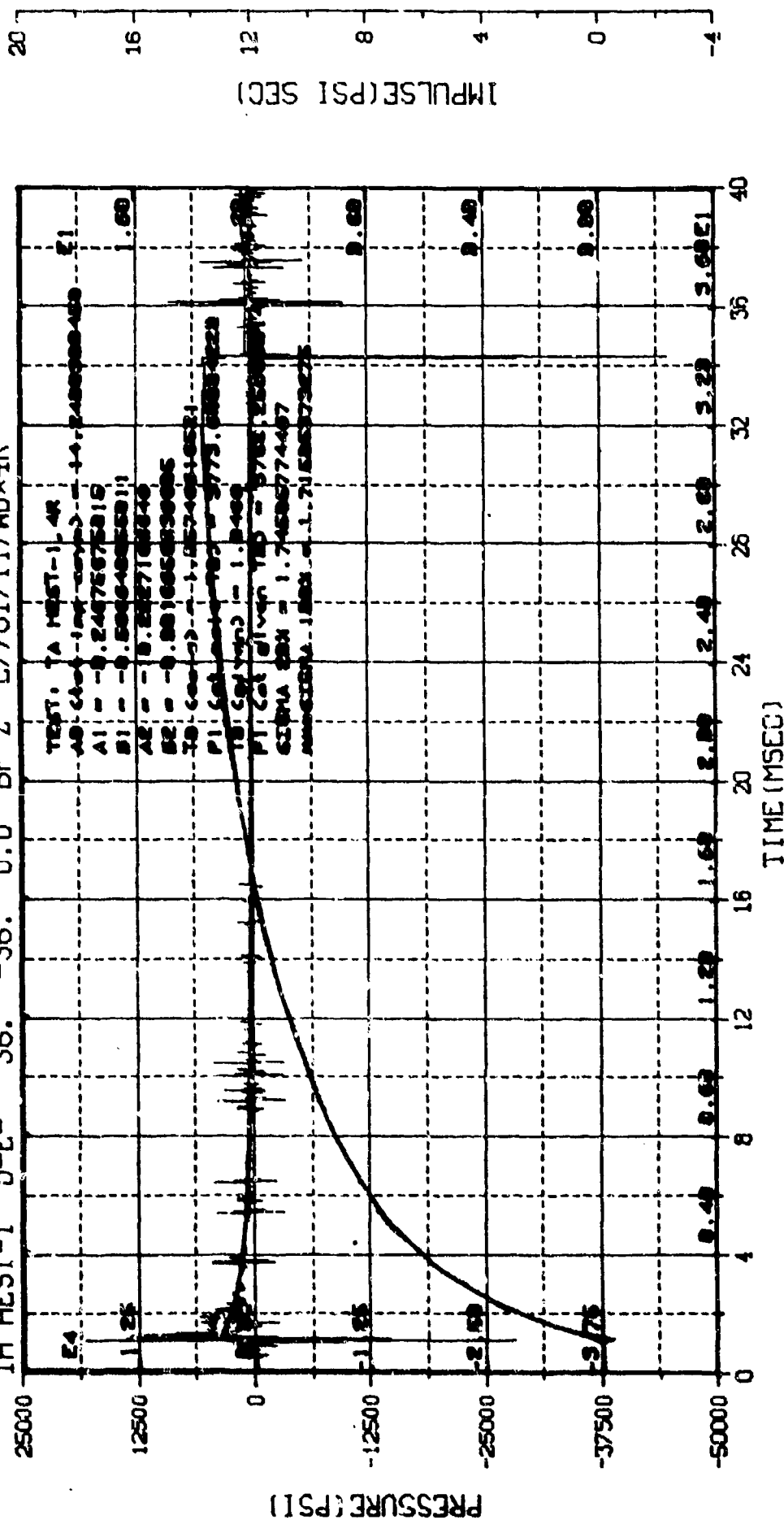
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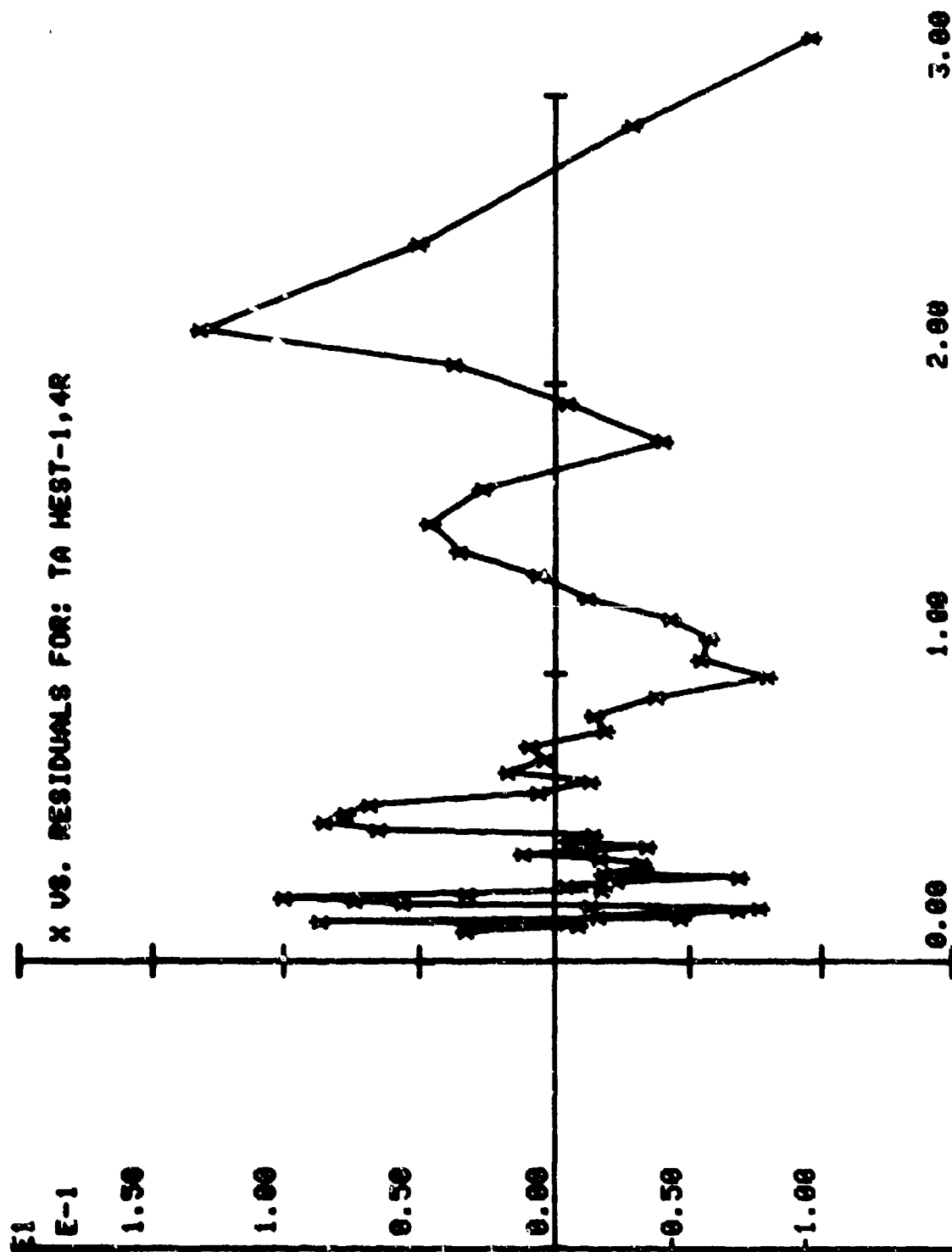
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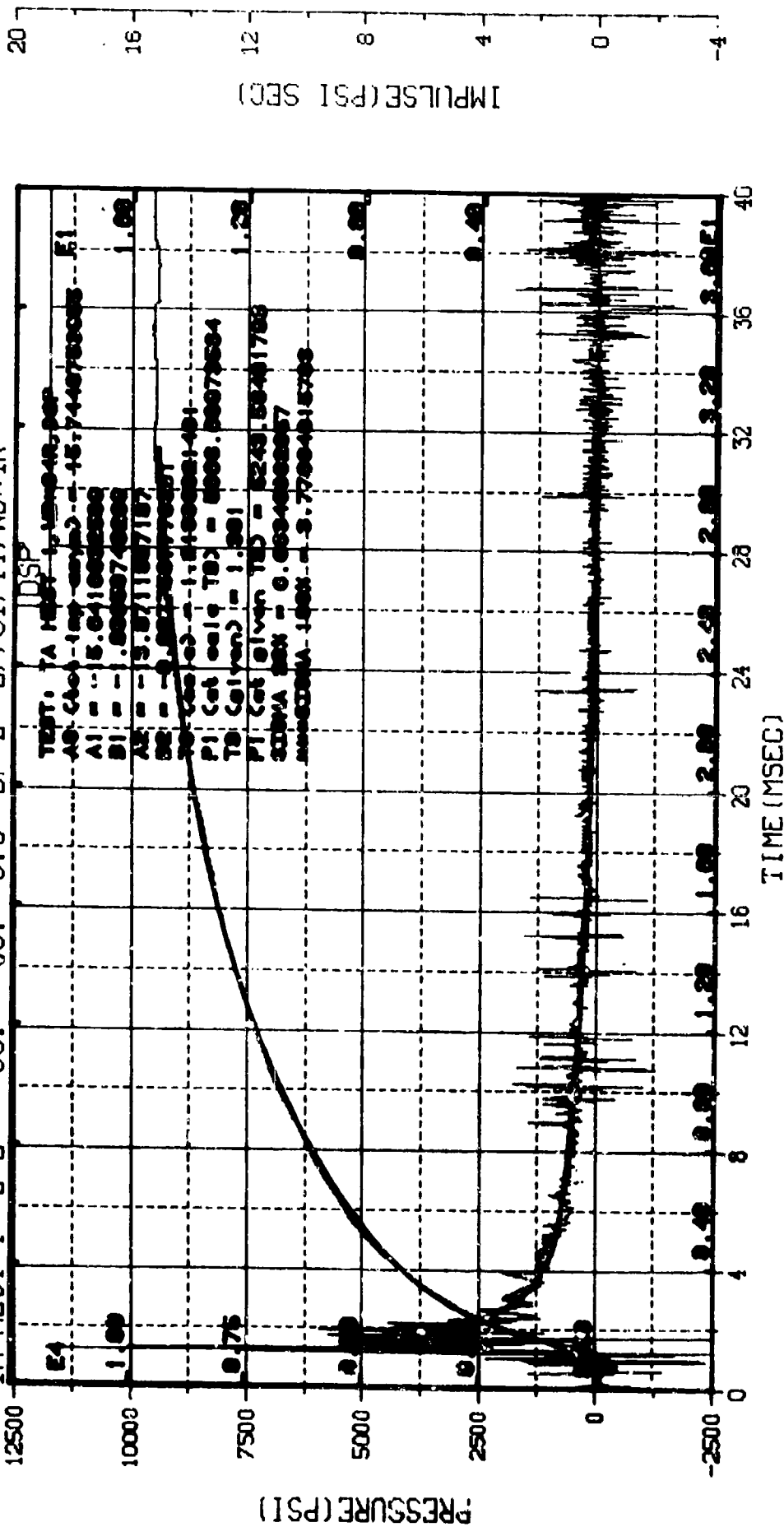
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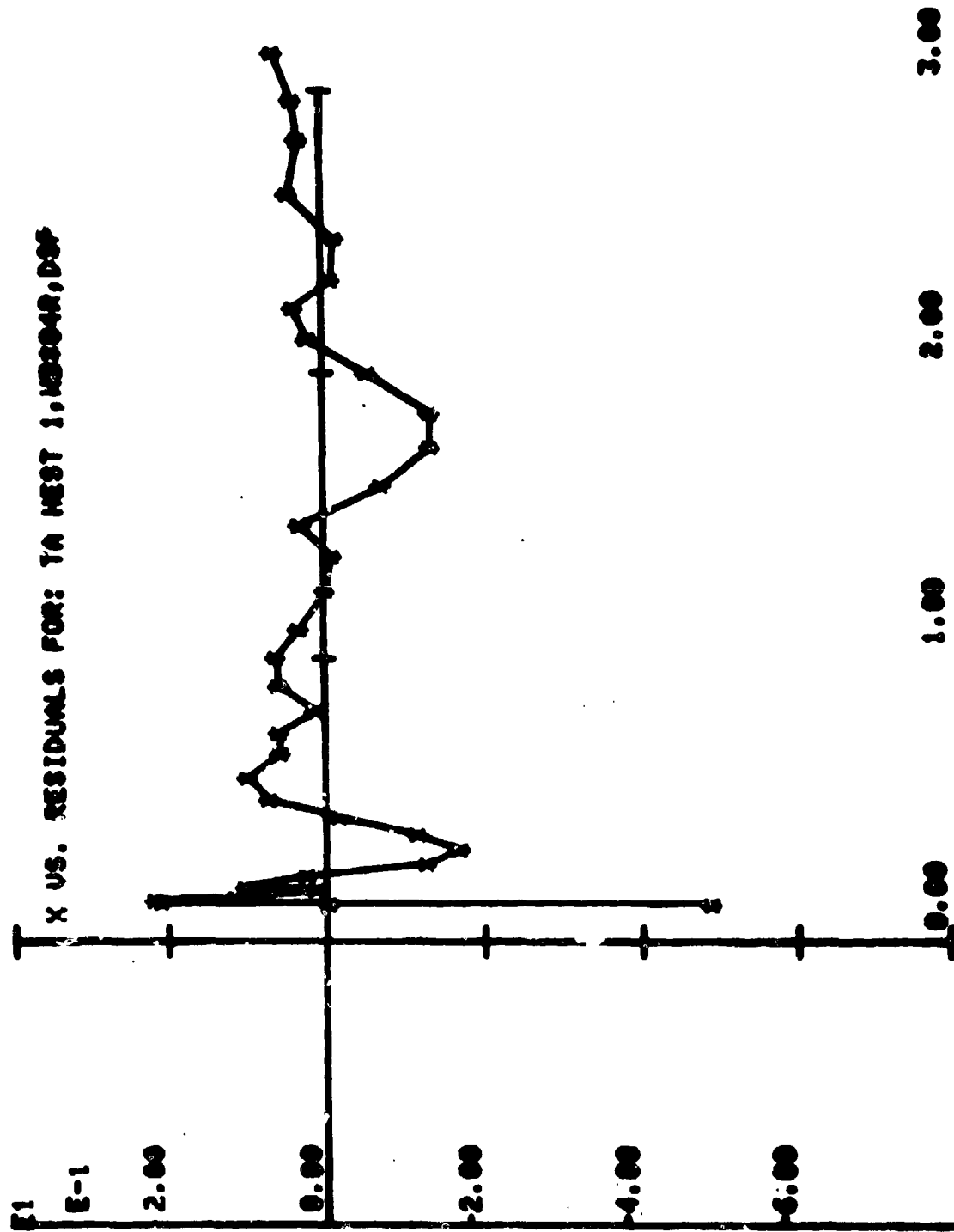
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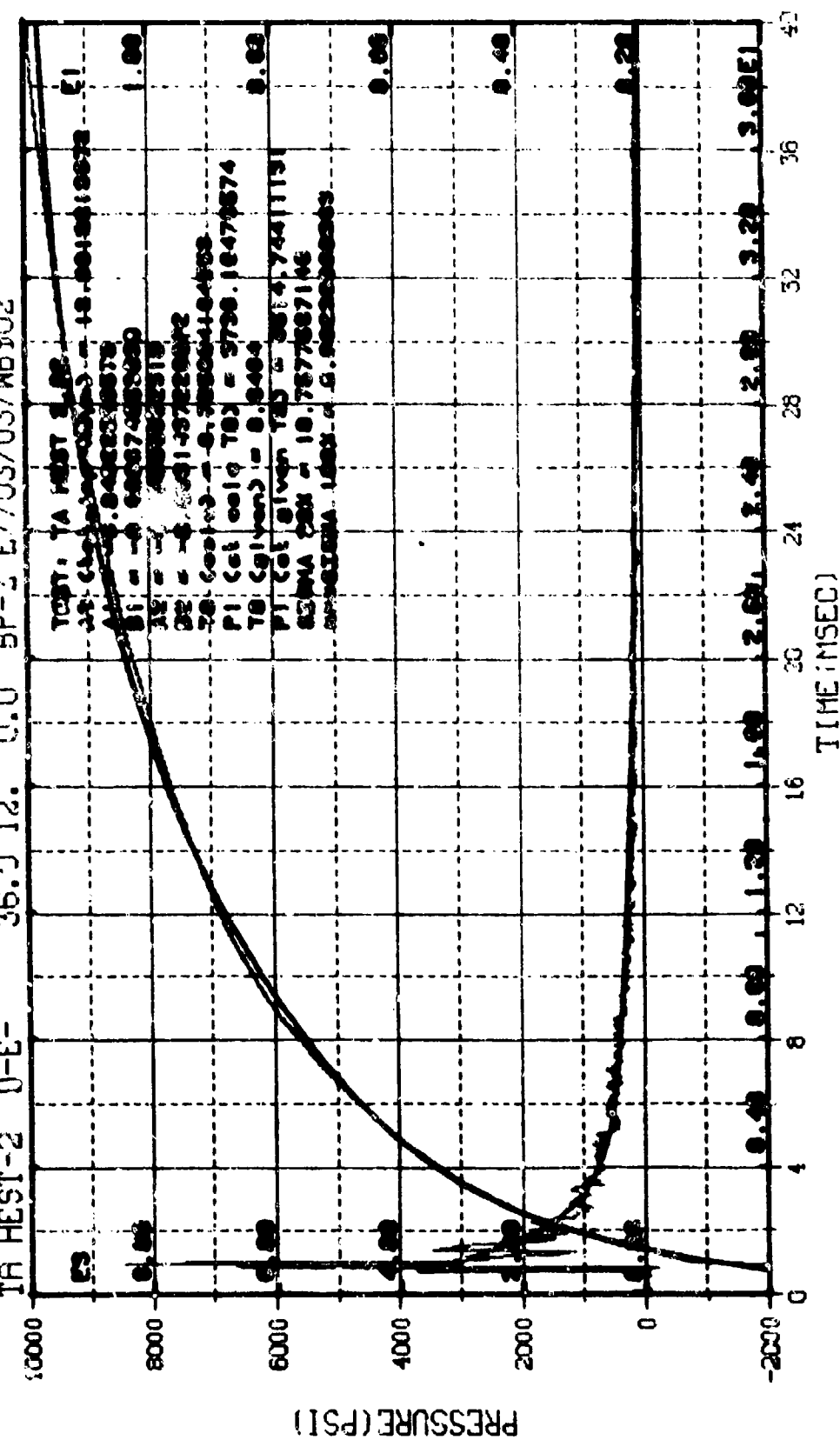


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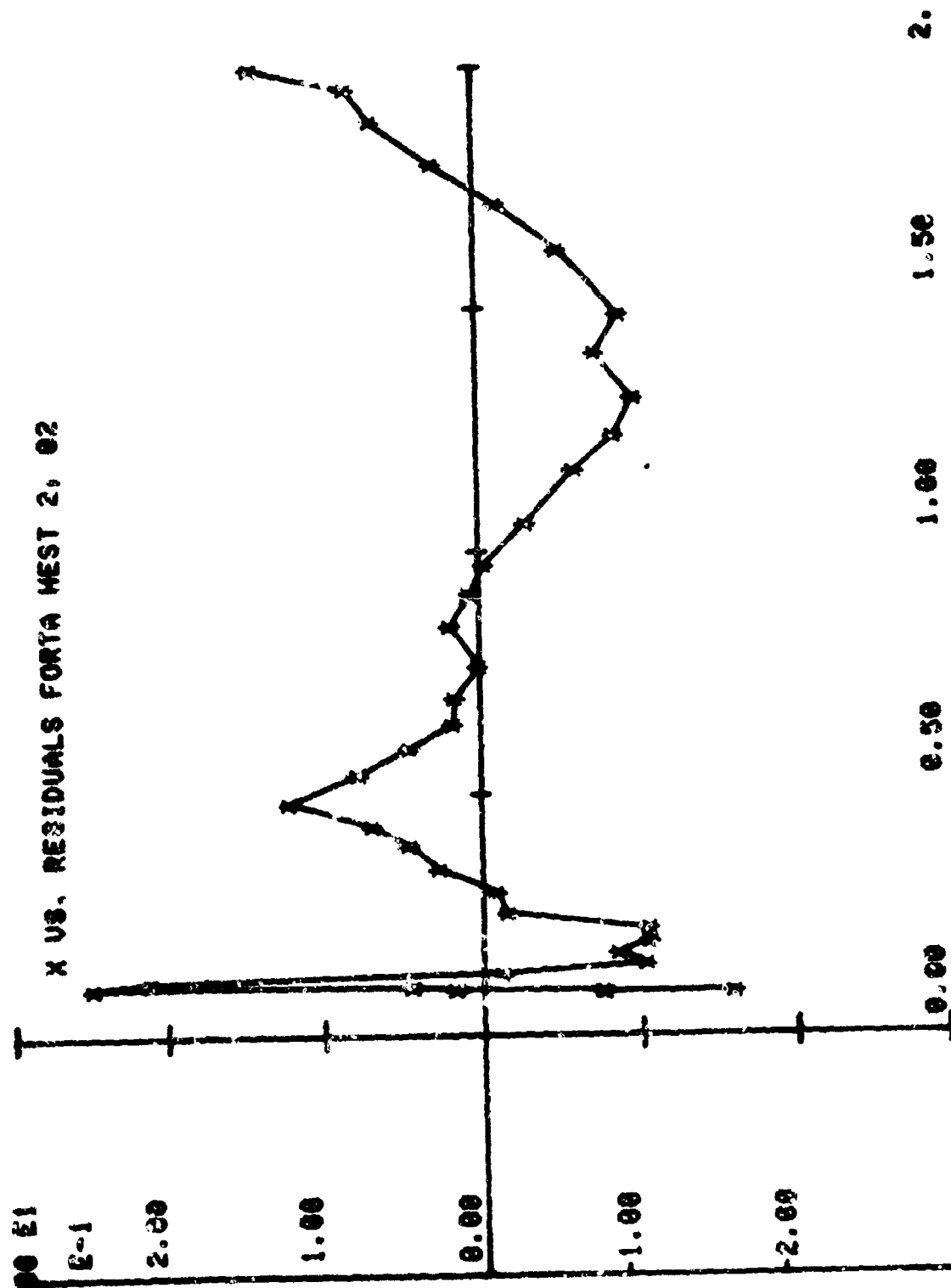


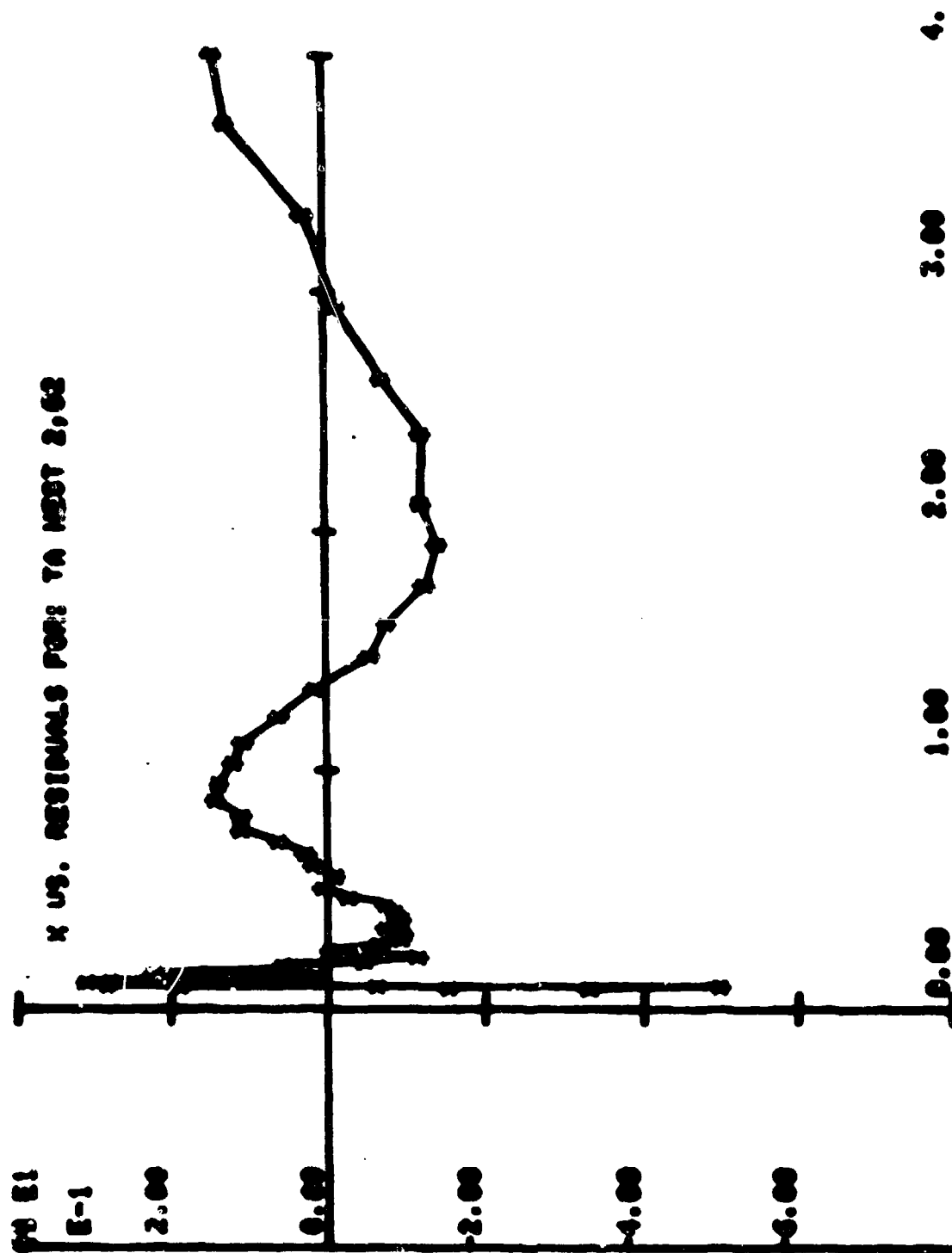
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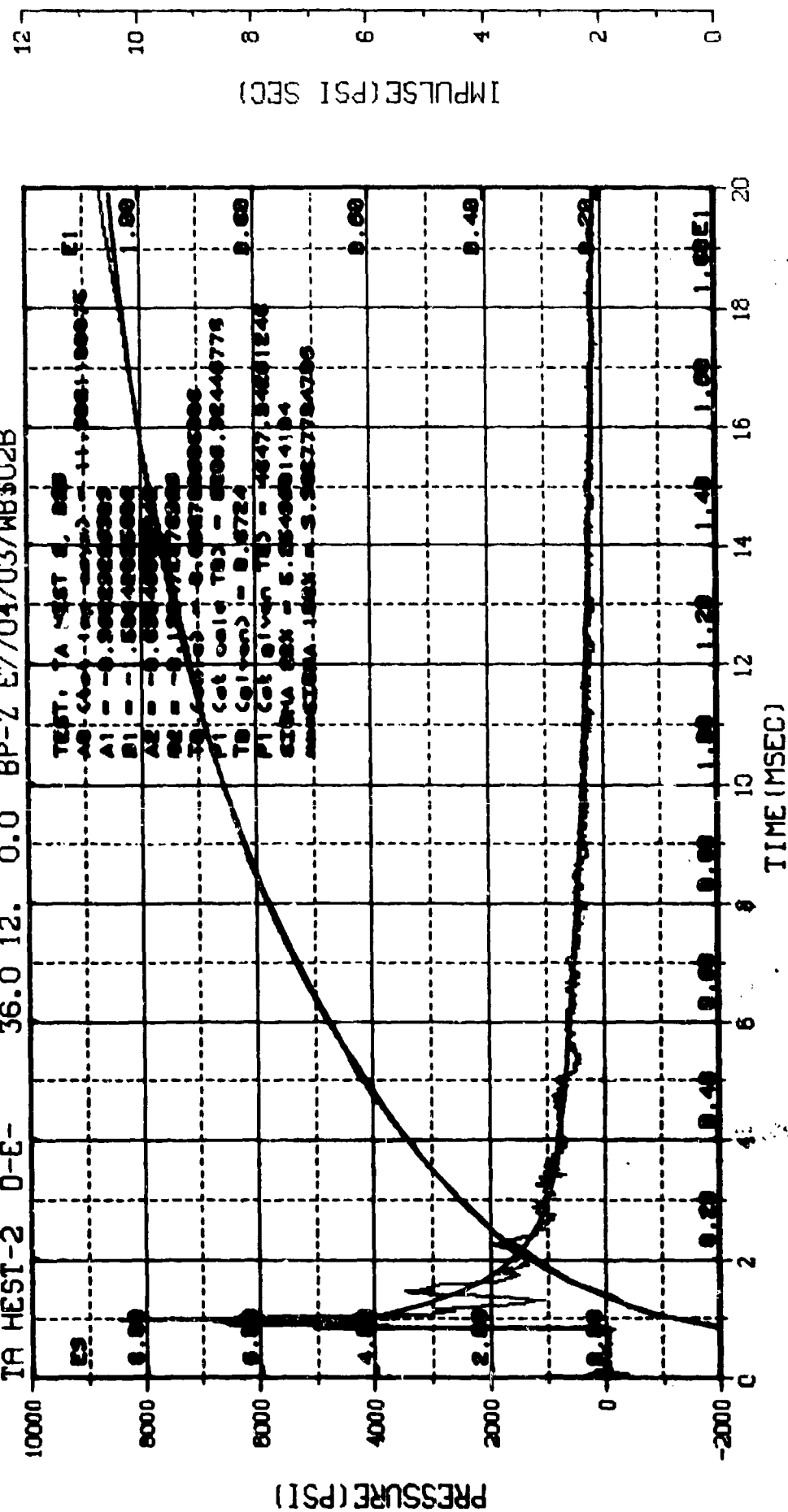




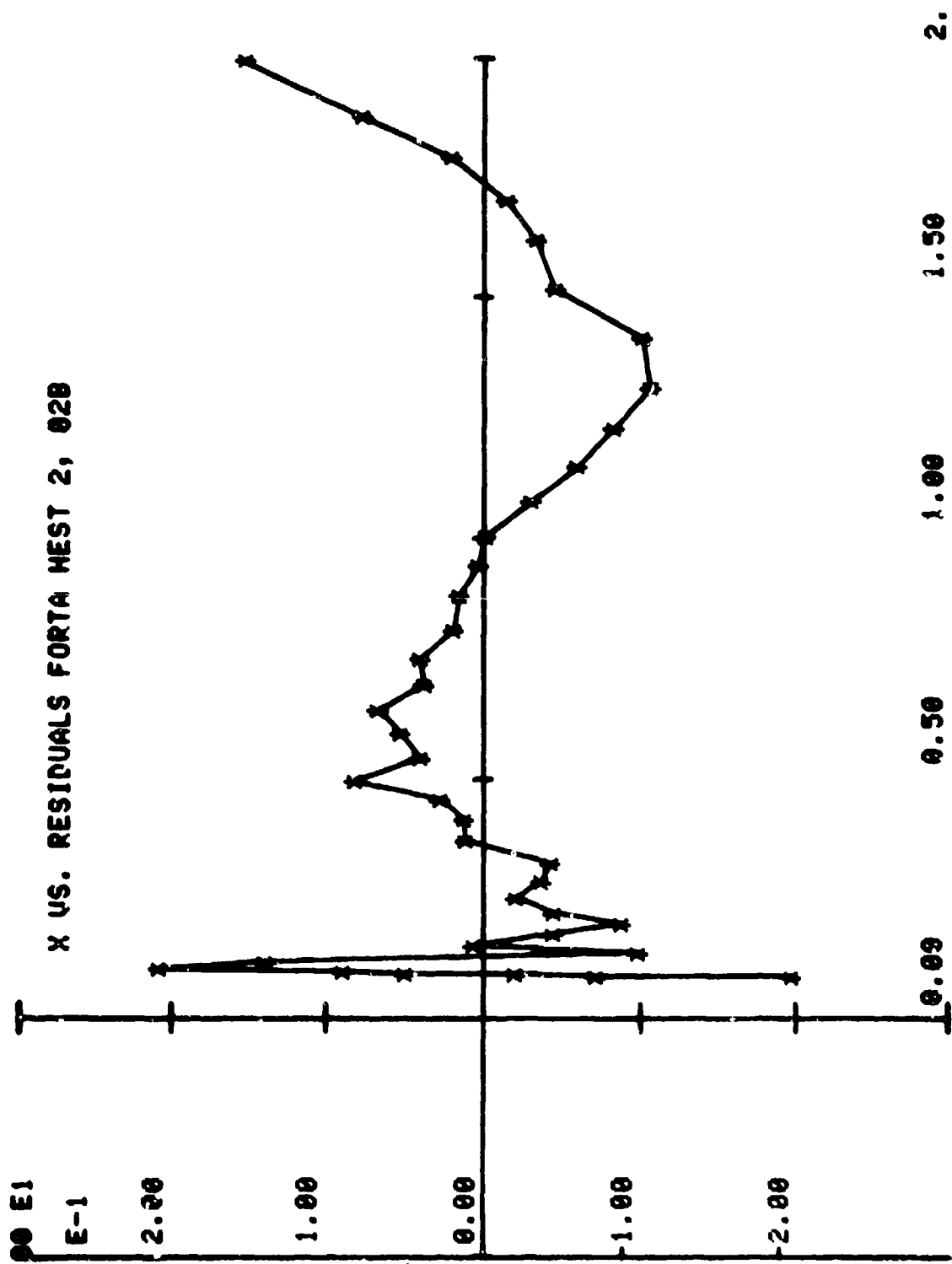
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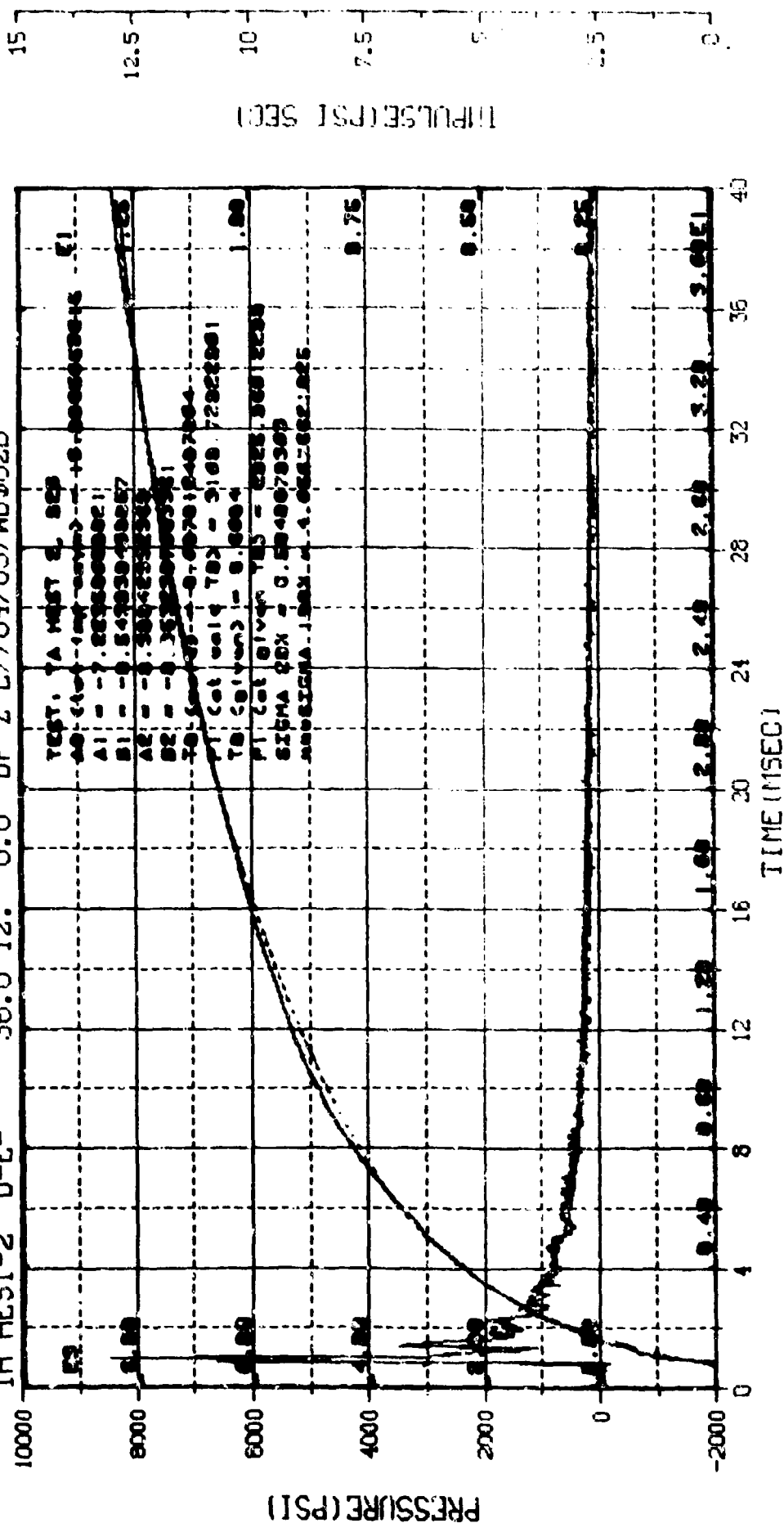




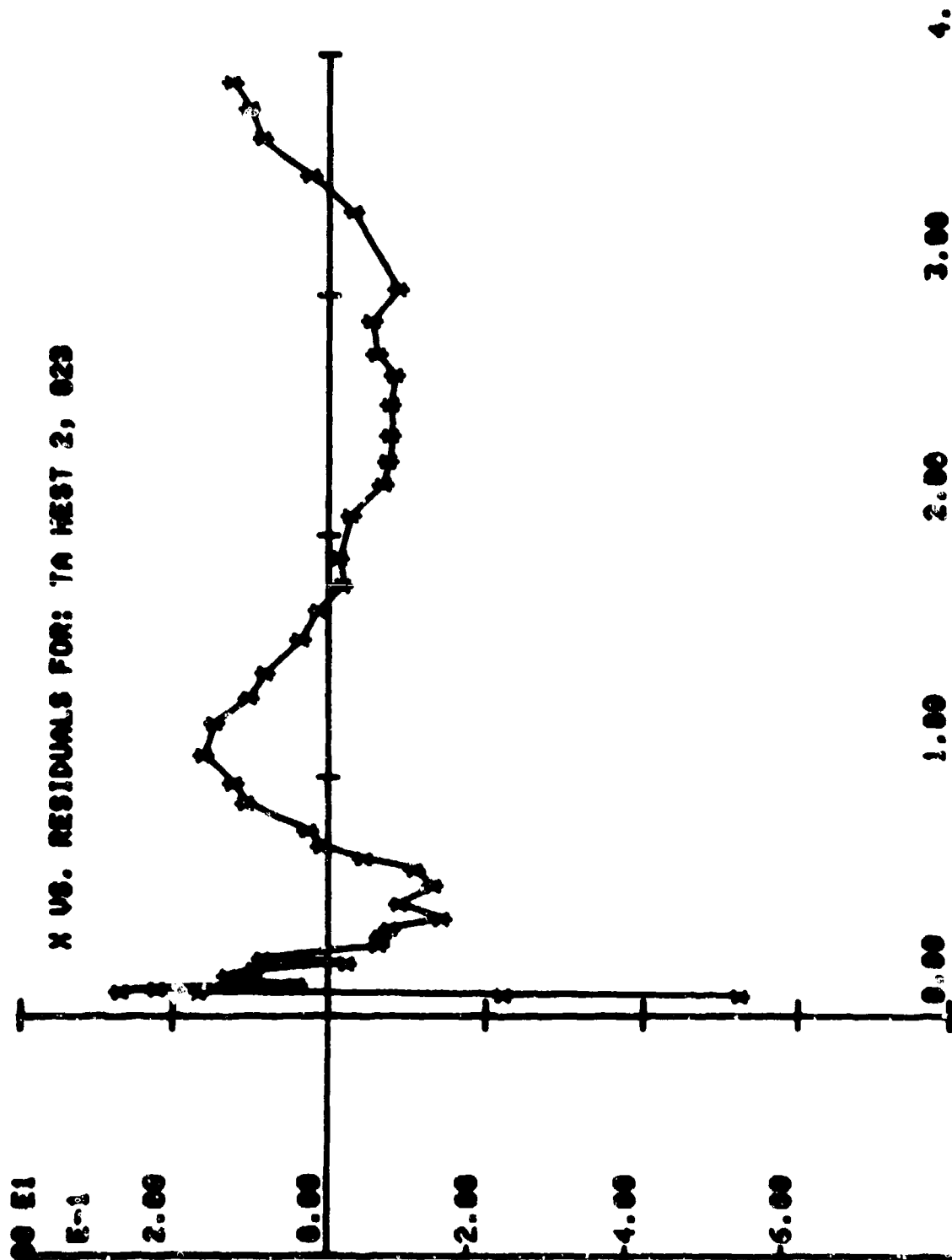
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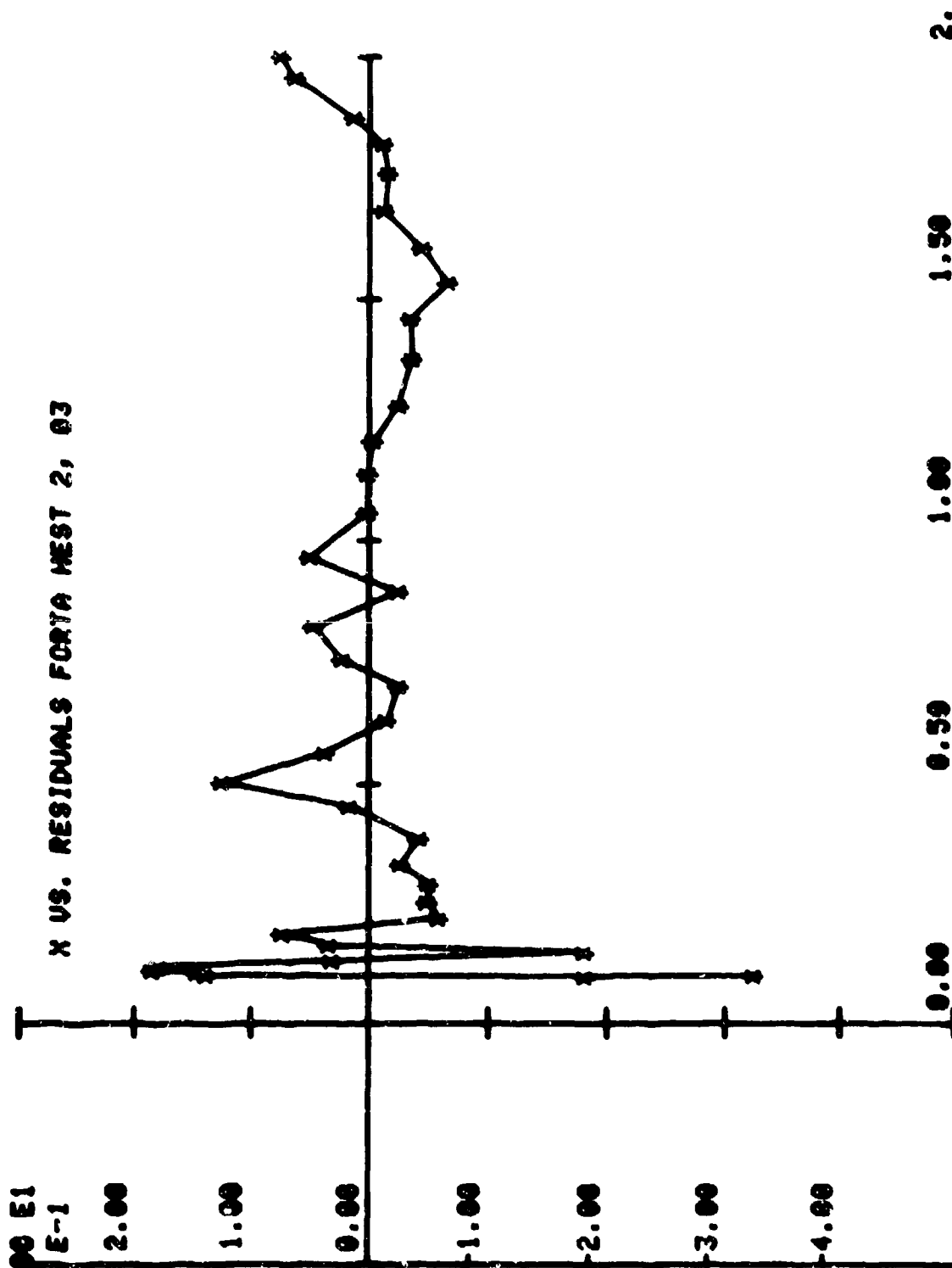


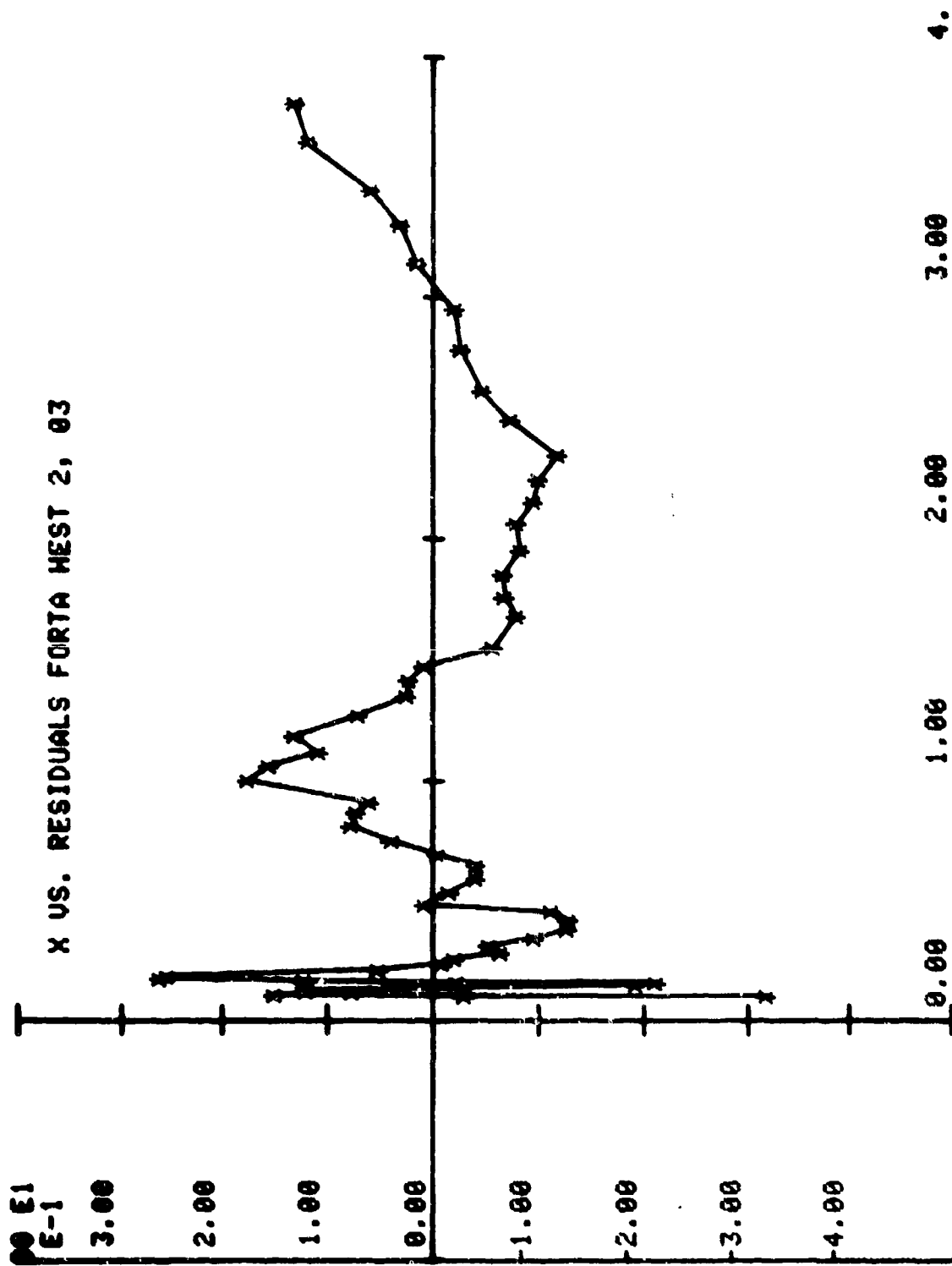
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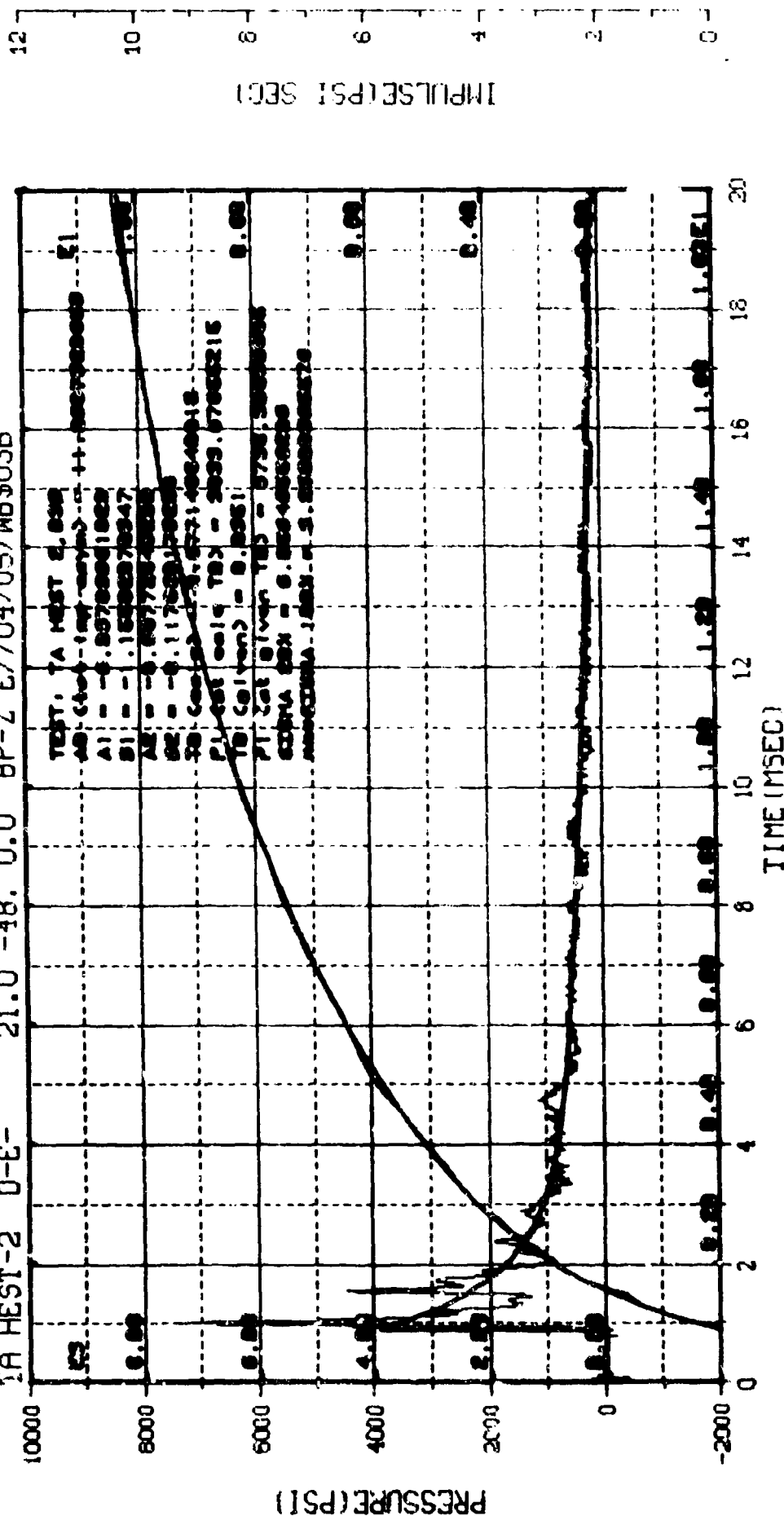
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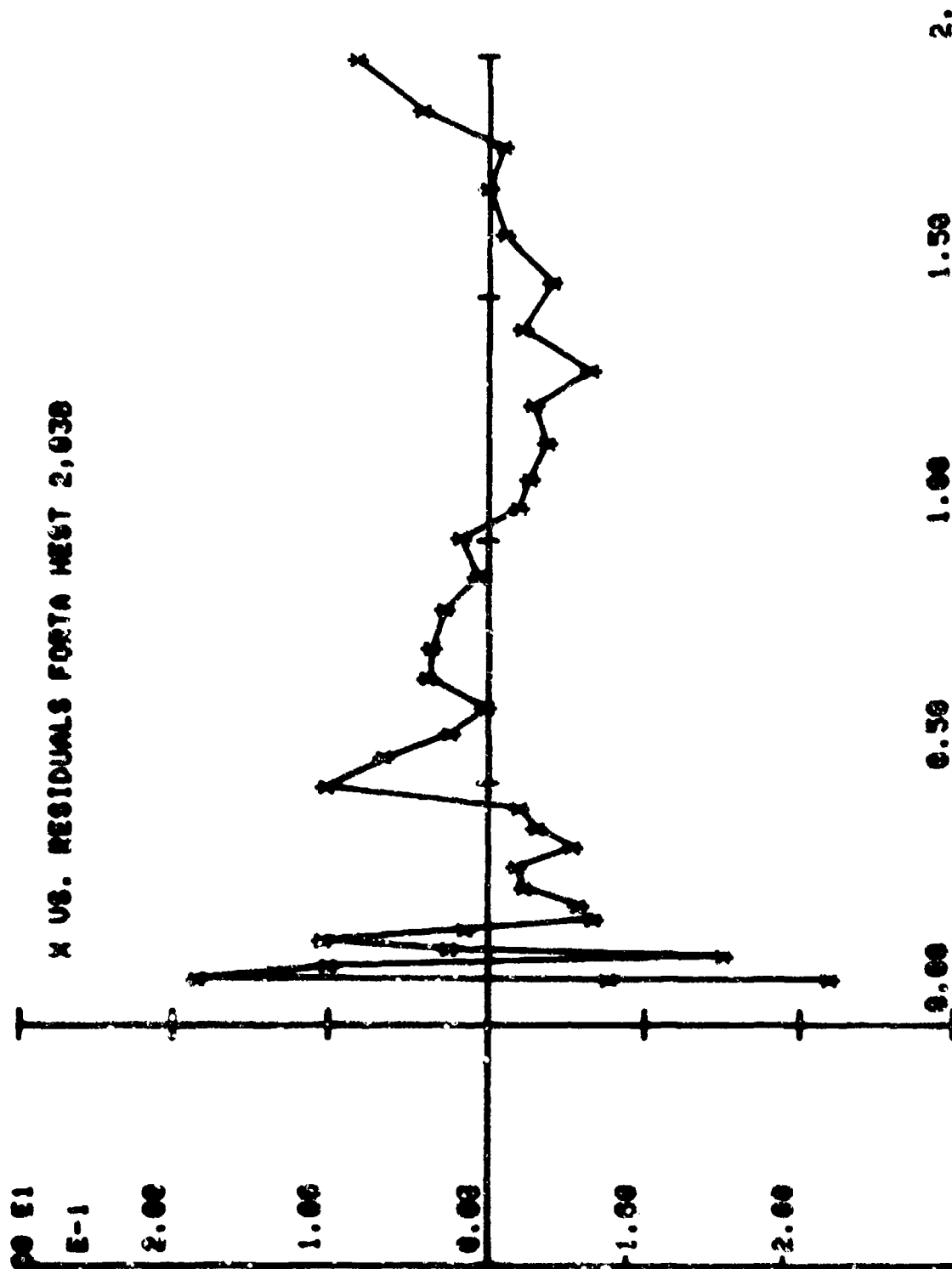


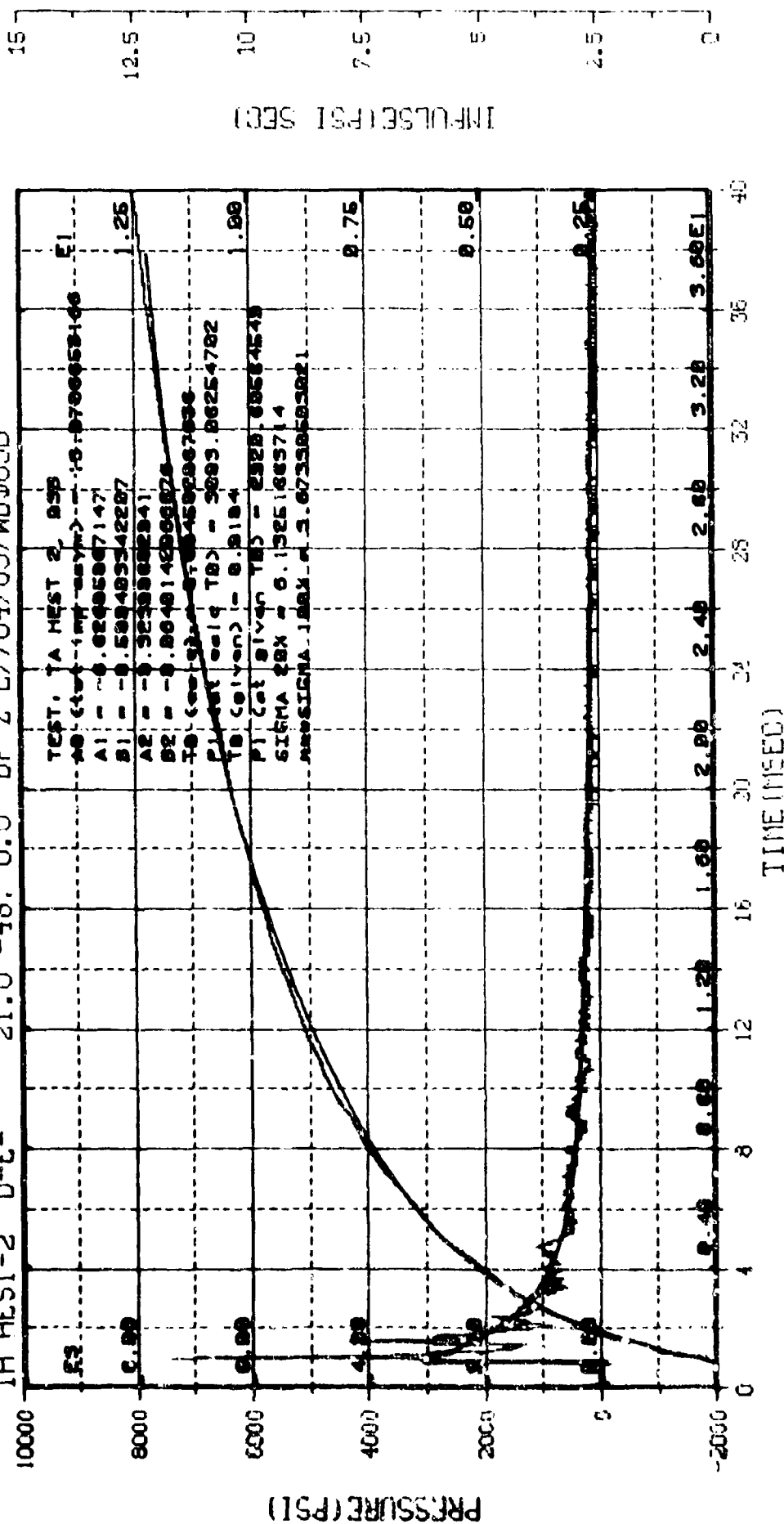


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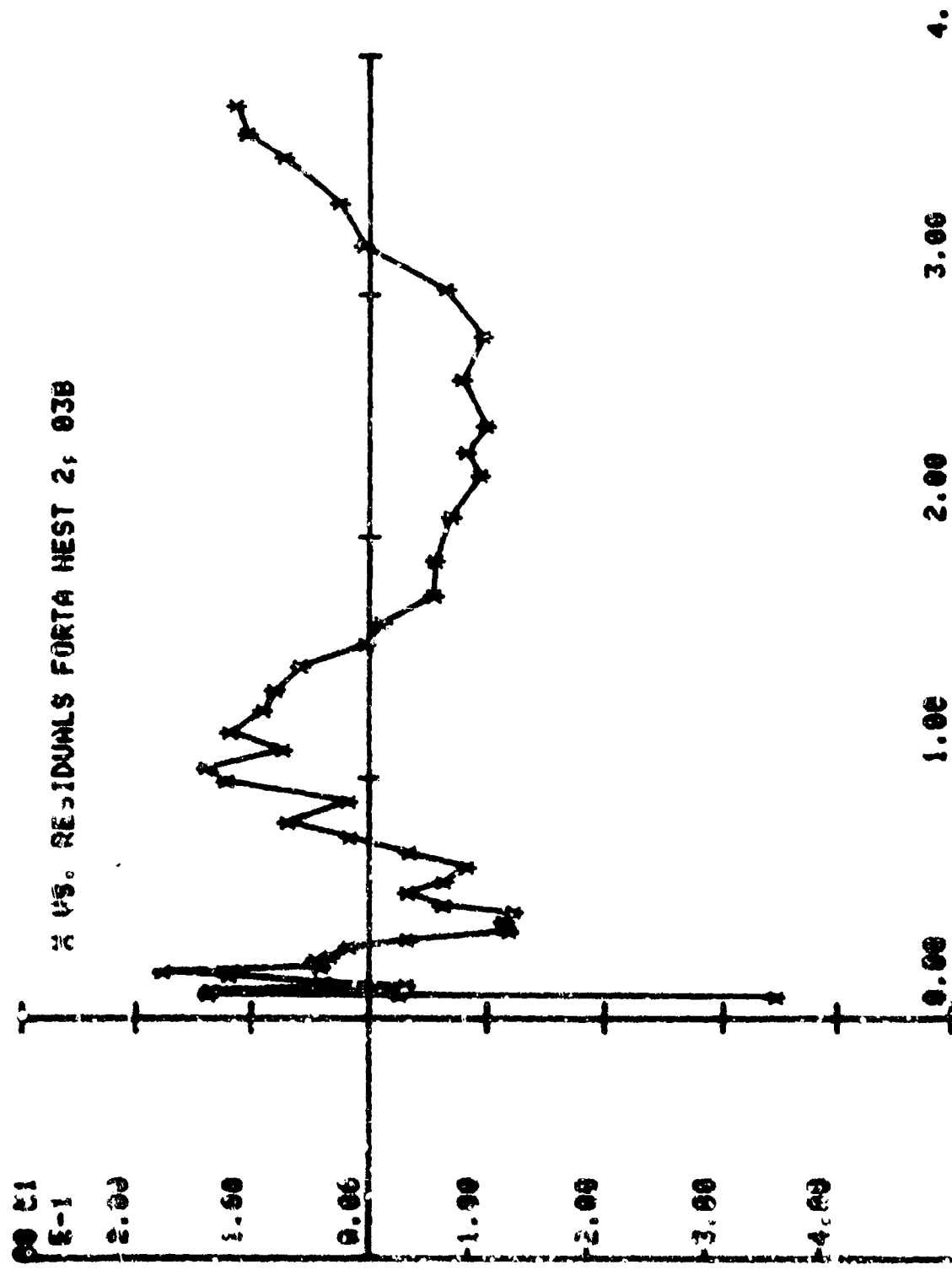


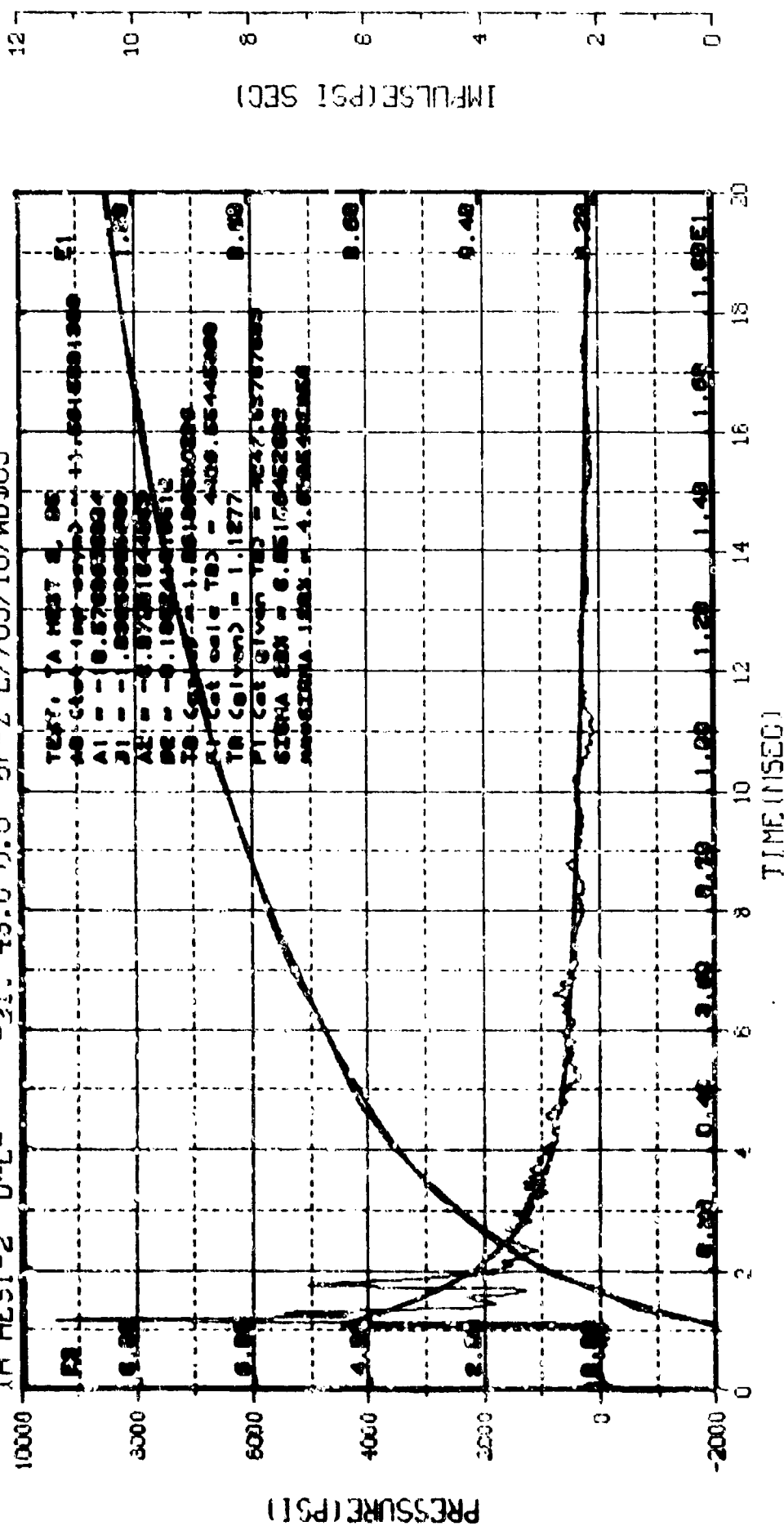
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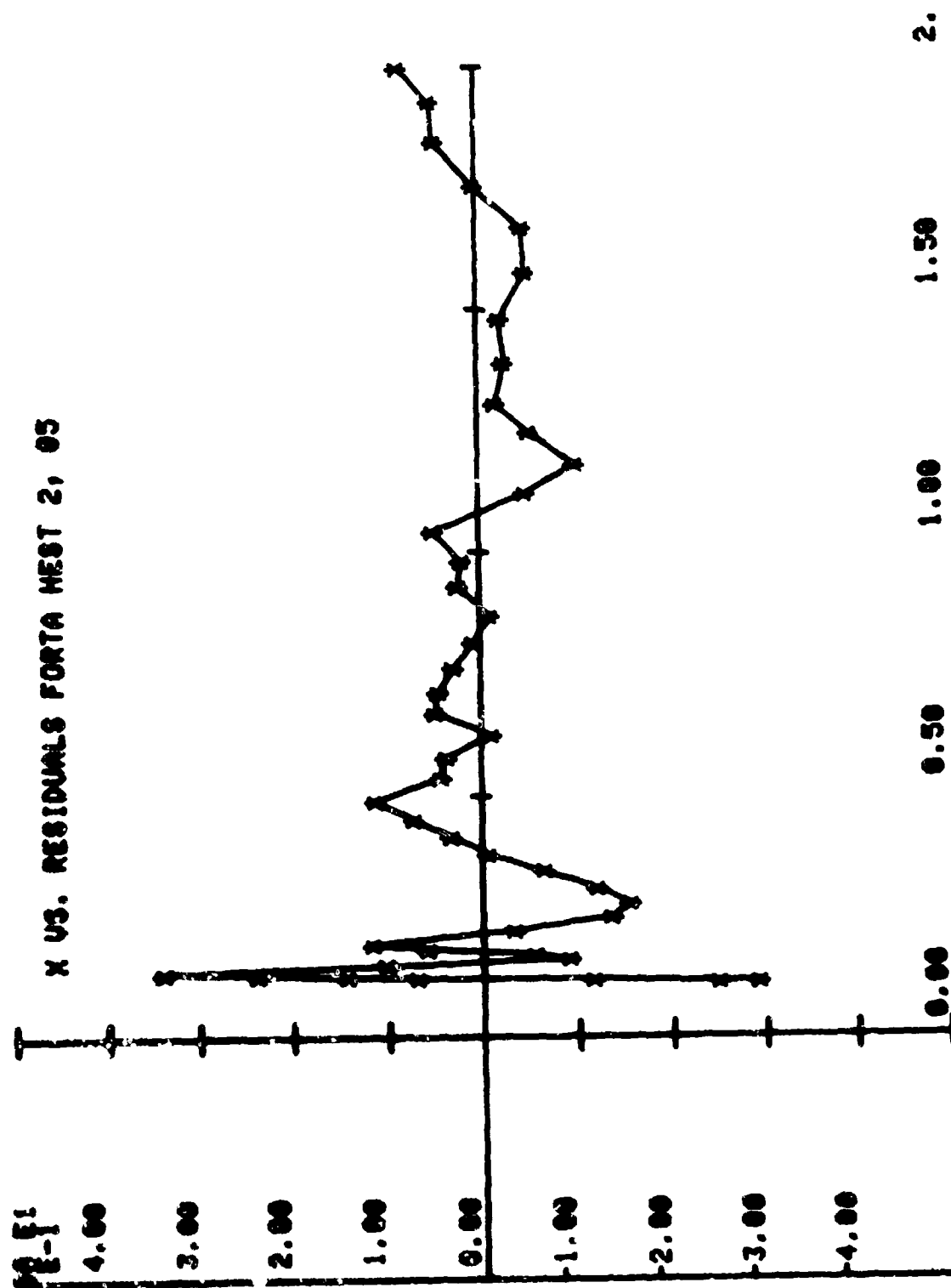


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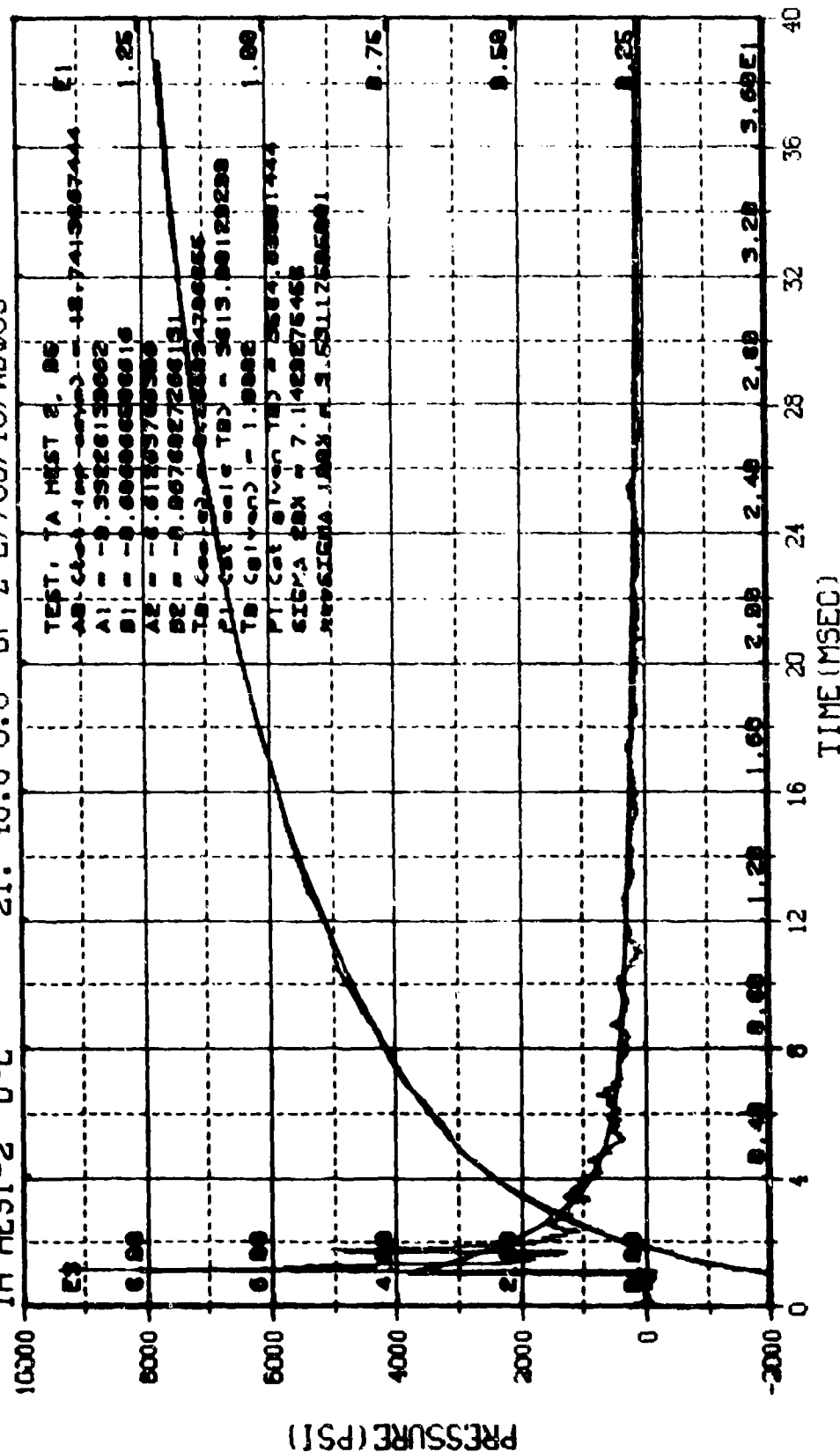




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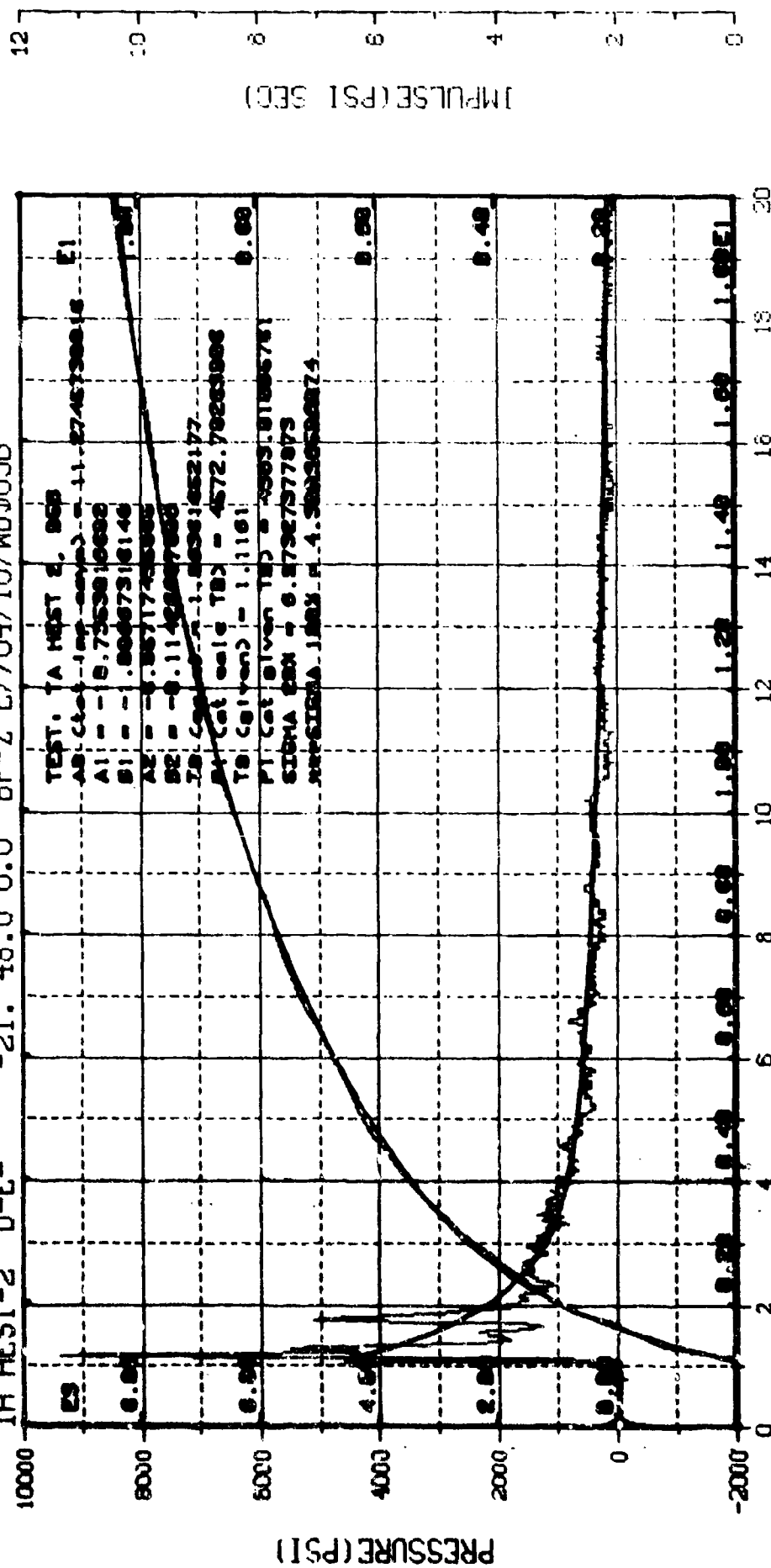


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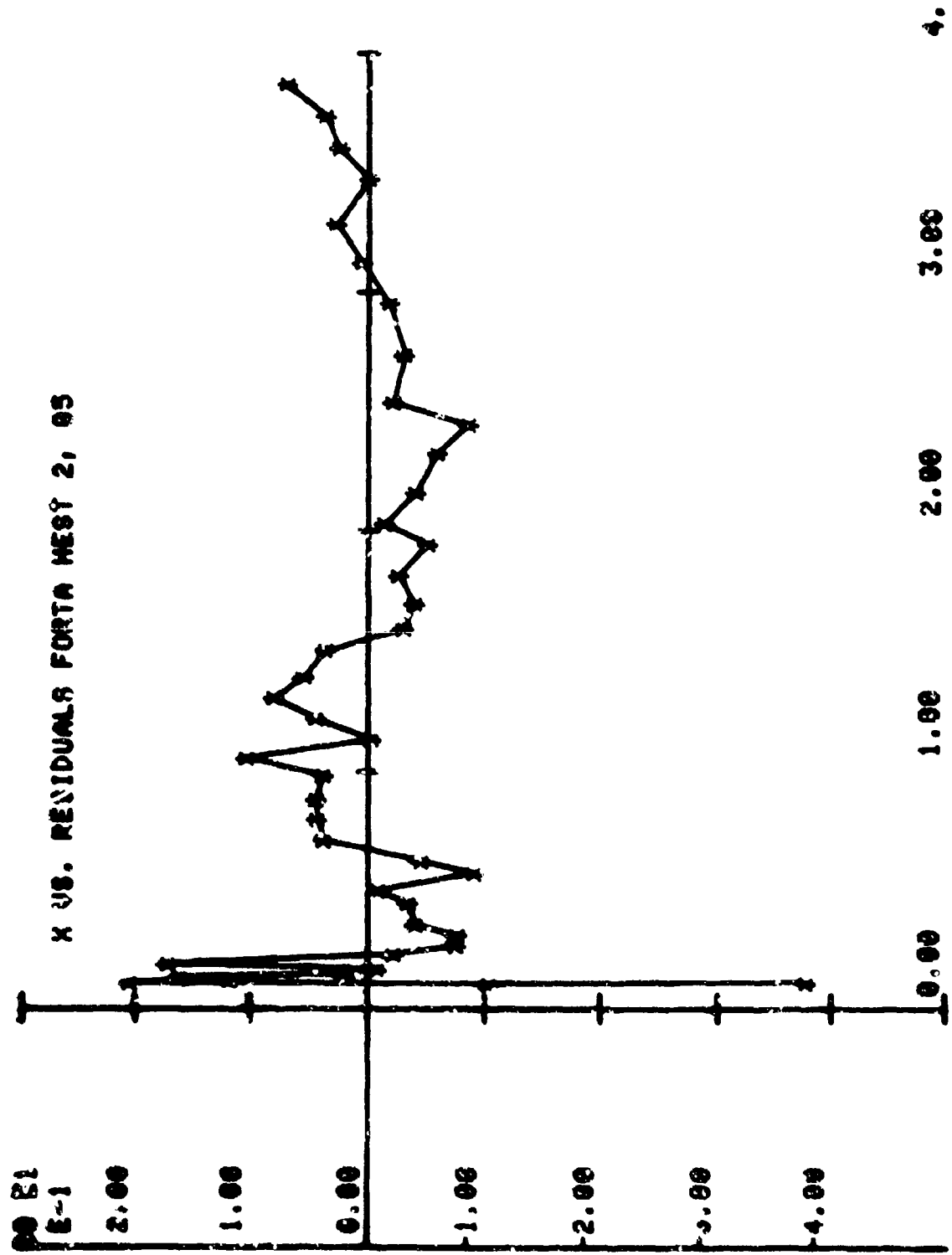


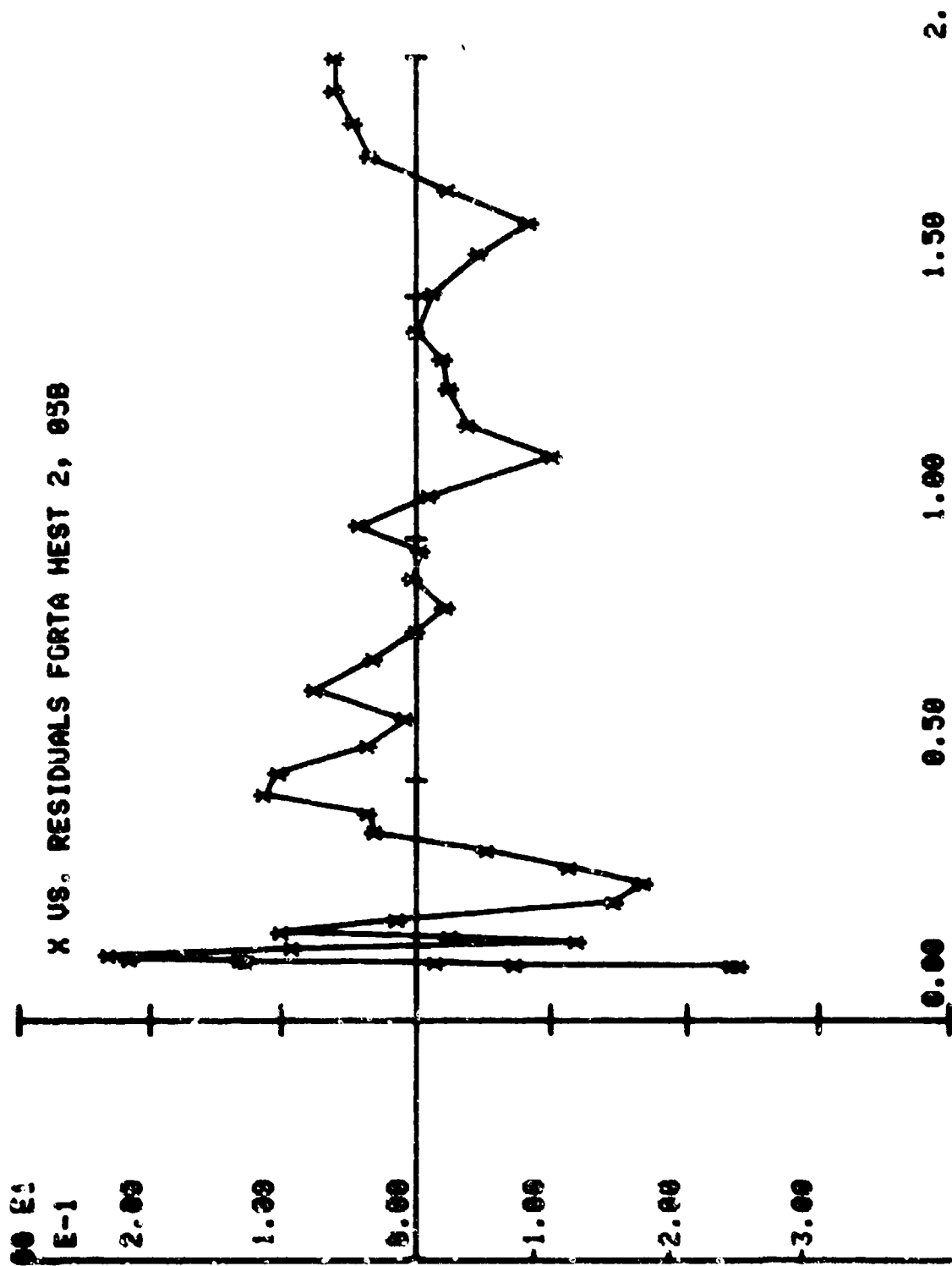
M.N. = 5 E.U. = 0.000, 5371.600 VSN=
 TSKIP=15.100 DIGITS=0.000, 722.500 TAPE22
 S.R. = 100.00 KHZ 10 04 PM, 28 MAR 78. FILE=48

TA HEST-2 D-E- -21. 48.0 0.0 BP-Z E7/04/10/WB\$05B

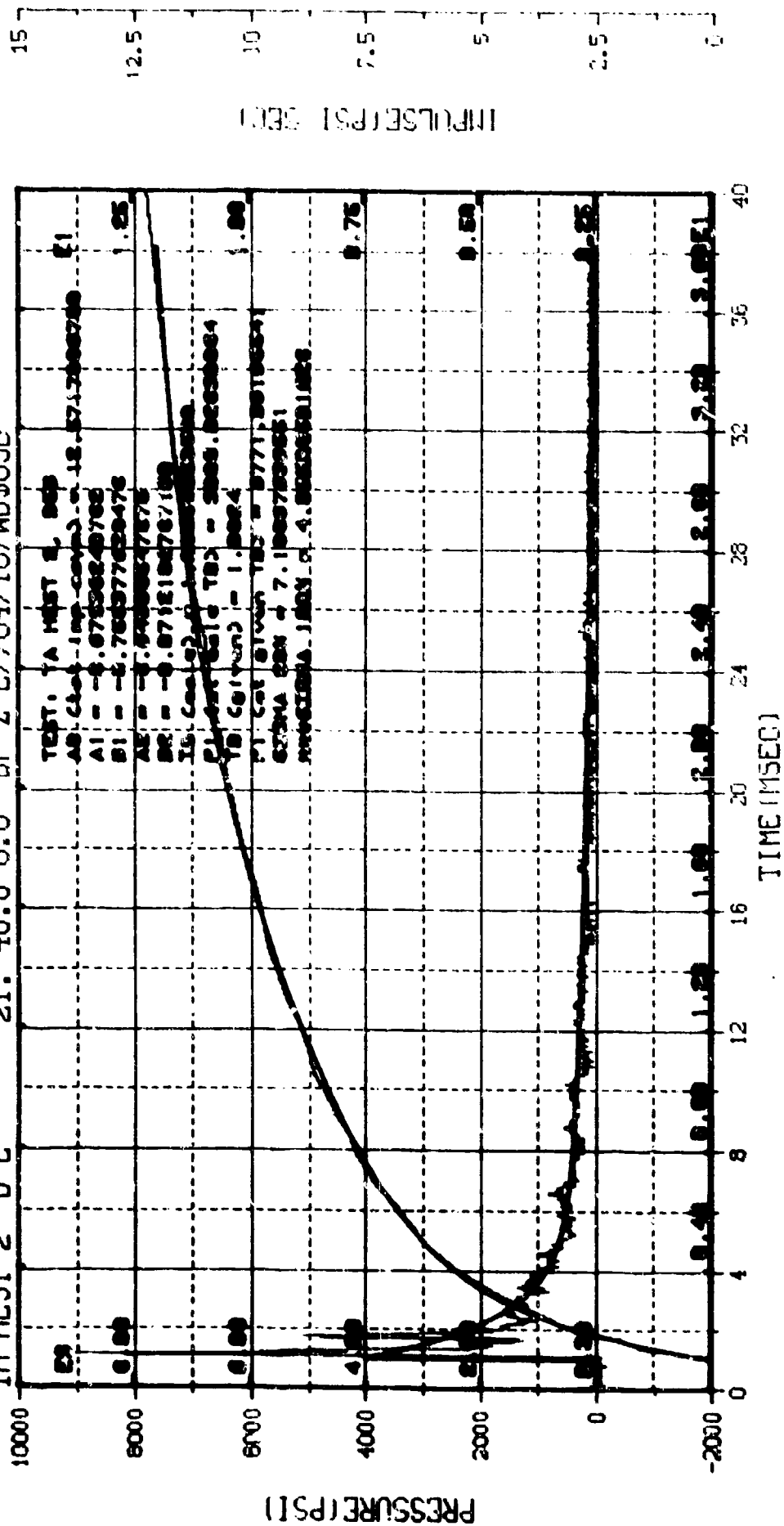


M.N. = 5 E.U. = 0.000, 5371.600 VSN=
 TSKIP=15.110 DIGITS=0.000, 200.000 TAPE22
 S.R. = 100.00 KHZ 9 00 AM, 29 MAR 78. FILE=64

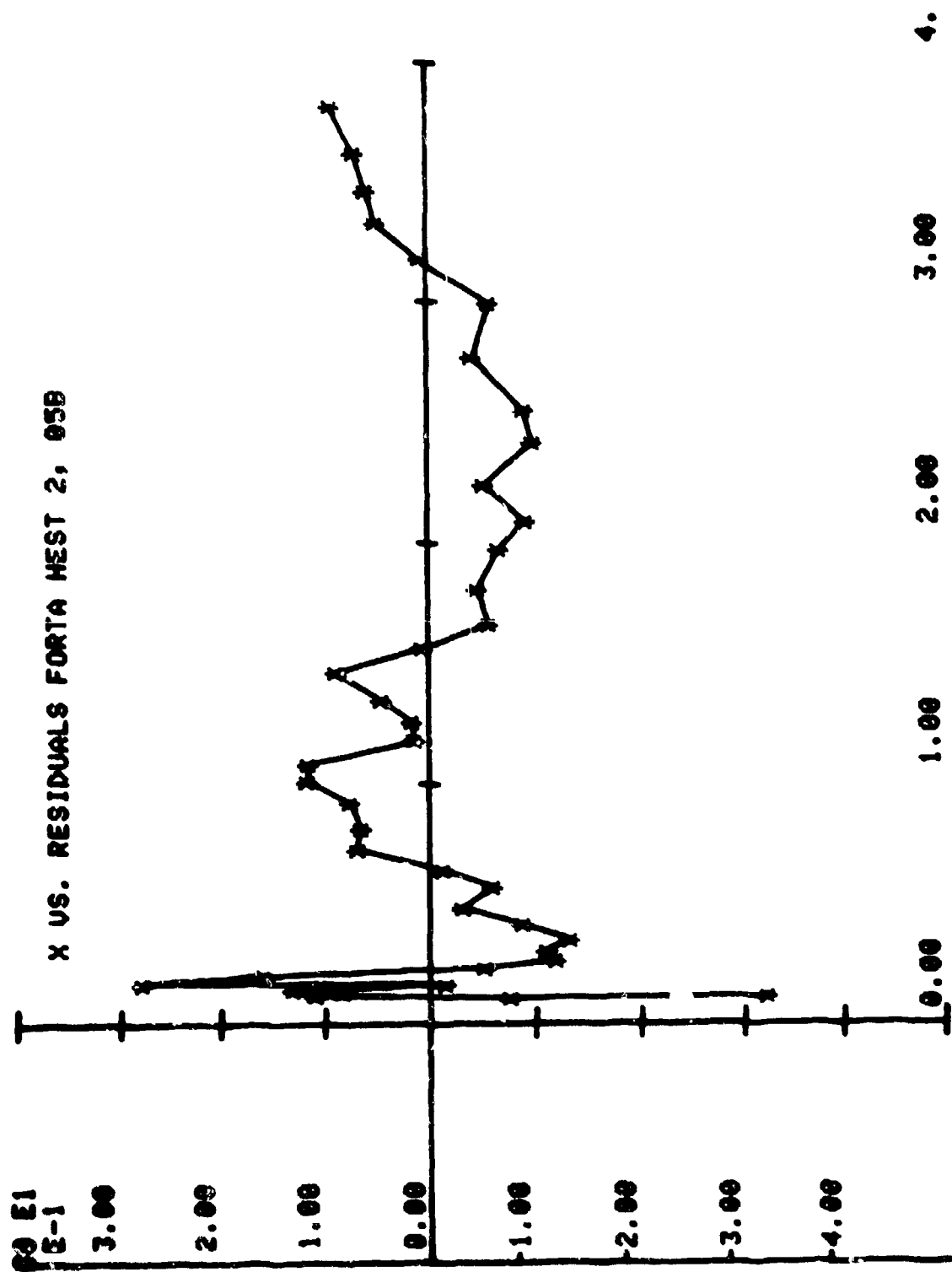


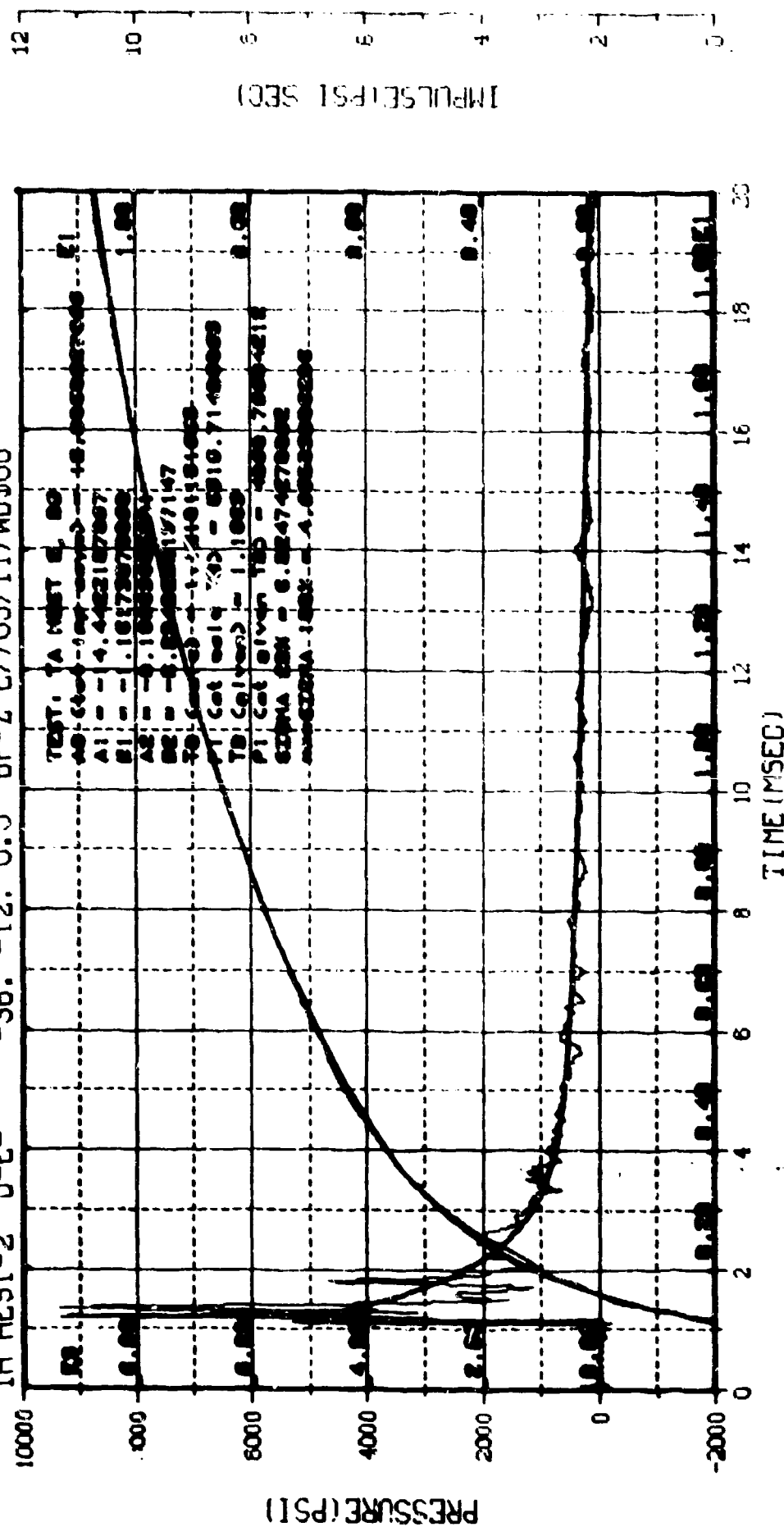


TA HEST-2 0-E-- -21. 48.0 0.0 BP-Z E7/04/10/WB\$05E



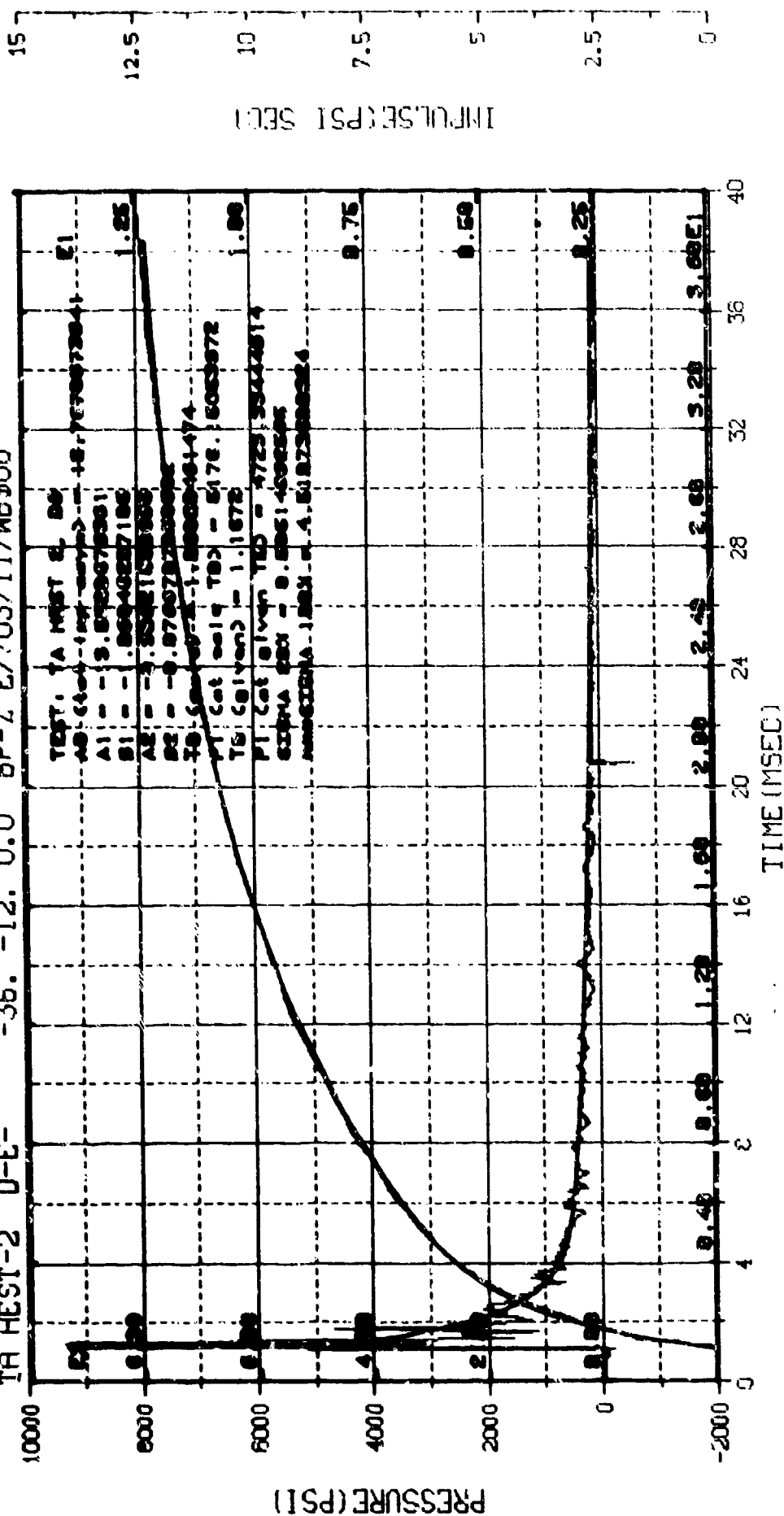
M.N. = 5 E.U. = -0.000, 5371.600 VSN =
 TSKIP = 15.110 DIGITS = 0.000, 206.000 TAPE 22
 S.R. = 100.00 KHZ 10 04 PM, 28 MAR 76. FILE = 64



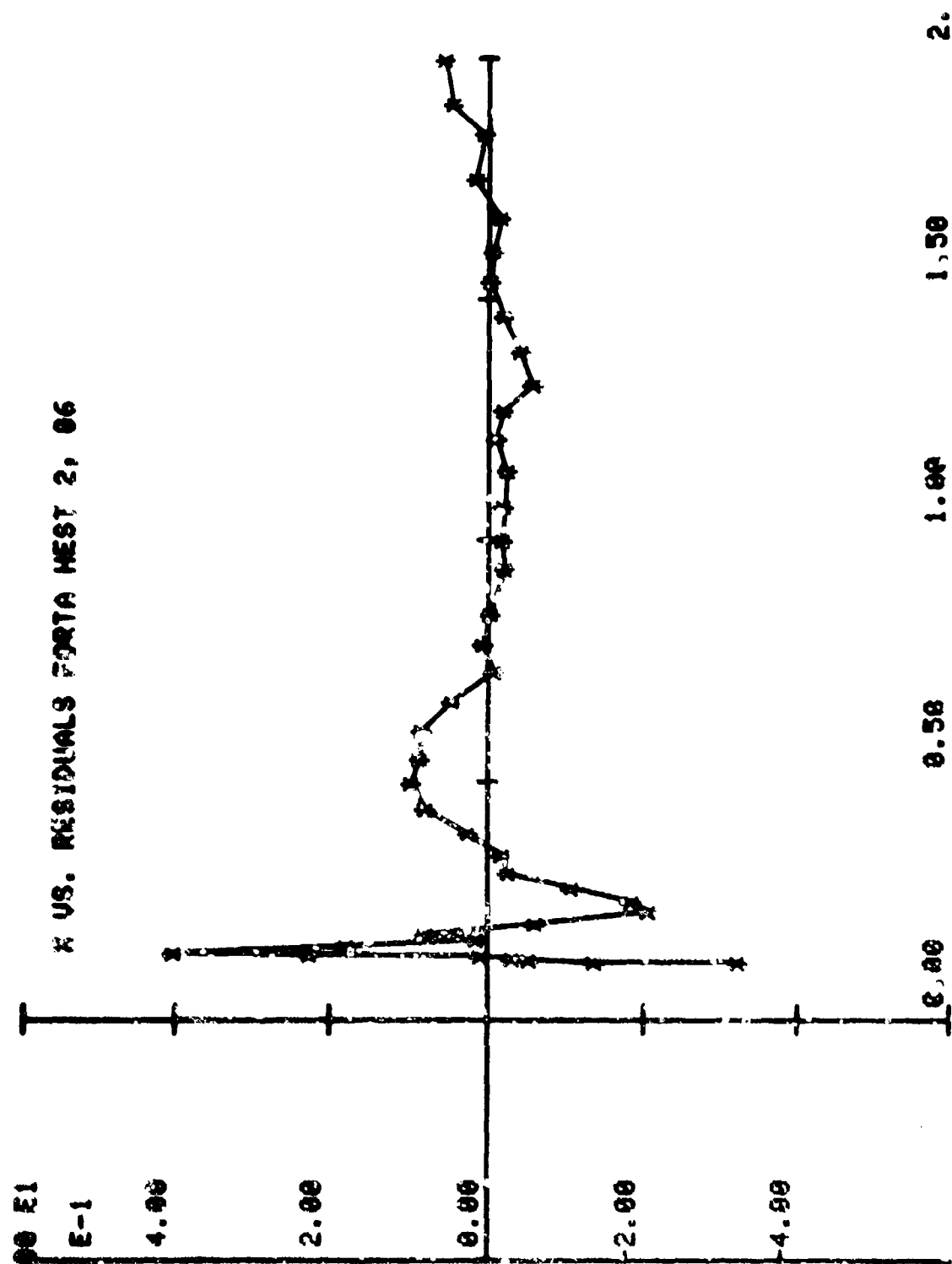


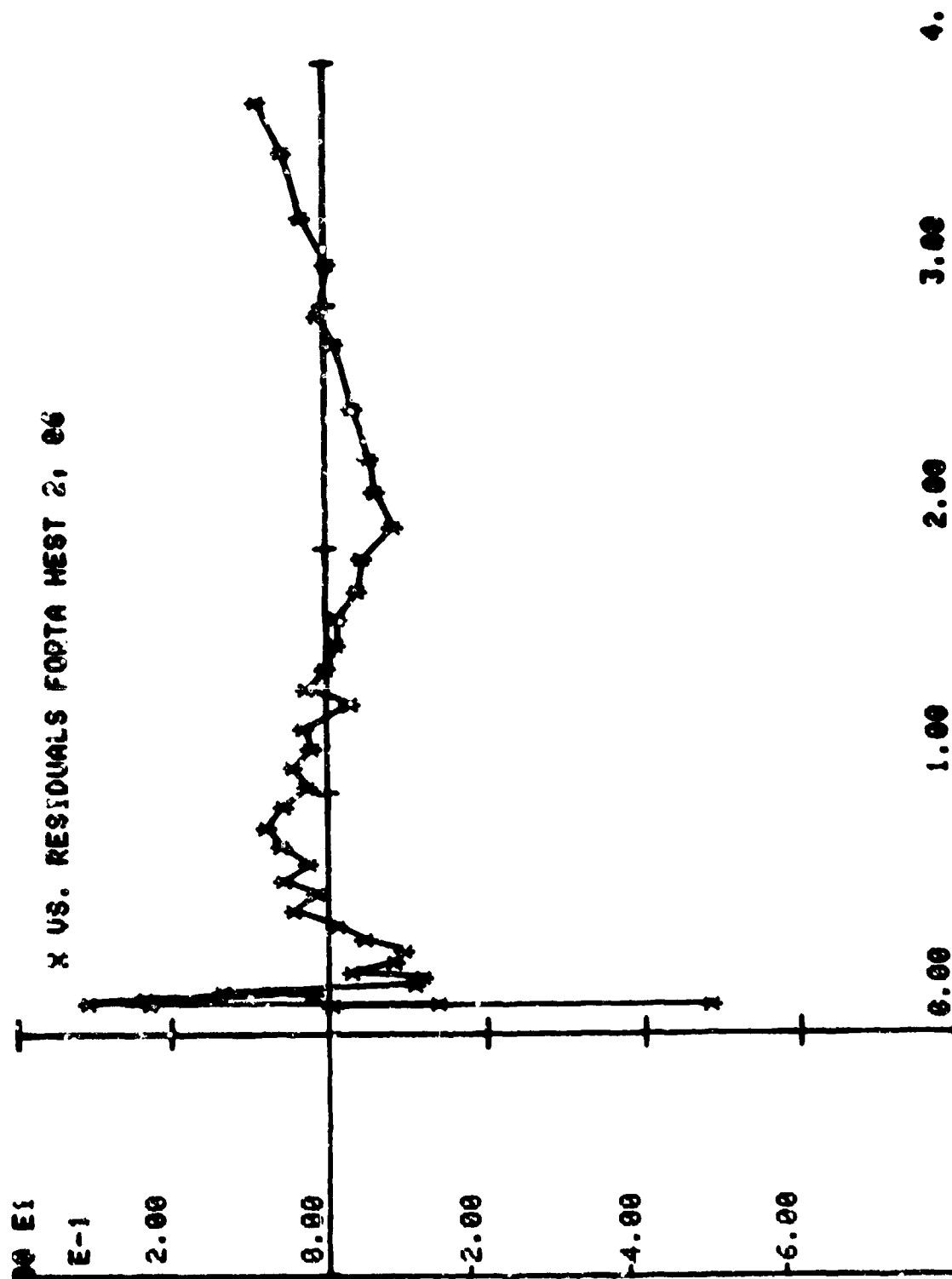
M.N. -	5	E.U. -	0.000, 5416.600	VSN-
TSKIP-	15,100	DIGITS-	0.000, 966.500	TAPE22
S.R. -	100.00 KHZ		10 04 PM, 28 MAR 76.	FILE-50

TA HEST-2 D-E- -36. -12. 0.0 8P-Z E7/03/11/WB\$06

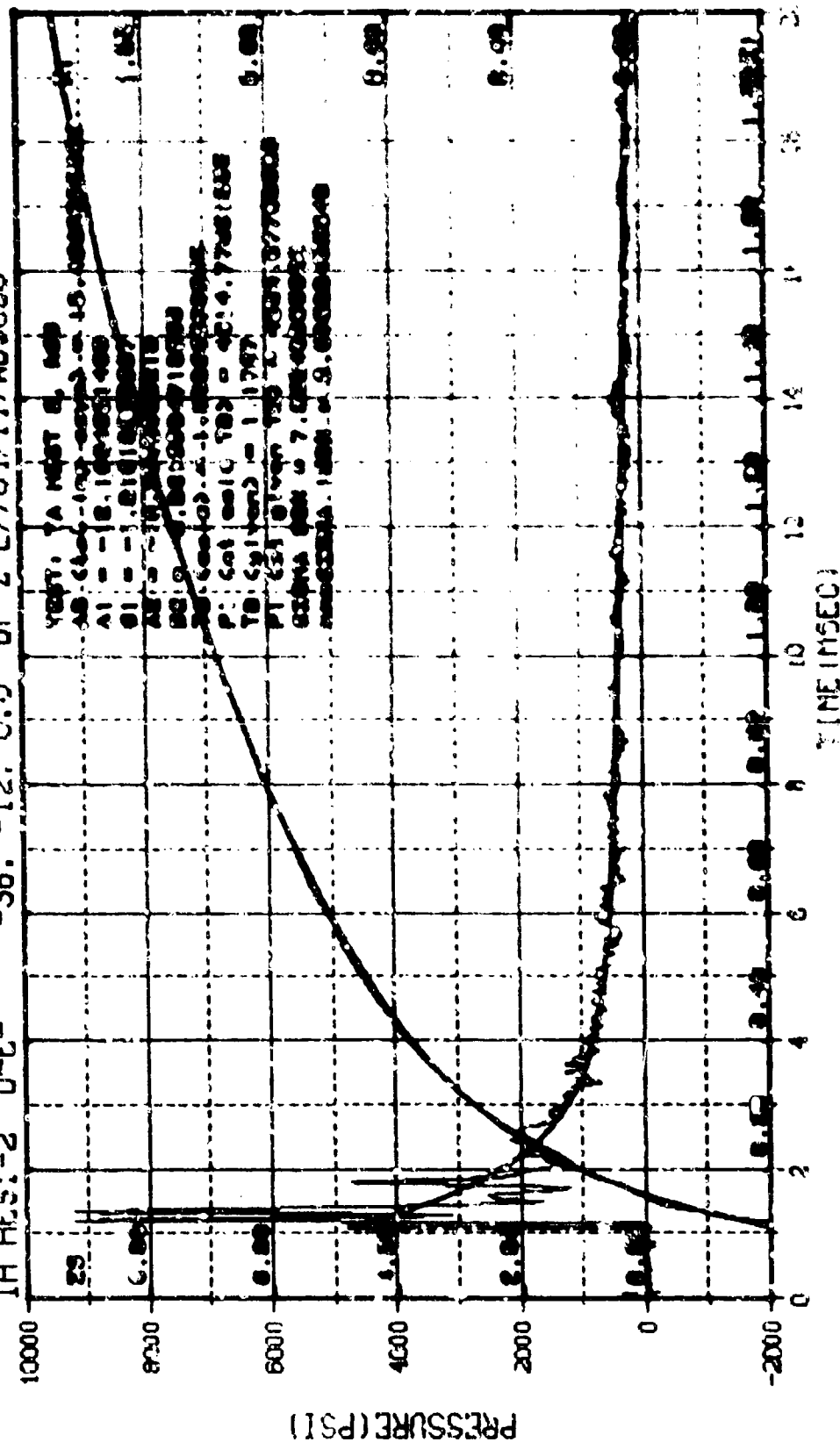


M.N. = 6 E.U. = 0.000, 5416.600 VSN=
 TSKIP=15.100 DIGITS=0.000, 966.500 TAPE22
 S.R. = 100.00 KHZ 10 04 PM, 28 MAR 78. FILE=50

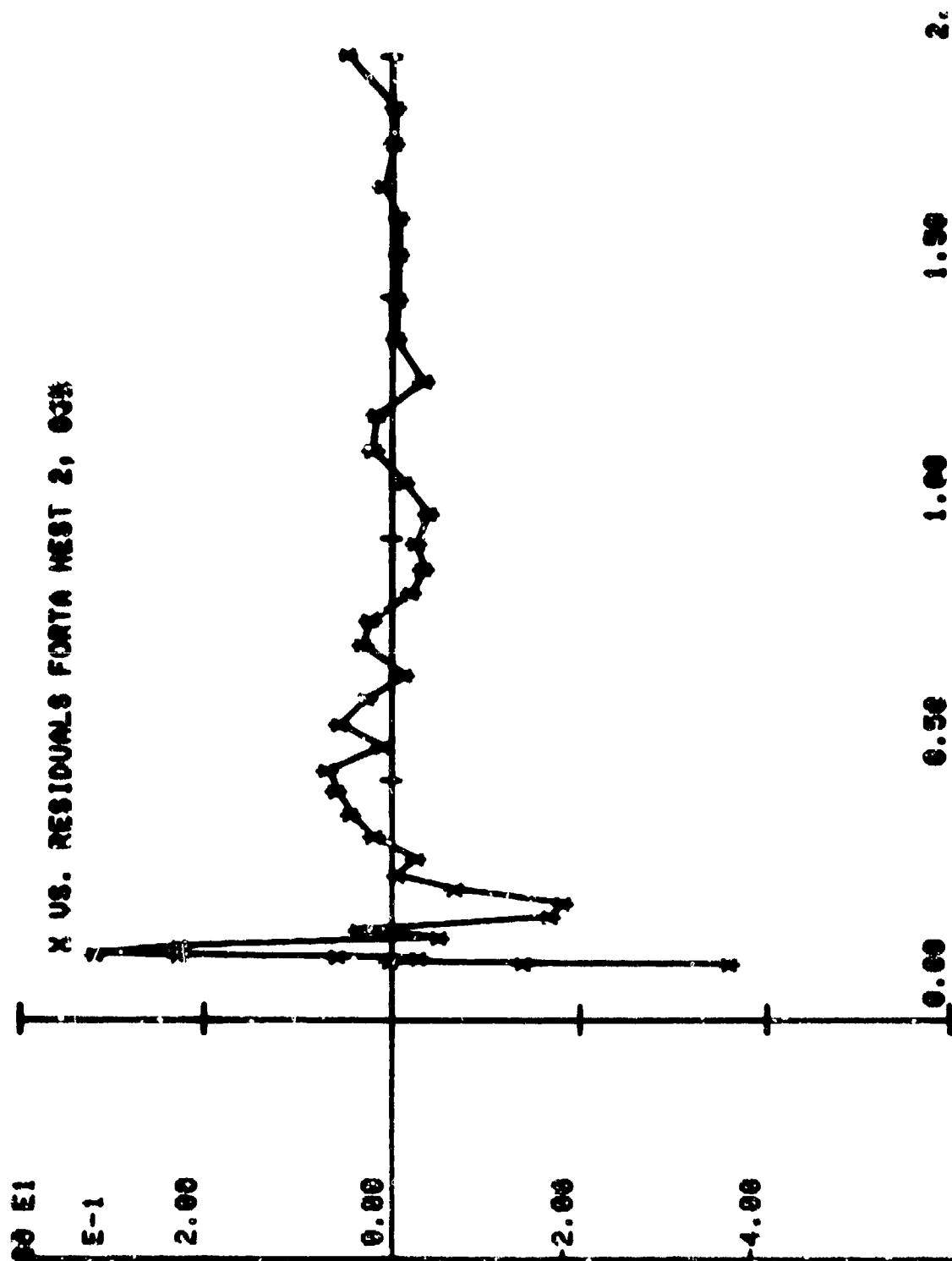


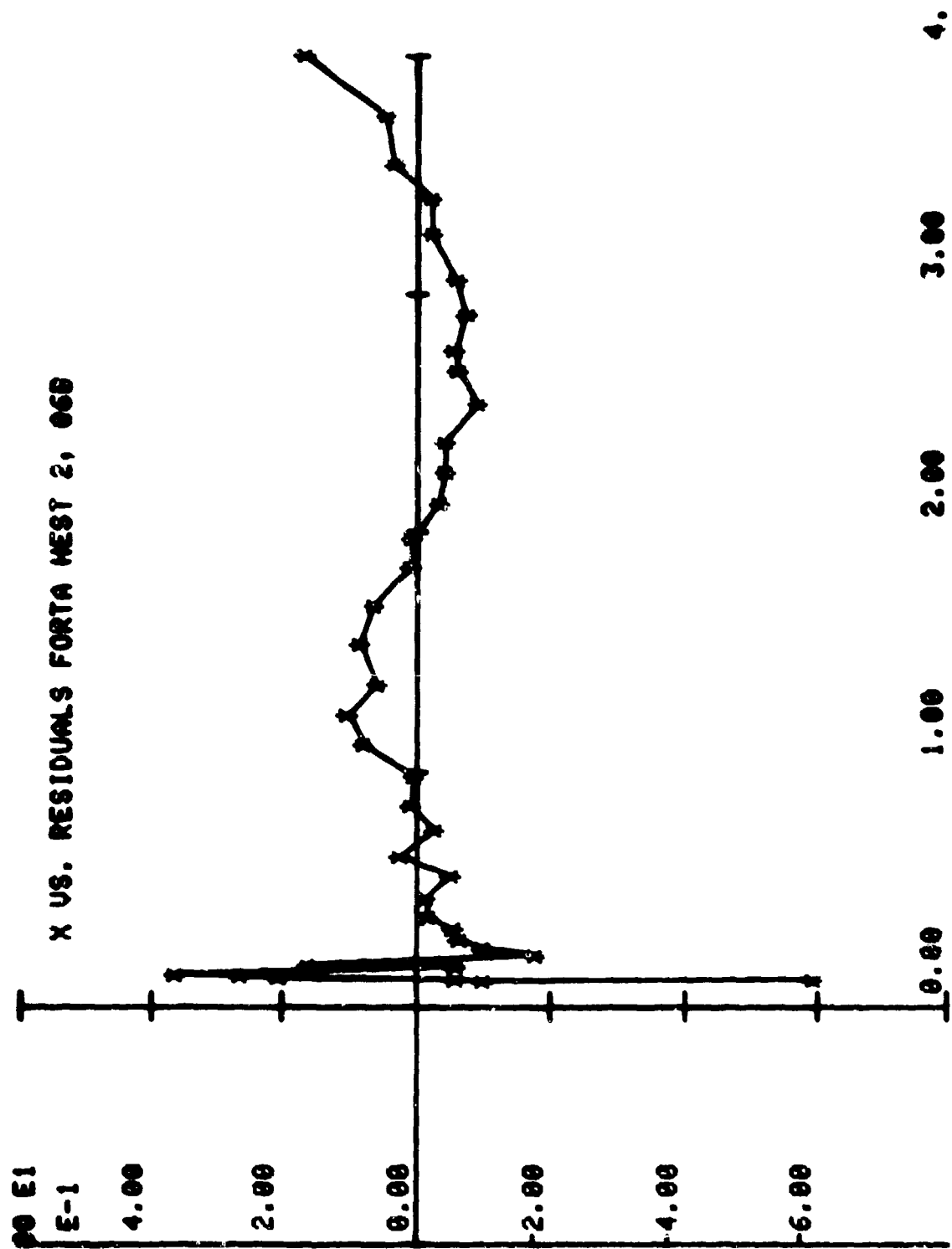


TA HEST-2 0-E- -36. -12. 0.0 BP-Z E7/04/11/WBSUS5

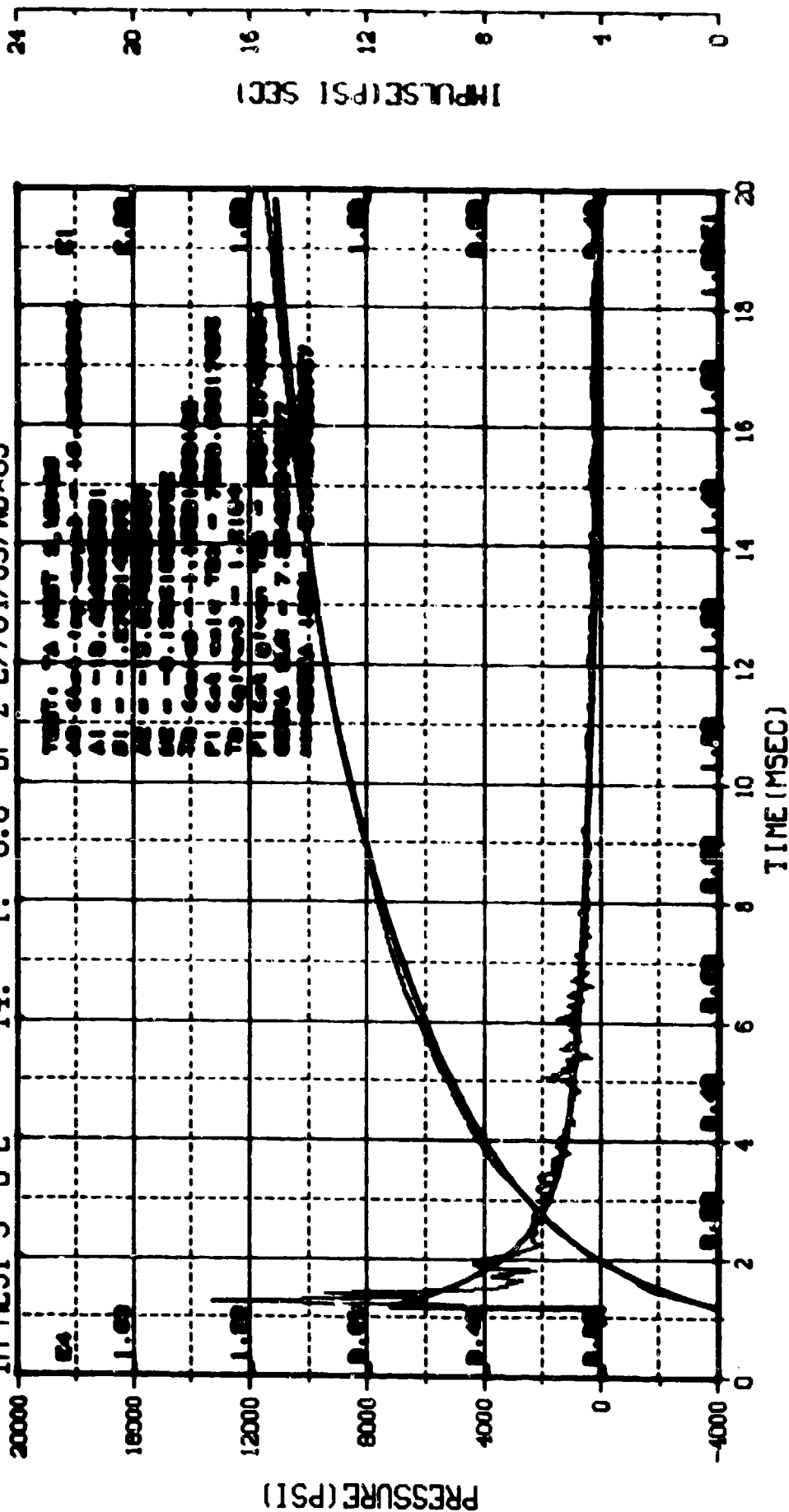


M.N. = 6 E.U. -0.000,5416,000 VEN
TSKIP=15.110 DIGITS=0.000,392,500 TIME=2
S.R. =100.00 KHZ 9 00 AM, 29 MAR 70. FILE=16

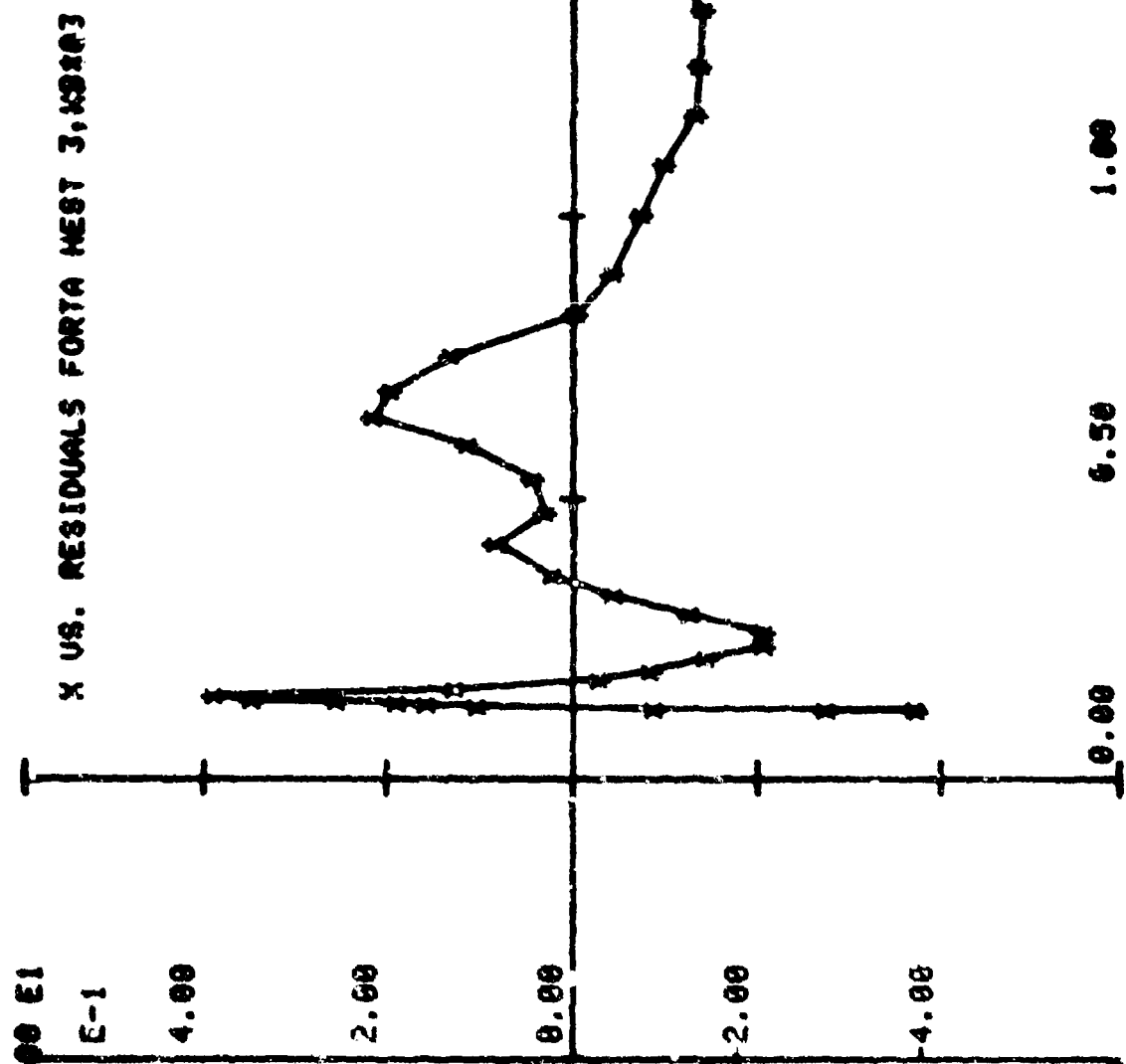




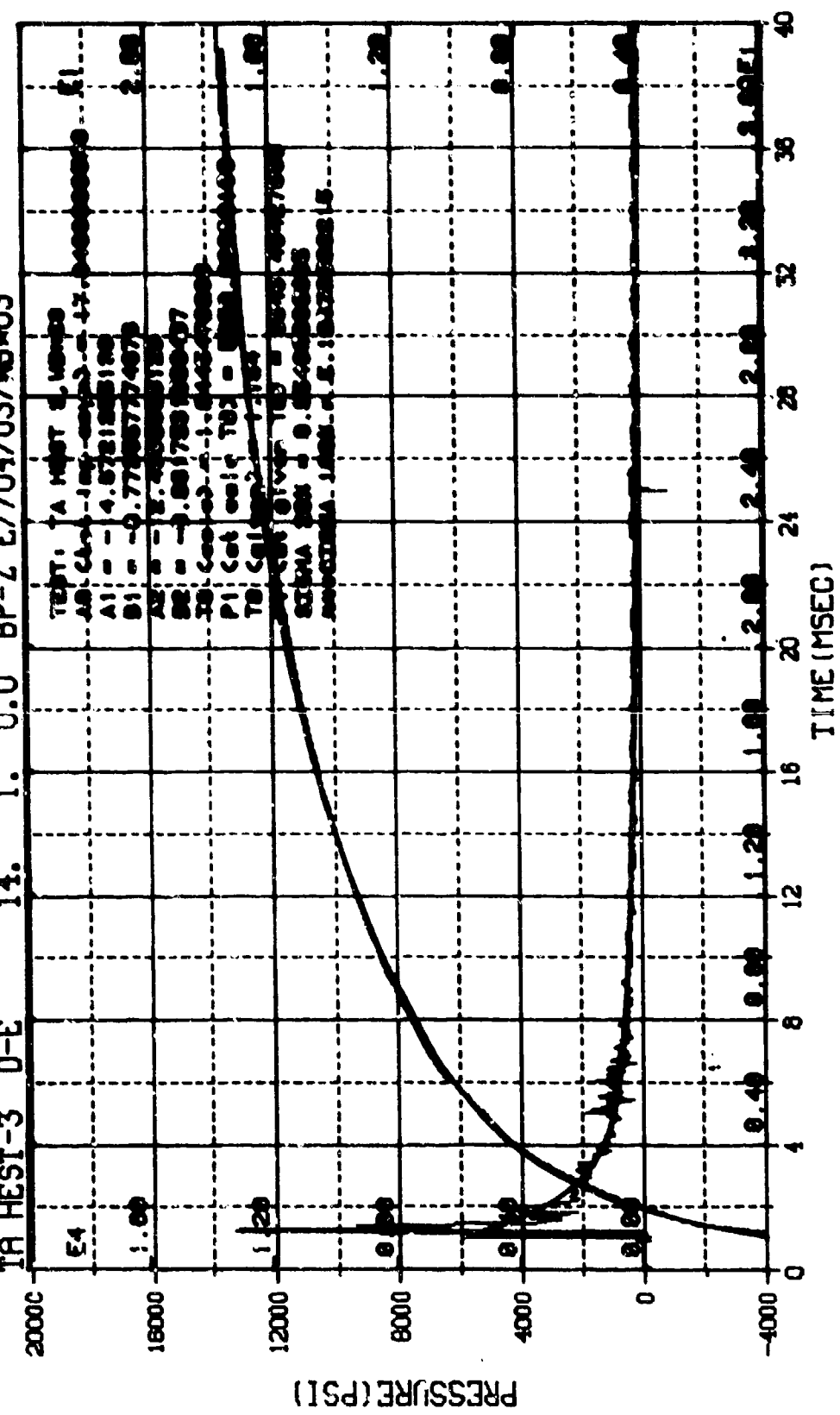
IA HEST-3 D-E 14. 1. 0.0 BP-Z E7/04/03/WB#03



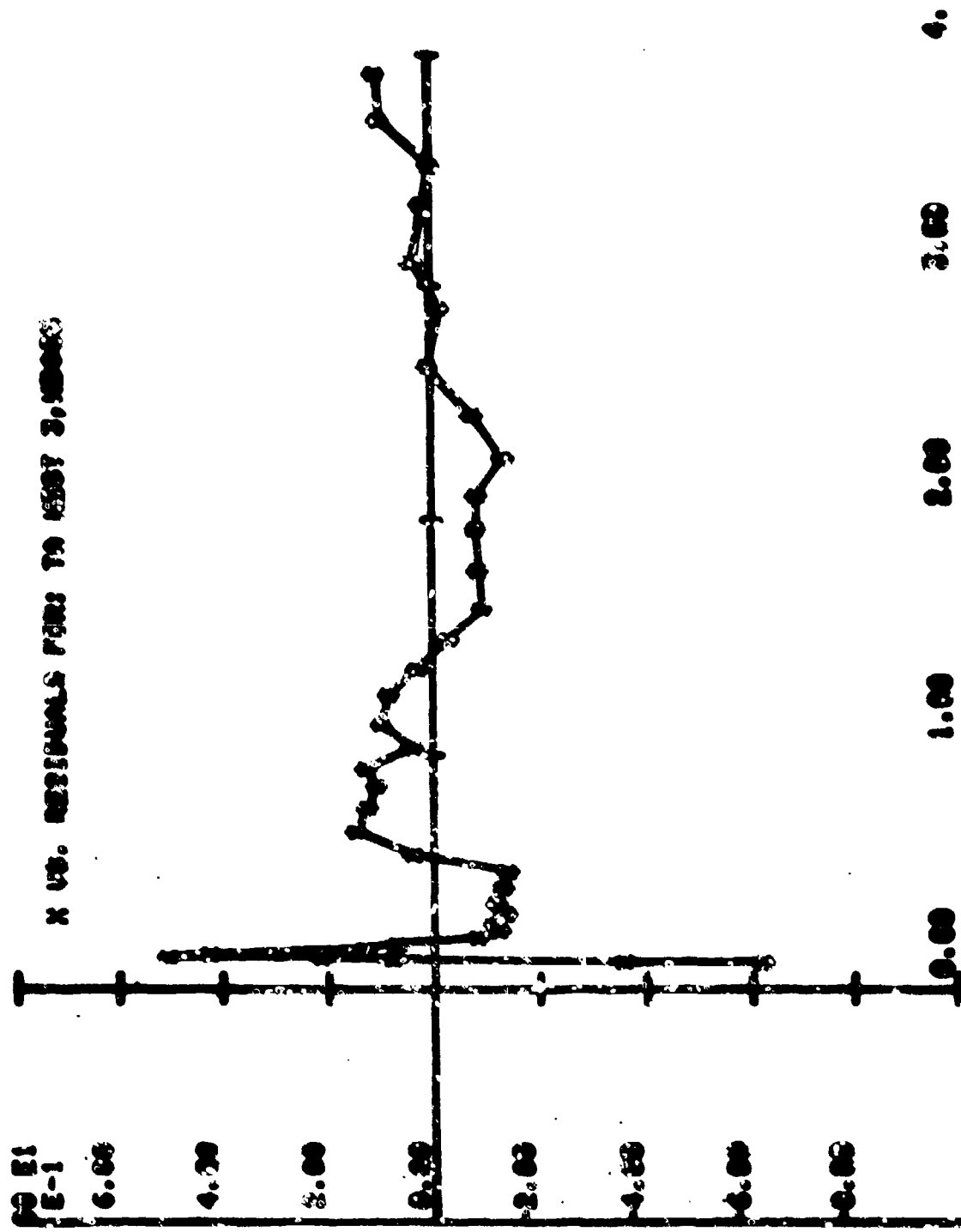
M.N. = 3 E.U. = -0.000,7820.000 VSN= ED23
 TSKIP=12.650 DIGITS=0.000,746.875 TAP222
 S.R. =100.00 KHZ 11 36 AM, 2 MAY 78. FILE=36

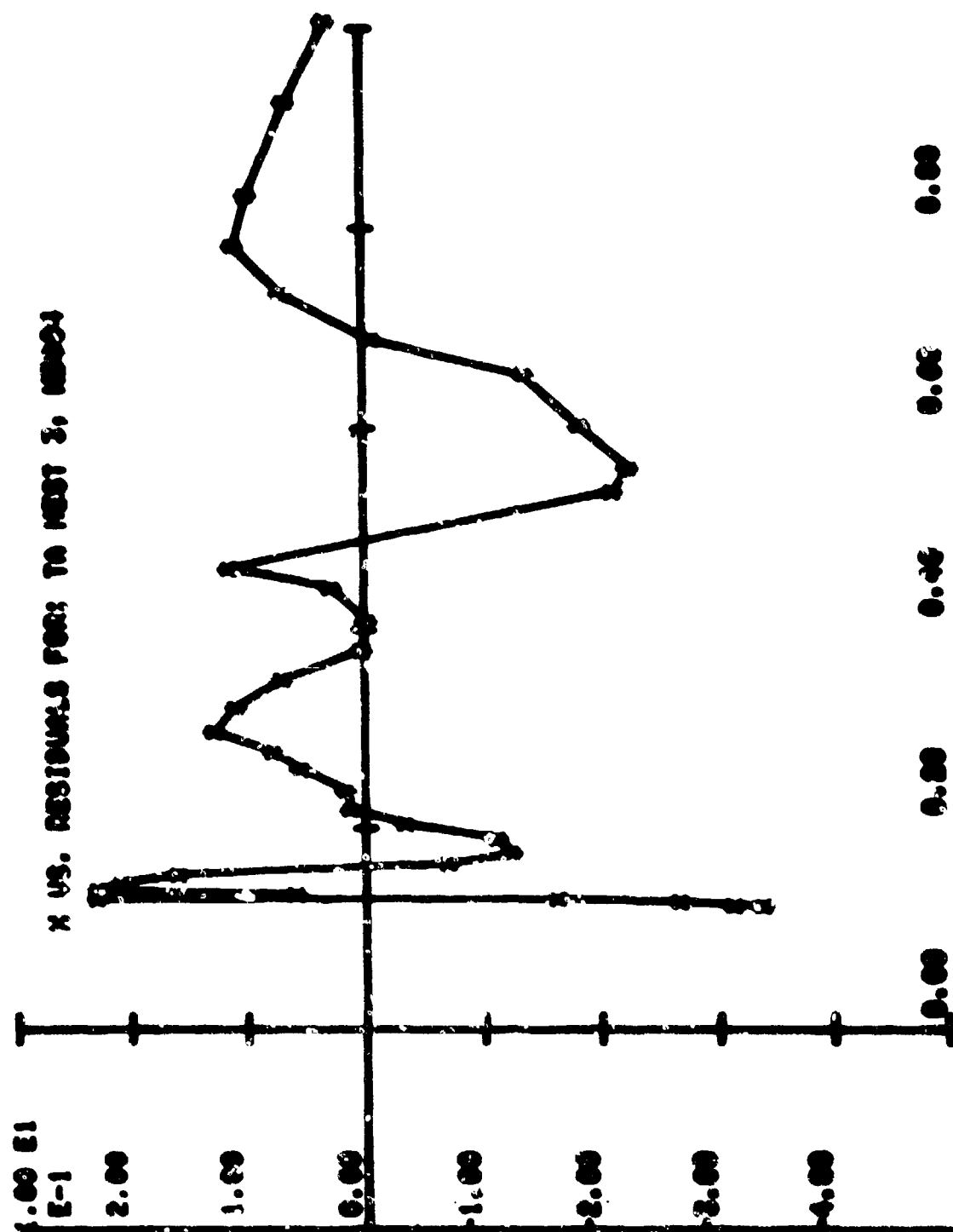


TA HEST-3 D-E 14. 1. 0.0 BP-Z E7/04/03/48#03

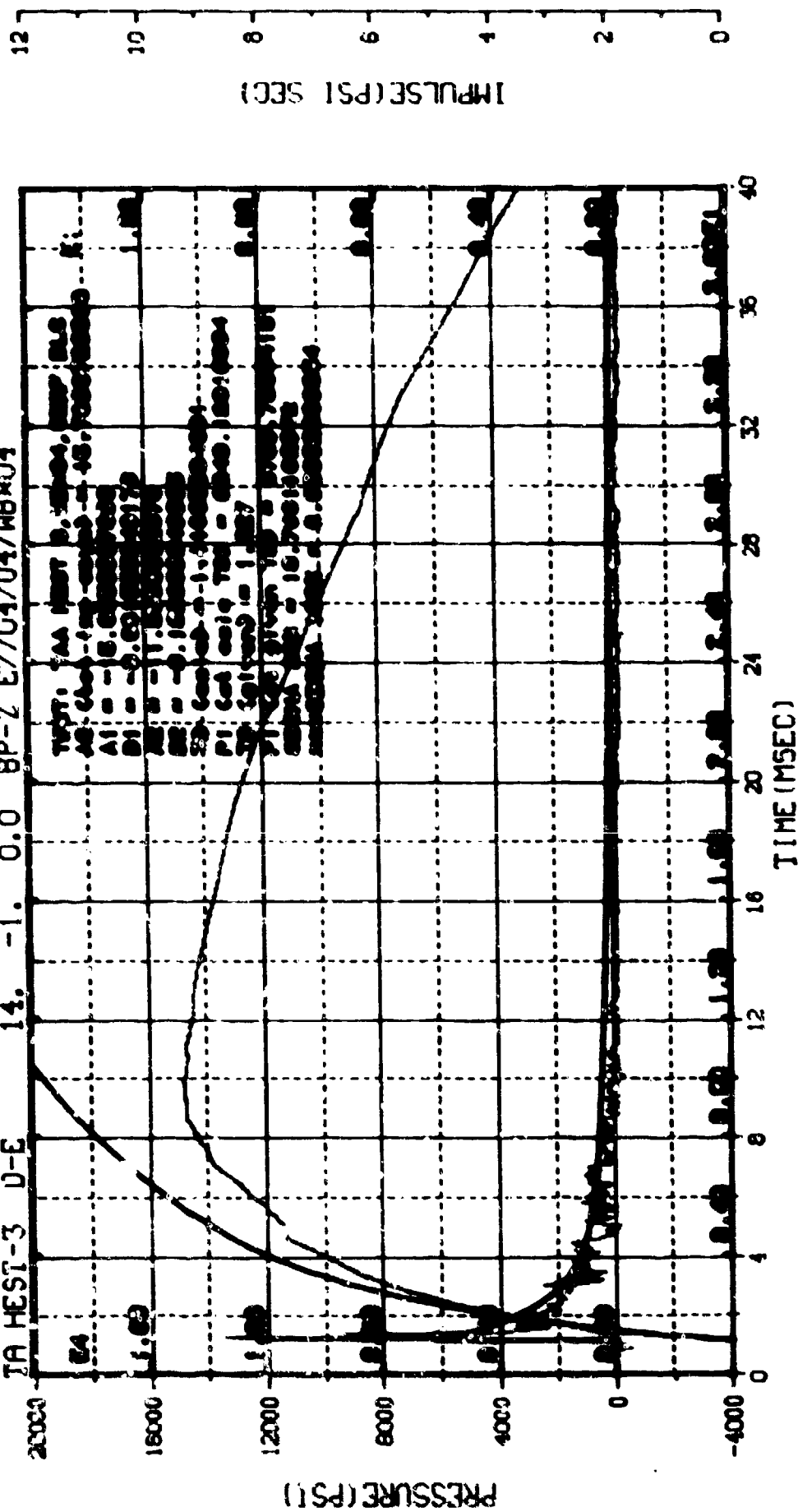


M.N. = 3 E.U. -0.000,7820.000 VSN=
 TSKIP-12.650 DIGITS-0.000,746.875 TAPE22
 S.R. -100.00 KHZ 8 50 AM, 2 MAY 78. FILE-36

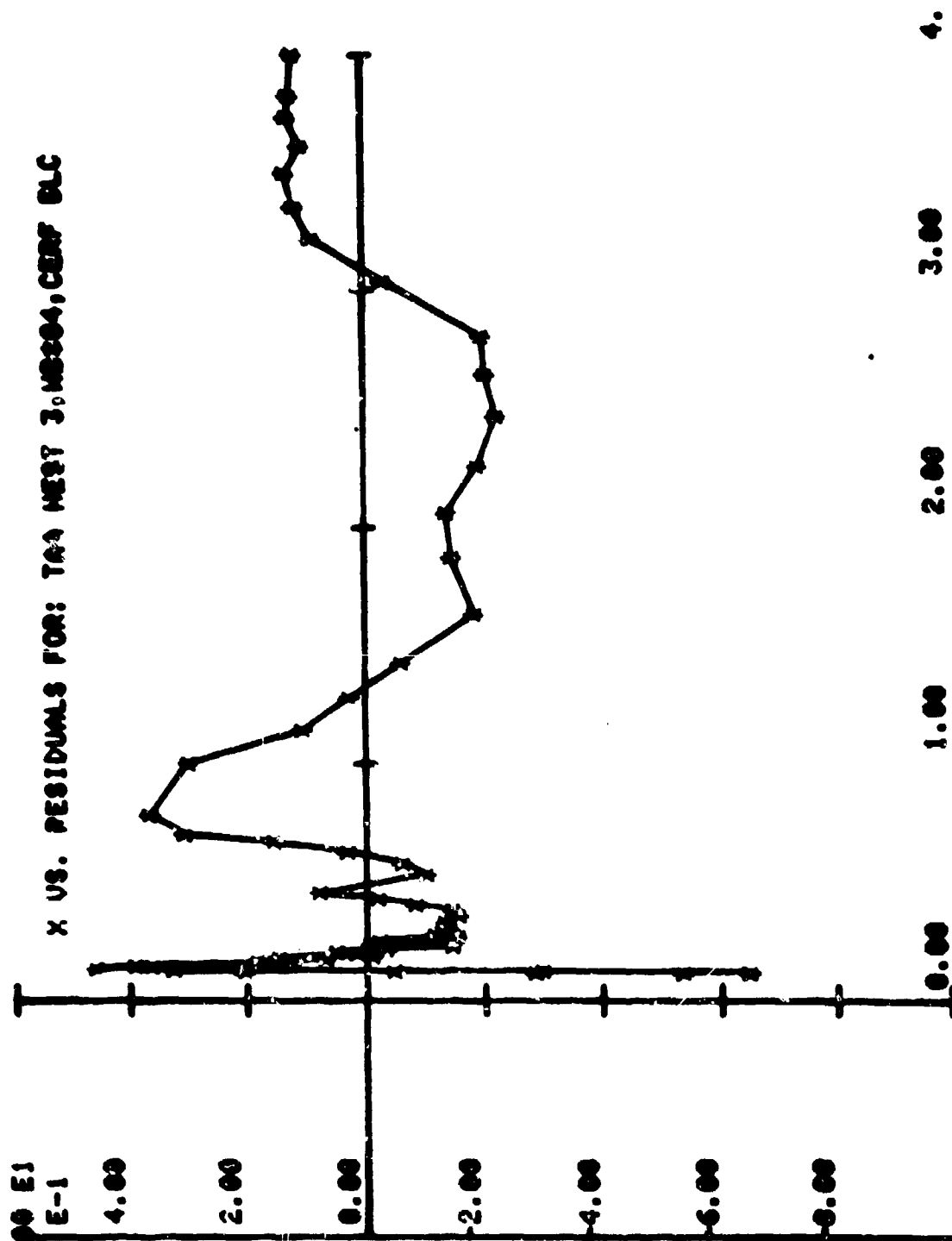


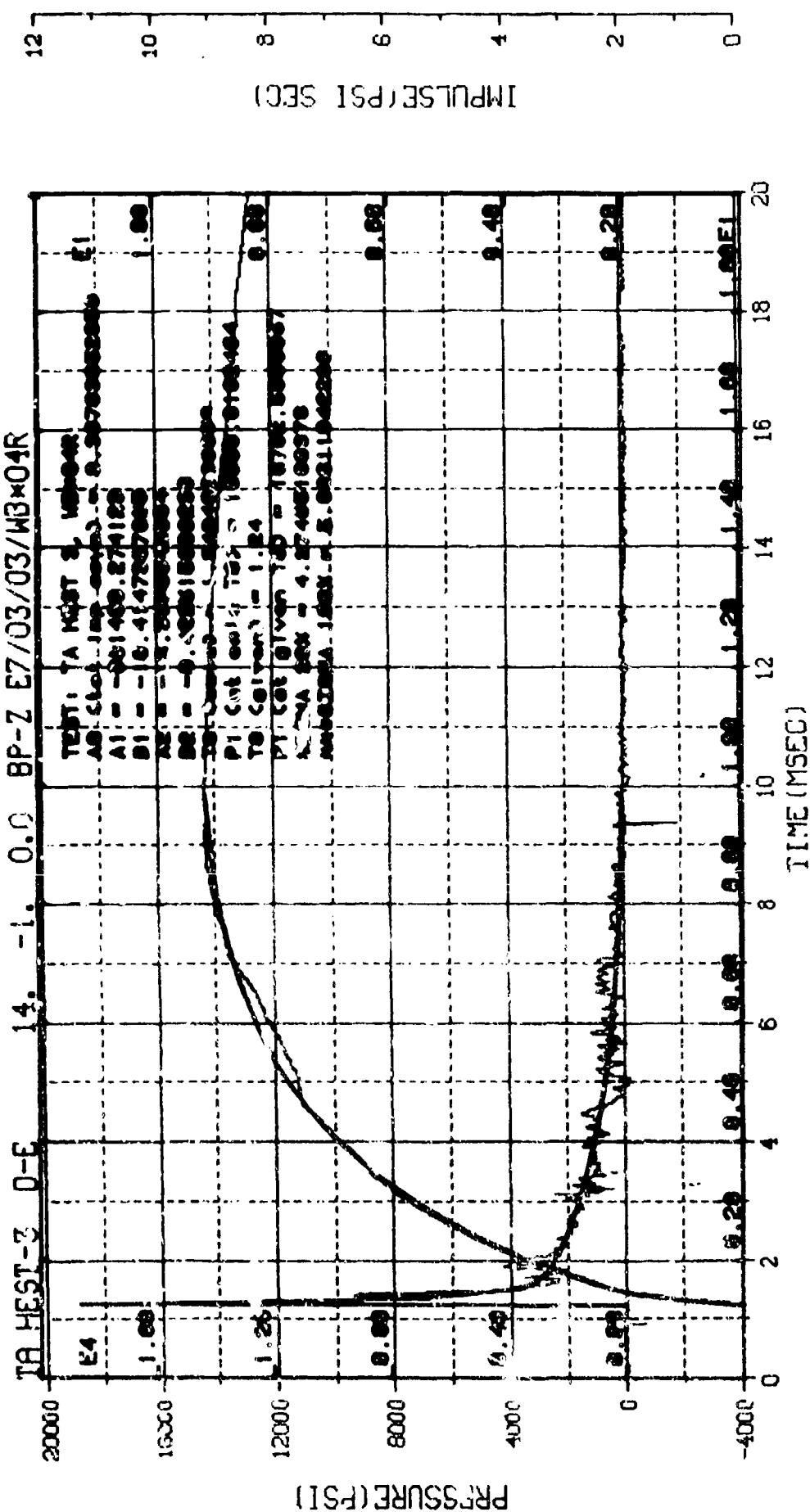


TA HEST-3 D-E 14. -1. 0.0 BP-Z E7/G4/04/WB*04

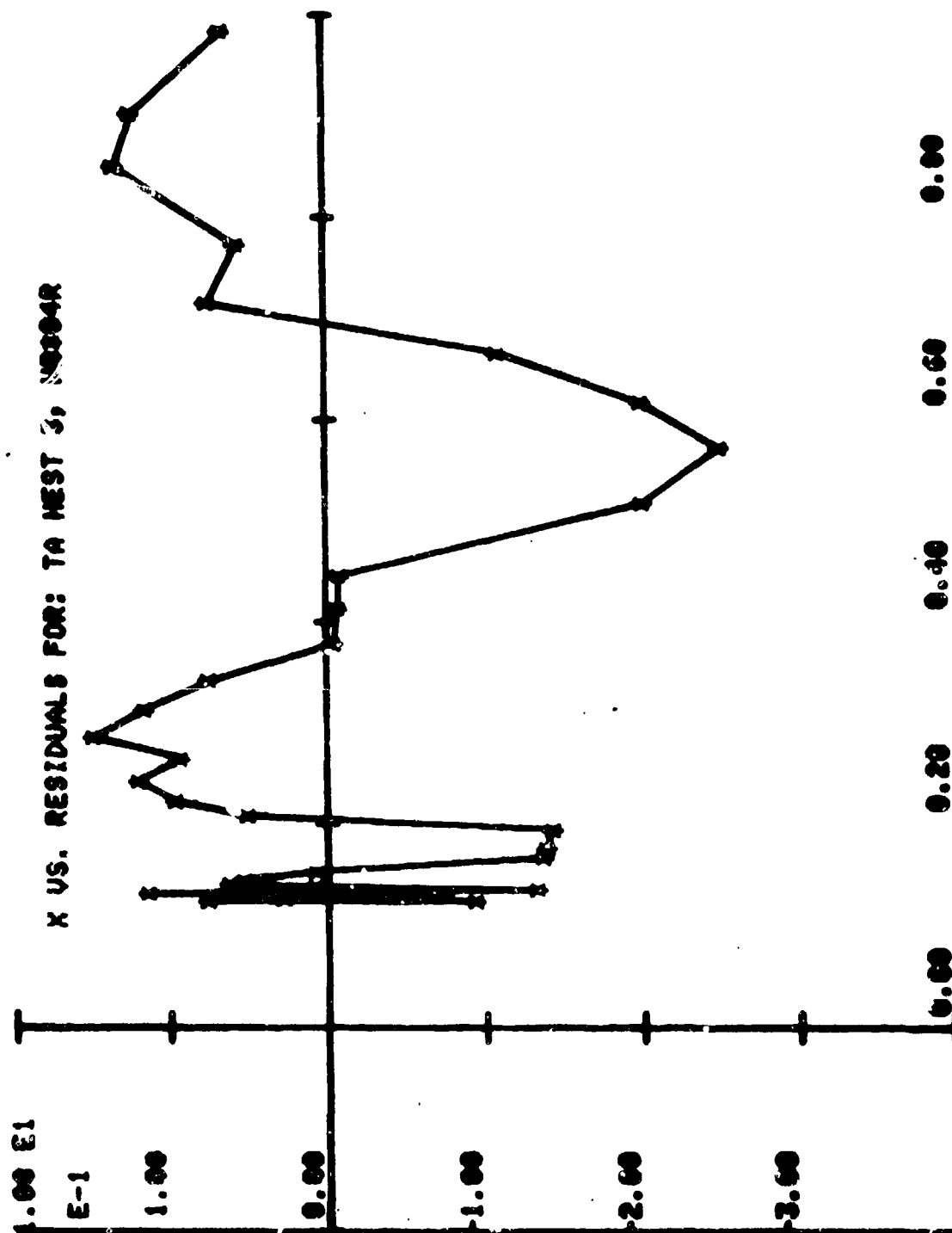


M.N. = 4 E.U. =0.000, 9265.000 VSN=
TSKIP=12.650 DIGITS=0.000, 692.000 TAPE22
S.R.=100.00 KHZ 8 50 AM, 2 MAY 78. FILE=38

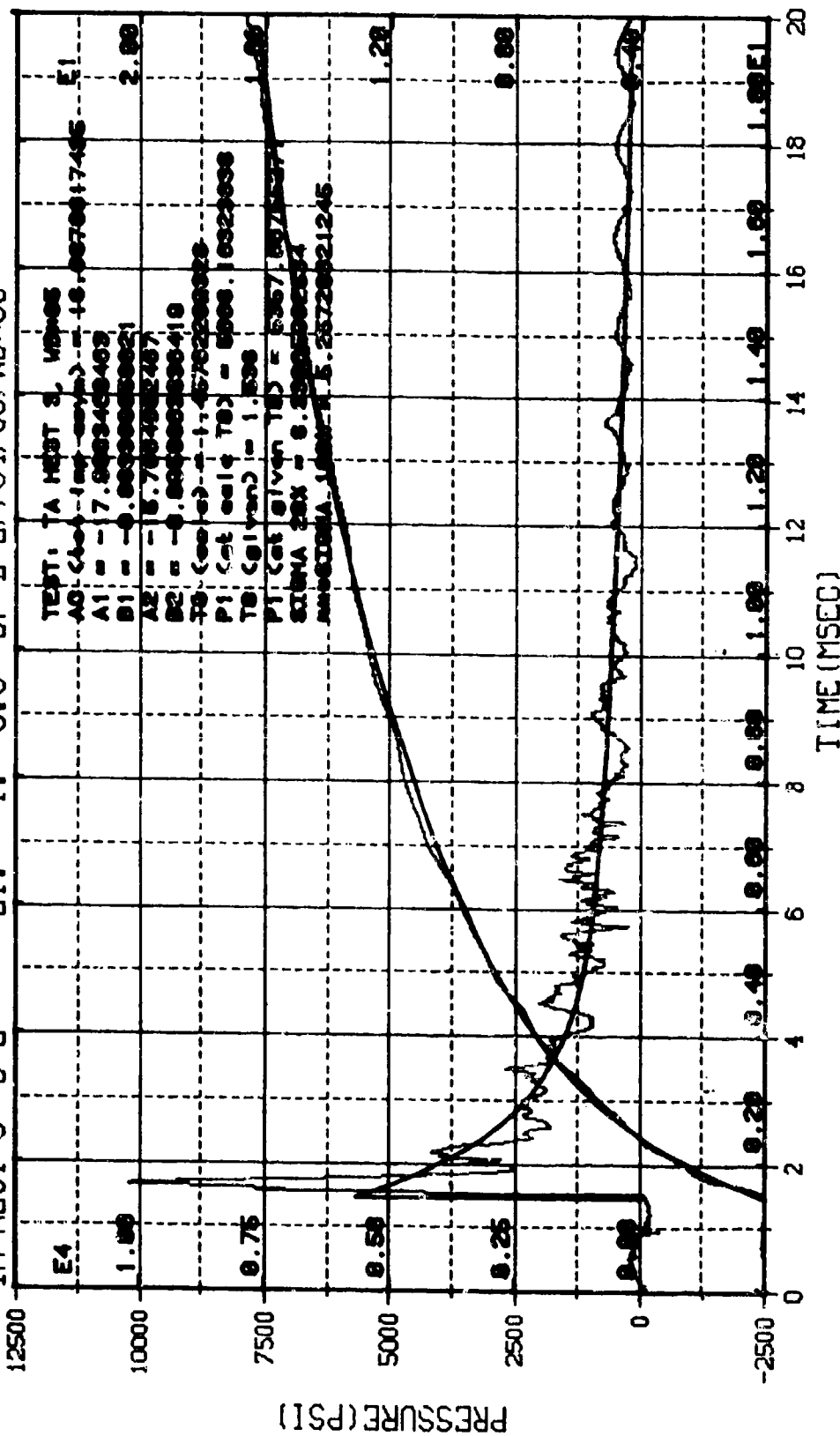




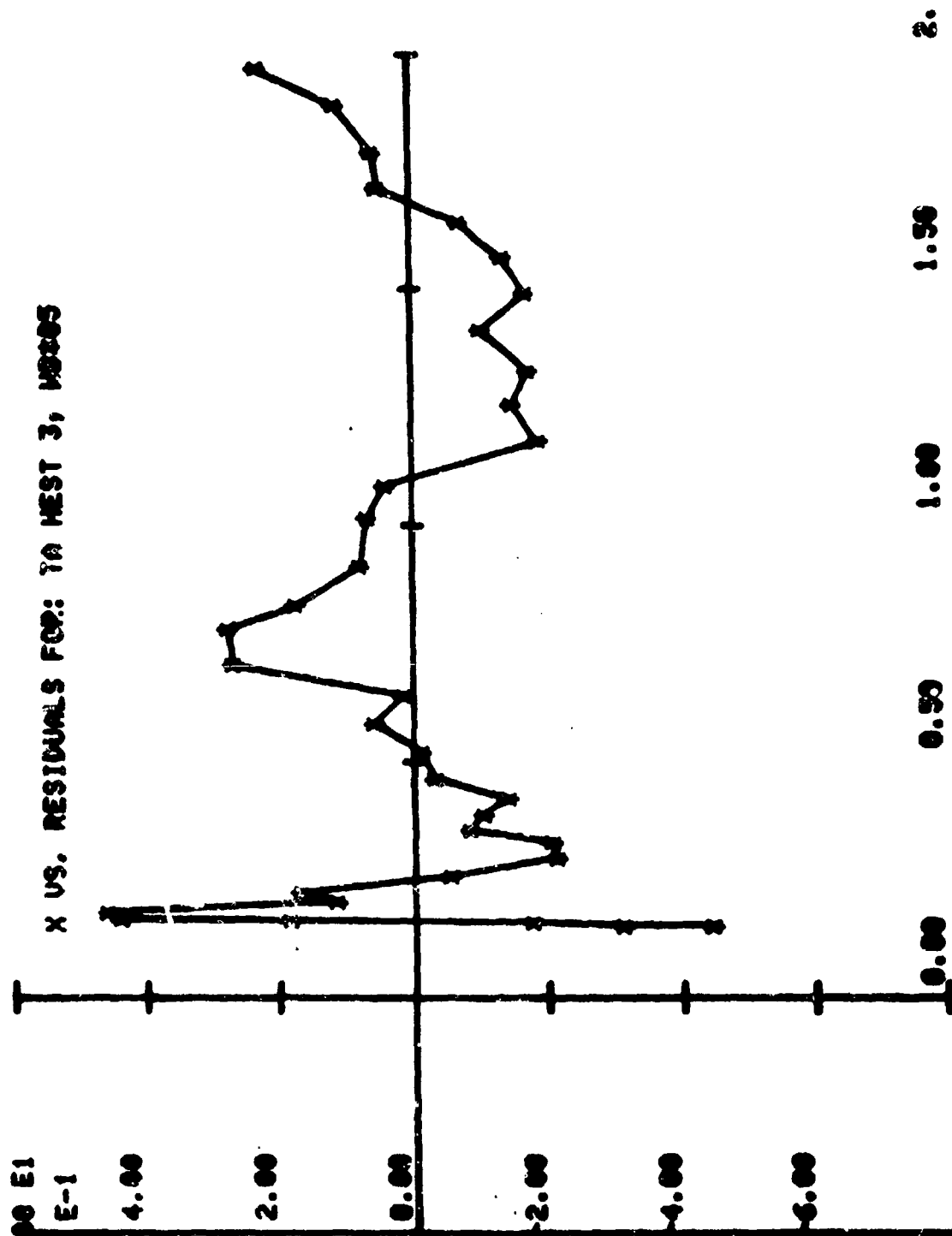
M.N. = 4
TSKIP=12.640
S.R. =100.00 KHZ
E.U. =0.000,9265.000
DIGITS=0.000,680.000
8 50 AM, 2 MAY 78.
VSN=
TAPE22
FILE=24

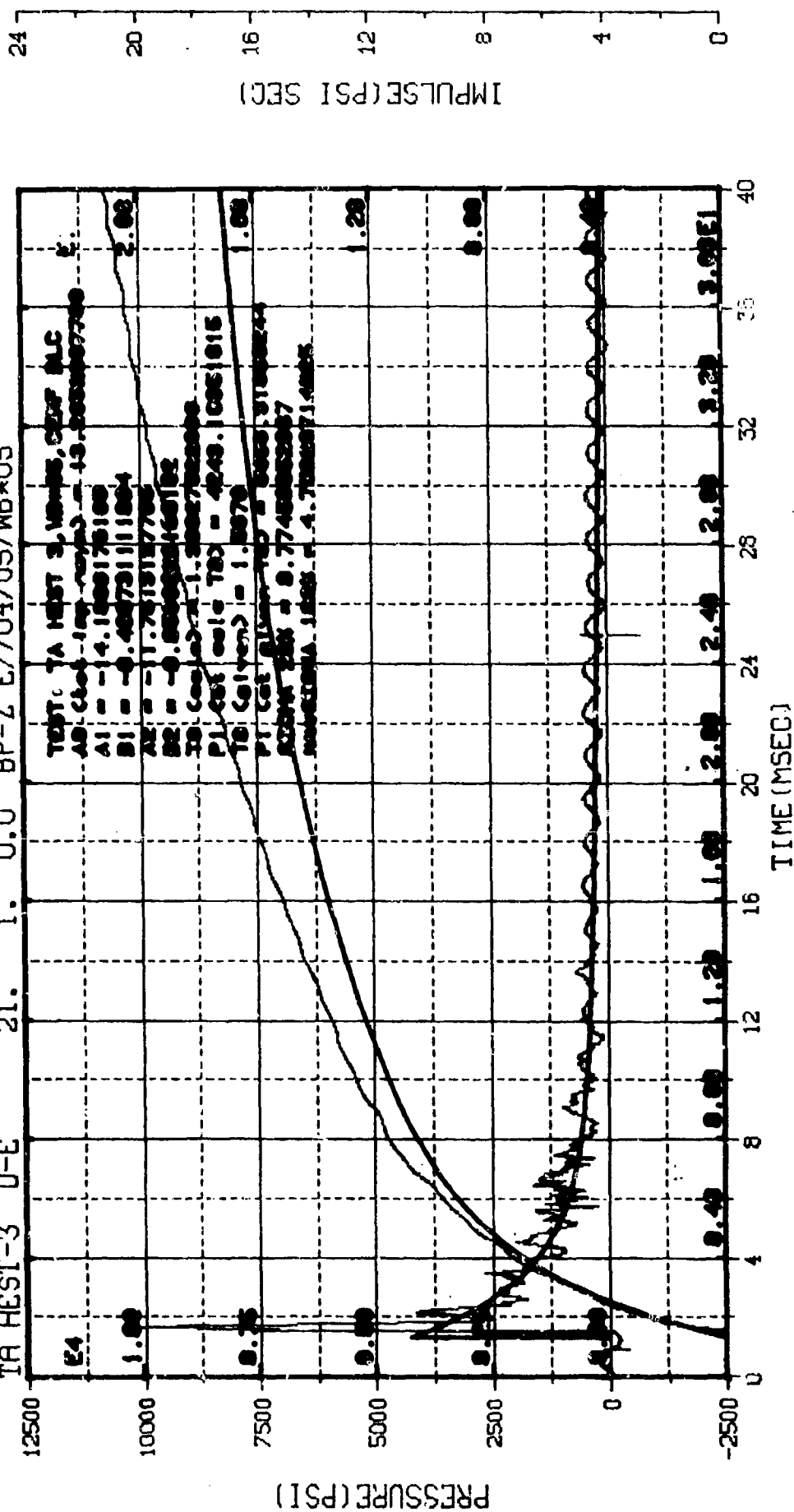


TA HEST-3 D-E 21. 1. 0.0 BP-Z E7/04/05/WB*05

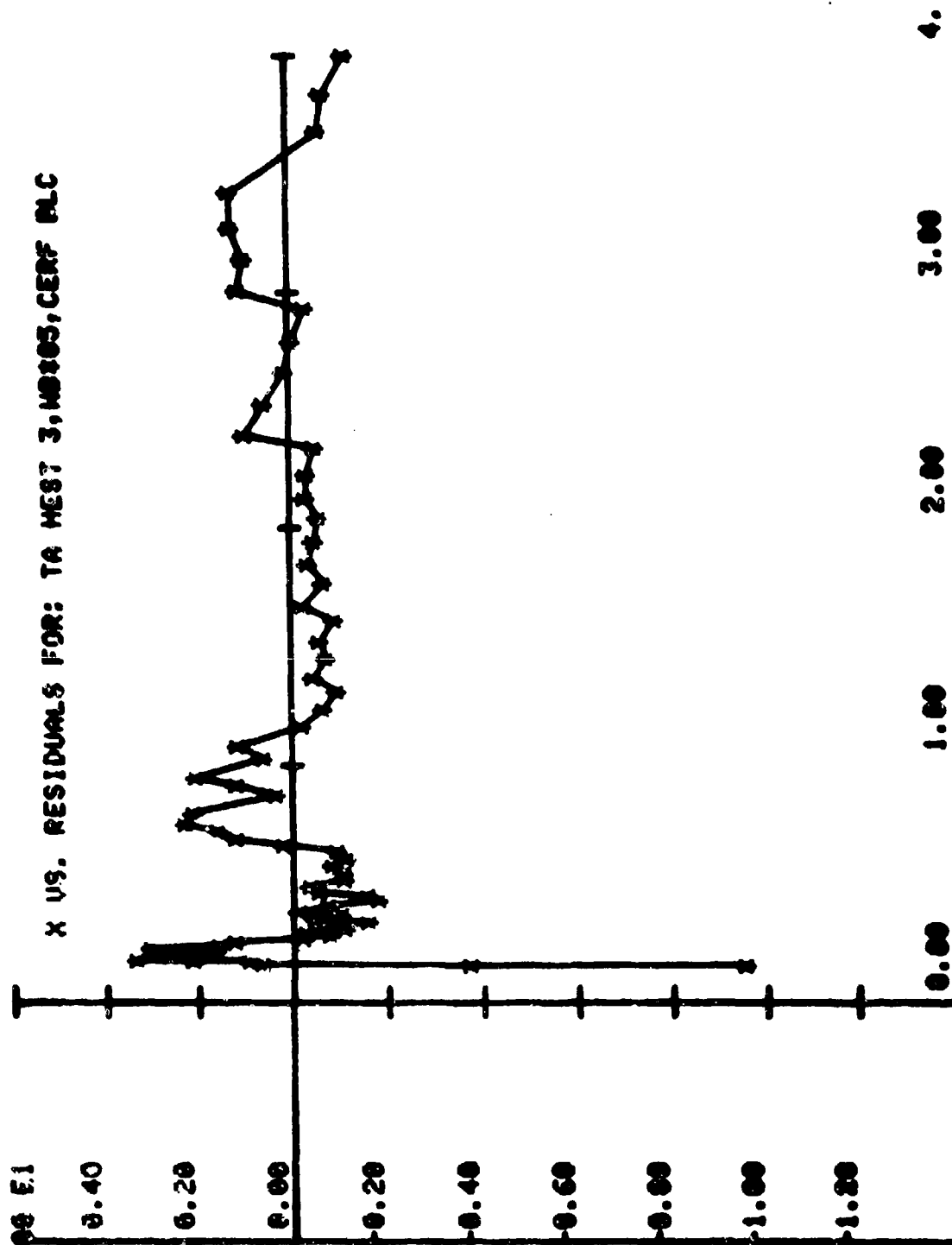


M.N. = 5 E.U. = 0.000,7095.000 VSN= ED23
 TSKIP=12.650 DIGITS=0.000,756.000 TAPE22
 S.R. =100.00 KHZ 11 36 AM, 2 MAY 78. FILE=40

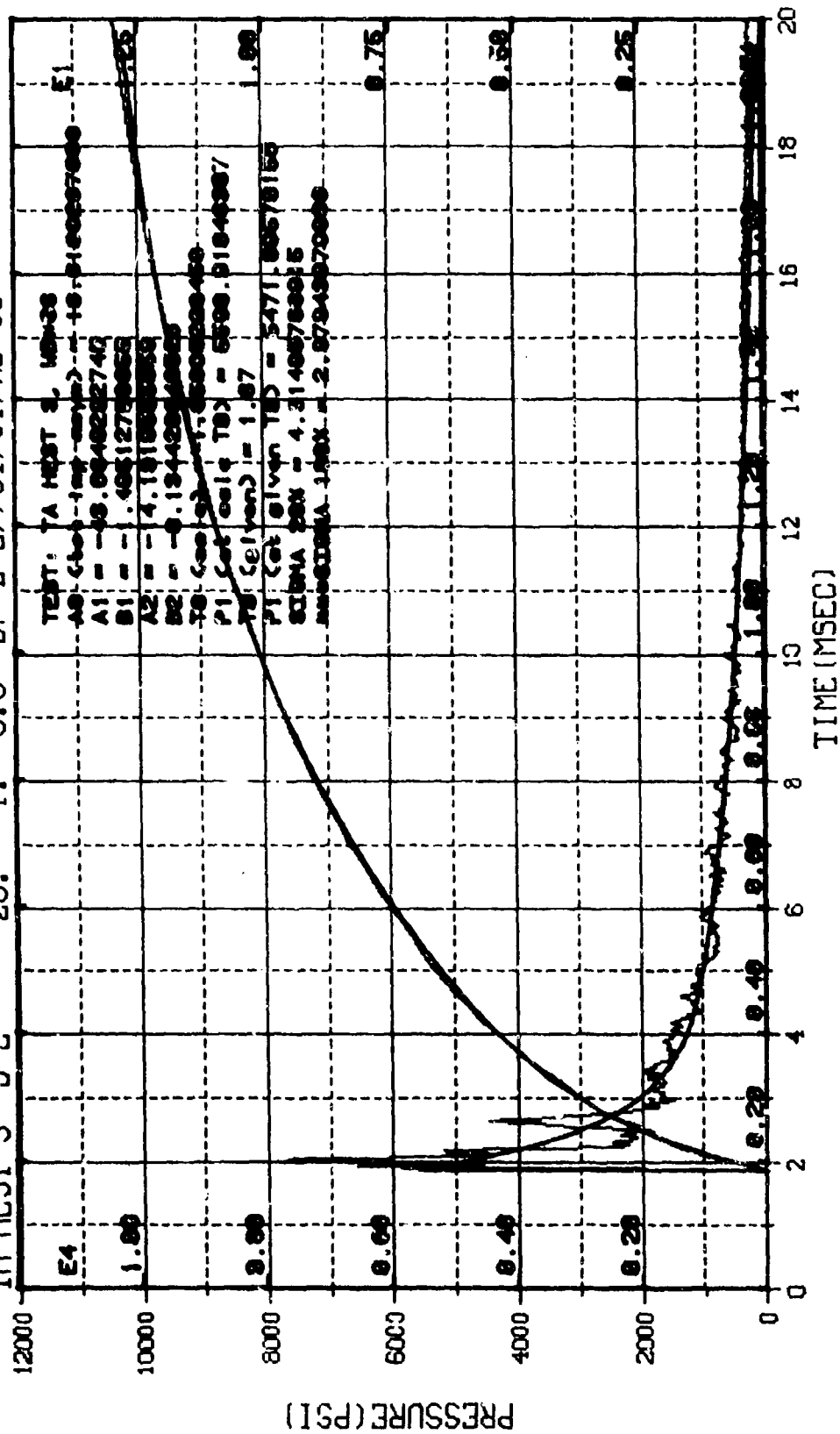




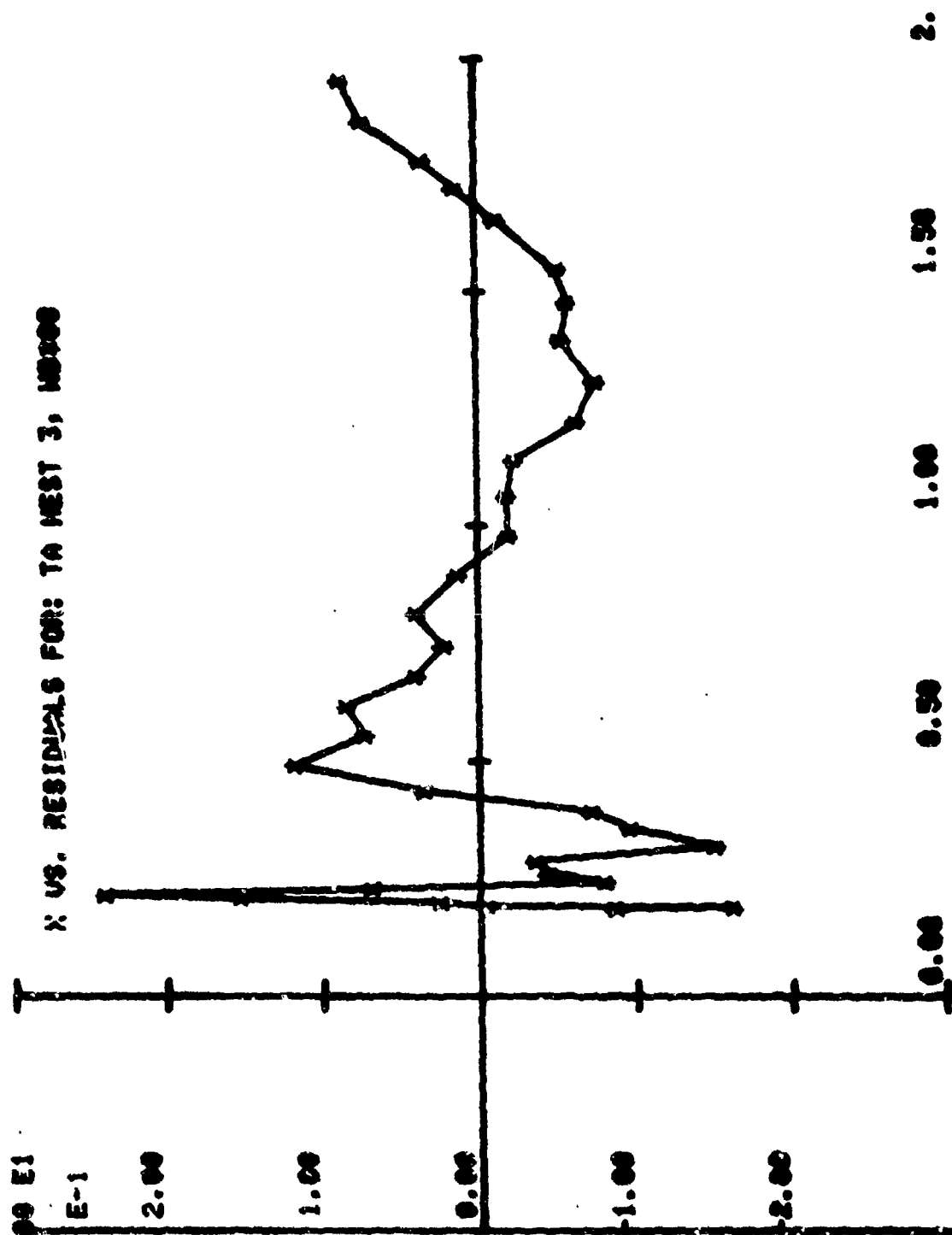
M.N.	-	5	E.U.	=0.000,7095.000	VSN=
TSKIP	-	12.650	DIGITS	=0.000,756.000	TAPE22
S.R.	-	100.00 KHZ		8 50 AM, 2 MAY 78.	FILE=40



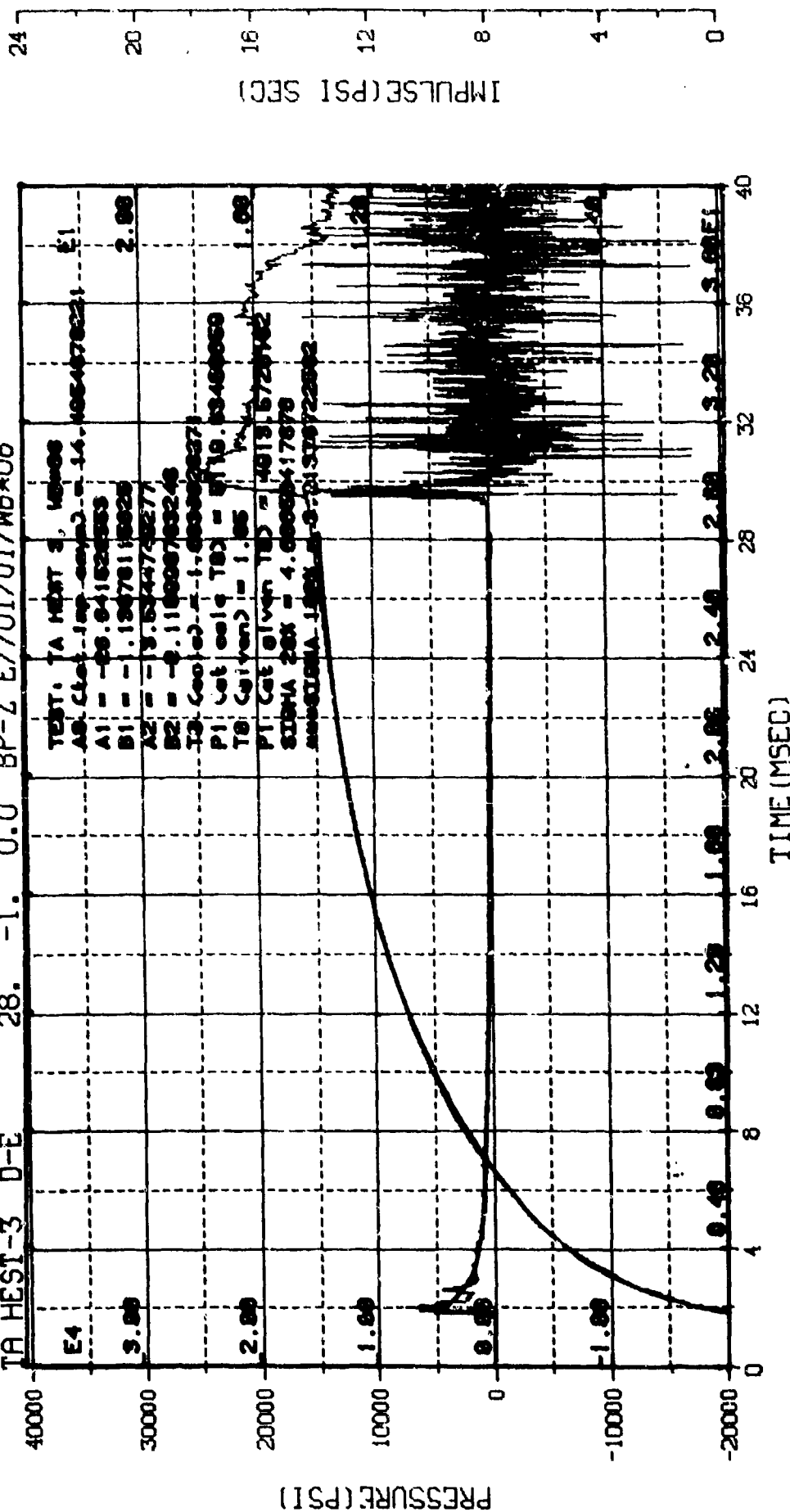
TA HEST-3 D-E 28. -1. 0.0 BP-Z E7/01/01/WBx08



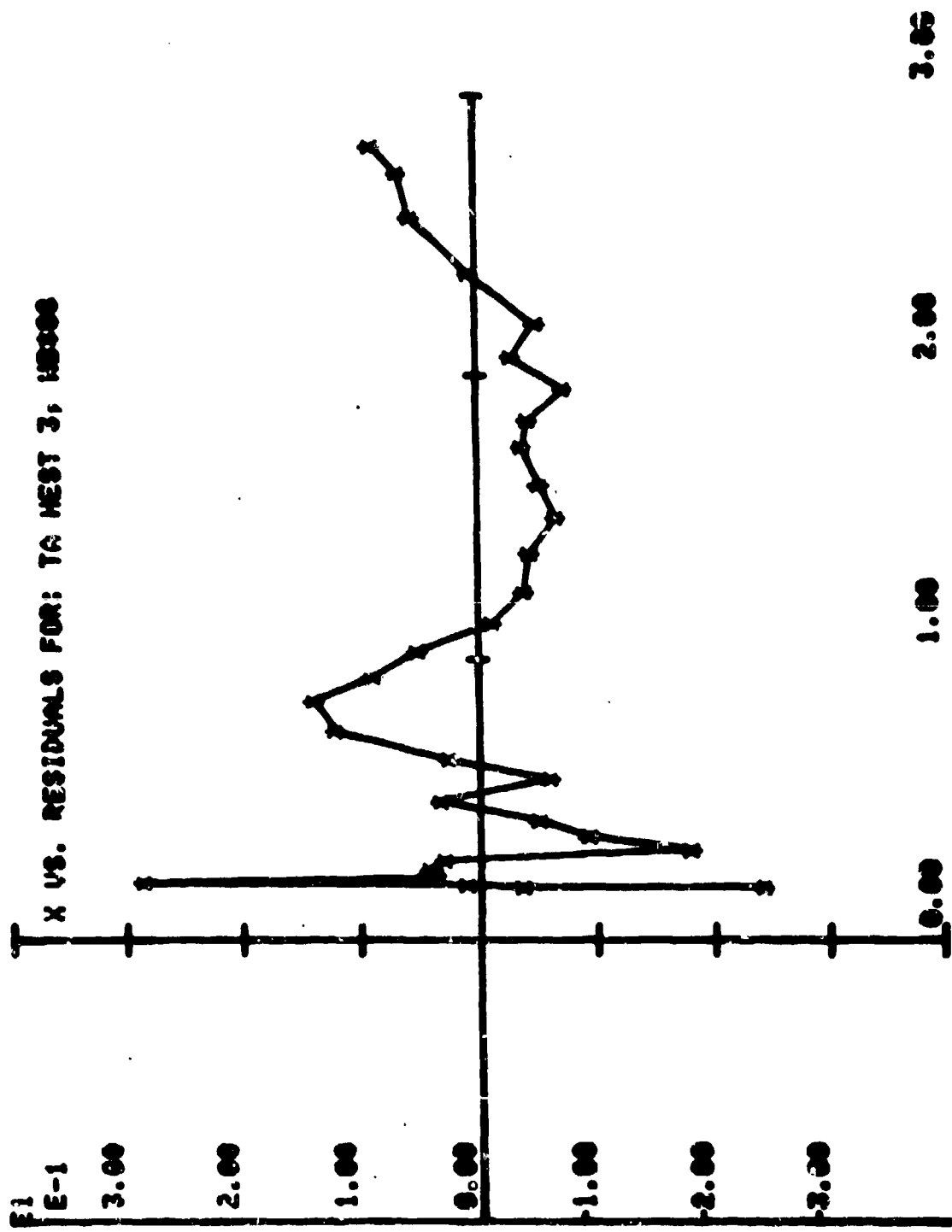
1.N. = 8 E.U. = 0.000,6514.000 VSN=
TSKIP=12.640 DIGITS=0.000,764.000 TAPE22
S.R. =100.00 KHZ 8 50 AM, 2 MAY 78. FILE=2
1

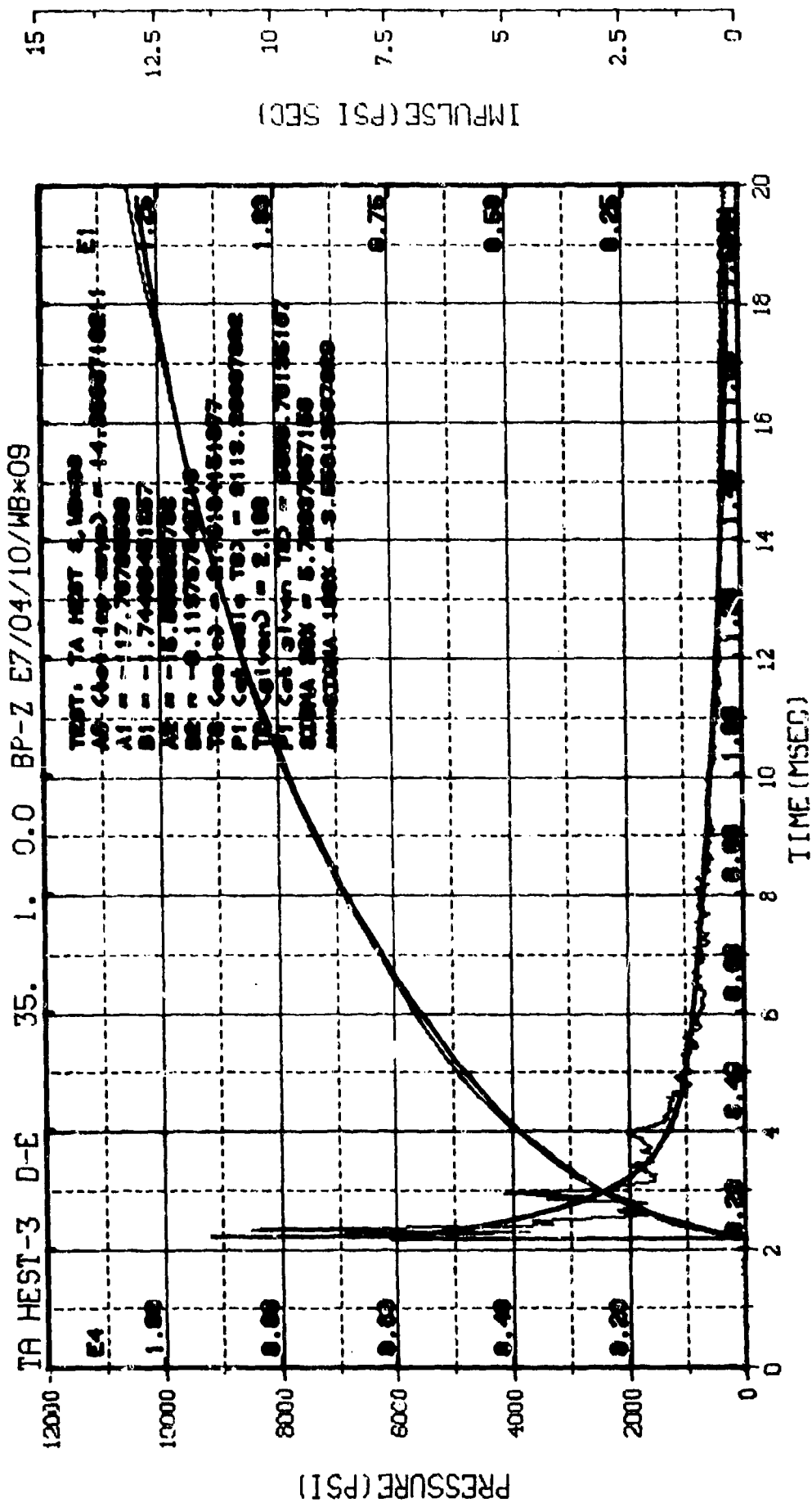


TA HEST-3 D-E 28. -1. 0.0 BP-Z E7/01/01/WBx08

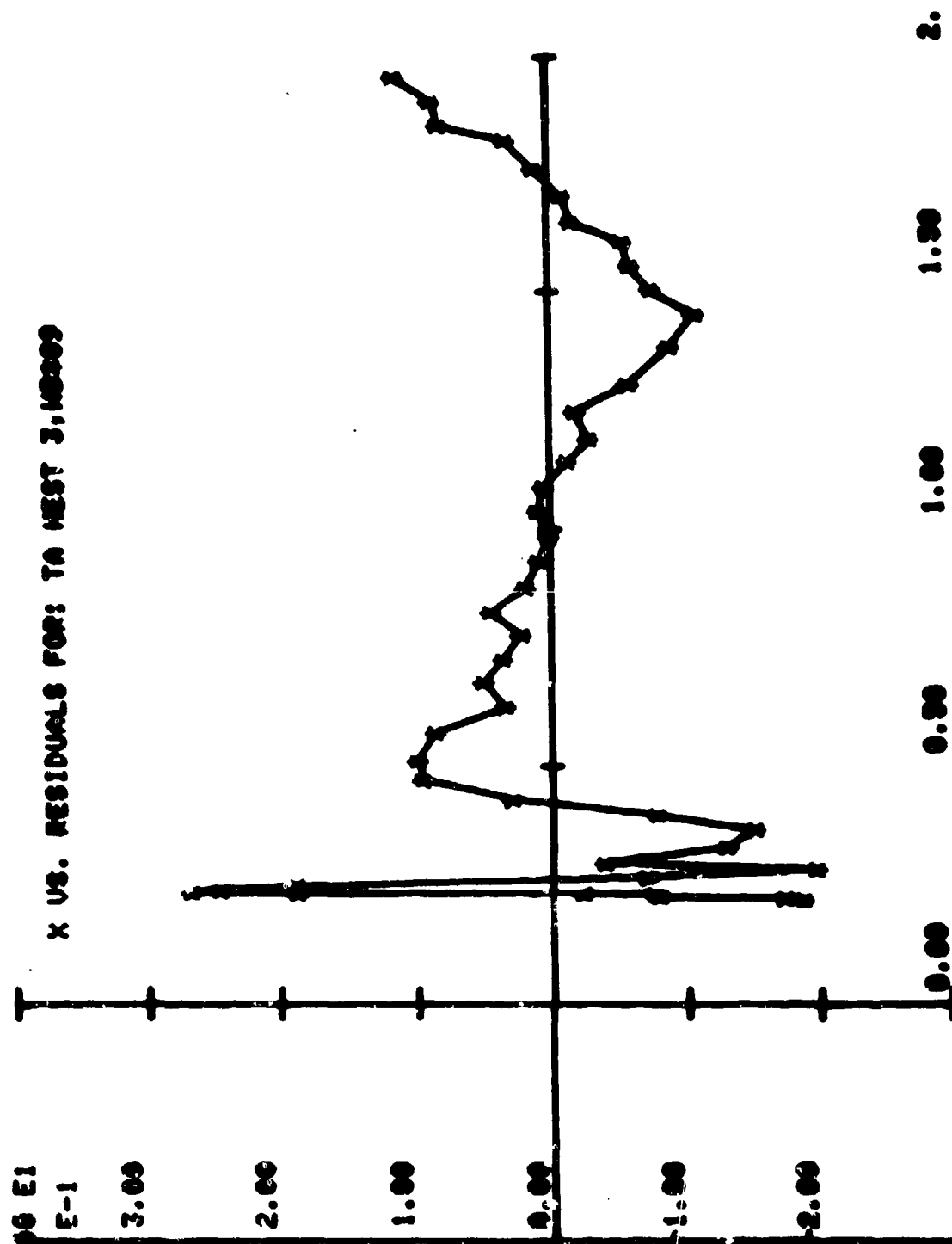


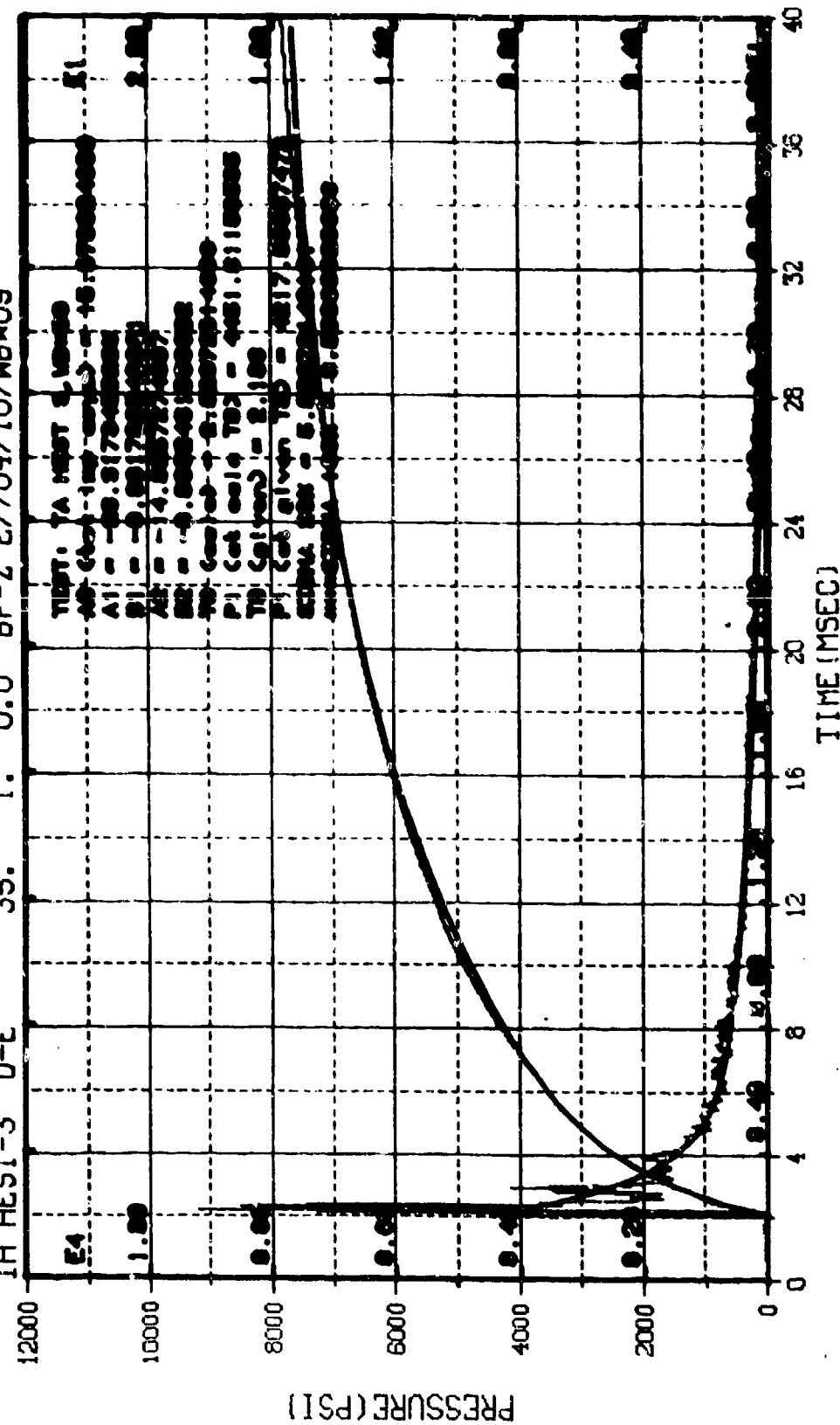
M.N. = 8 E.U. -0.000,6514.000 VSN=
 TSKIP=12.640 DIGITS=0.000,754.000 TAPE22
 S.R. =100.00 KHZ 8 50 AM, 2 MAY 78. FILE=2



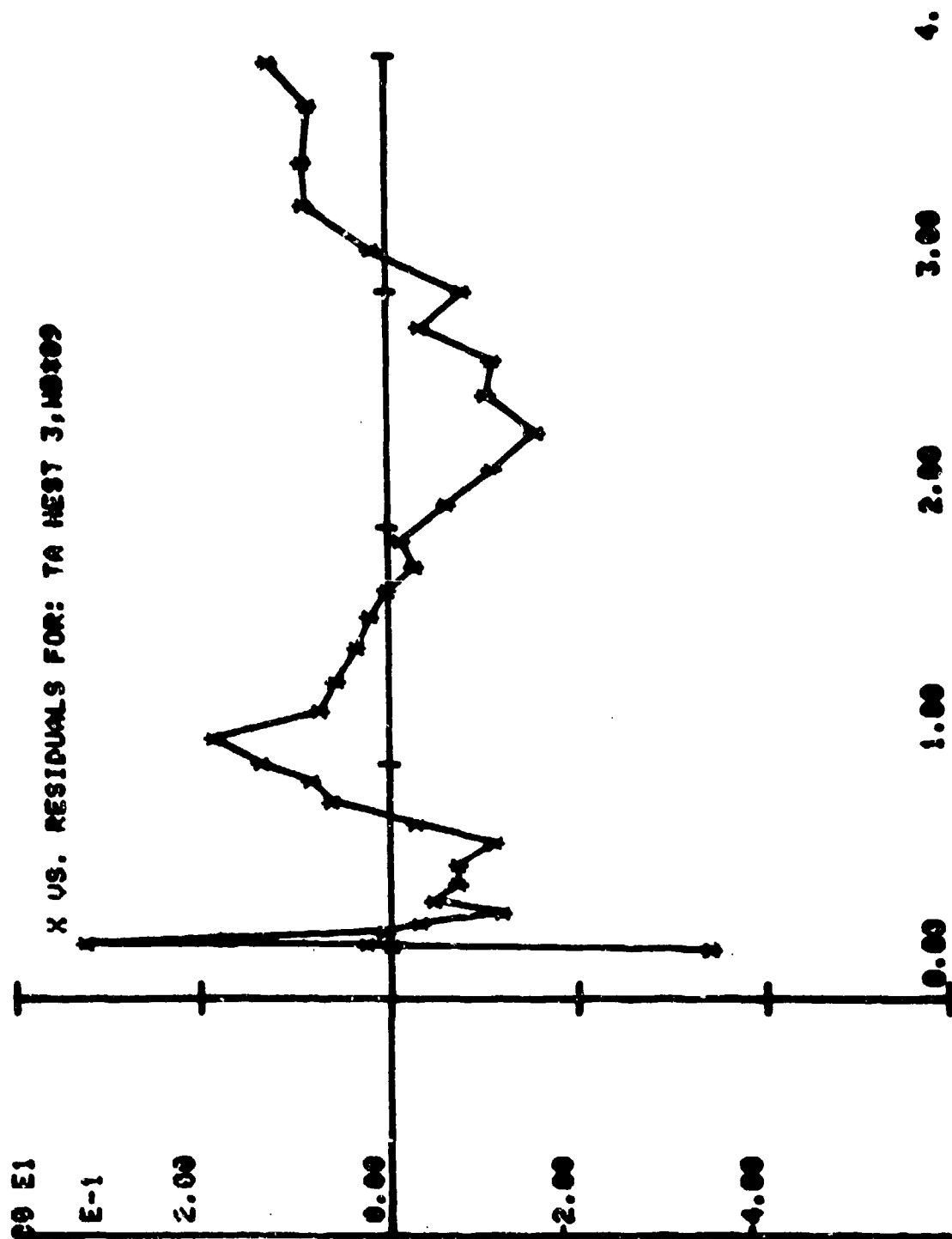


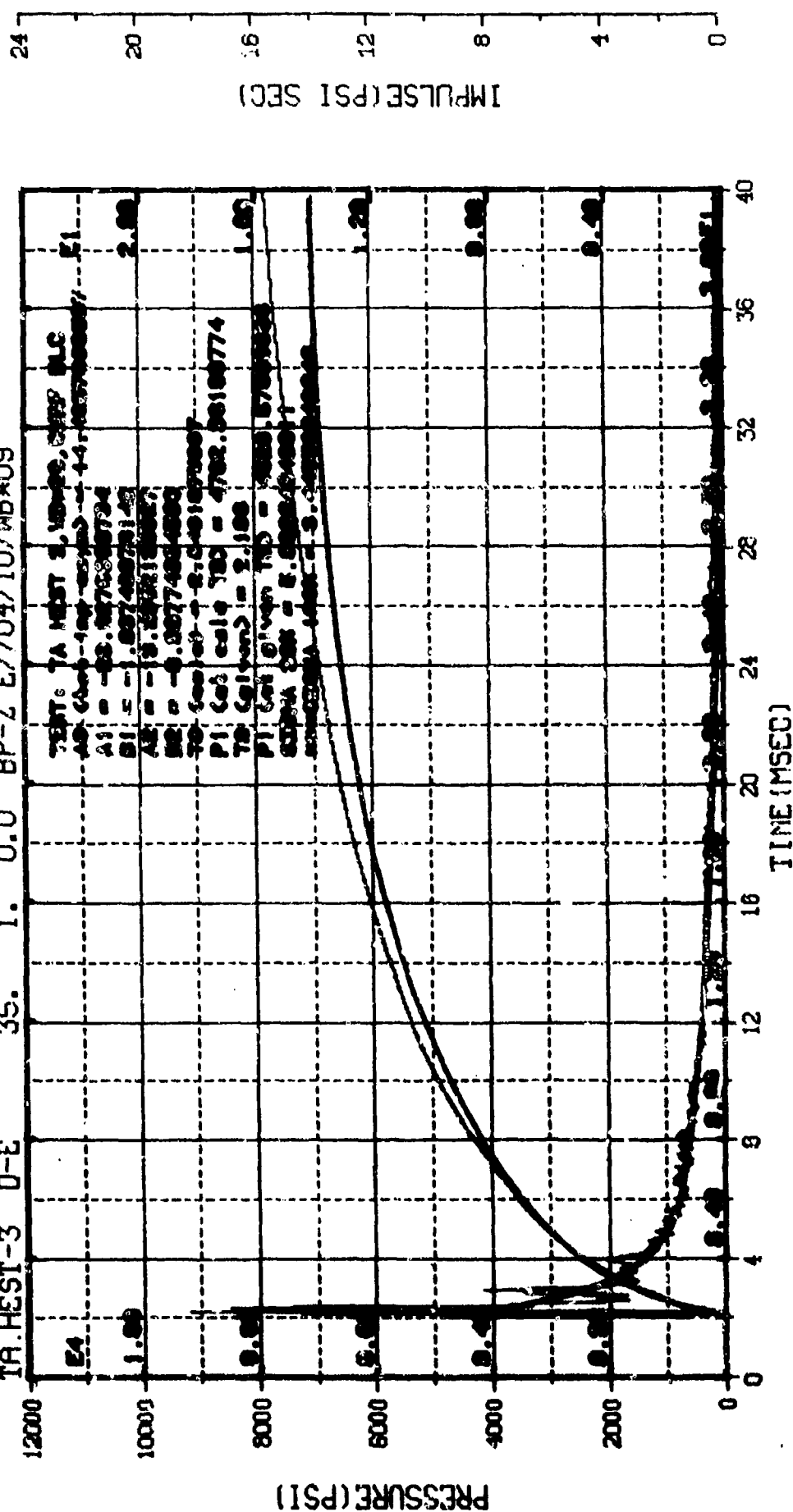
M.N. = 9 E.U. -0.000,6454.000 VSN= ED23
 TSKIP=12.650 DIGITS=0.000,831.500 TAPE22
 S.R. =100.00 KHZ 11 36 AM, 2 MAY 78. FILE=44



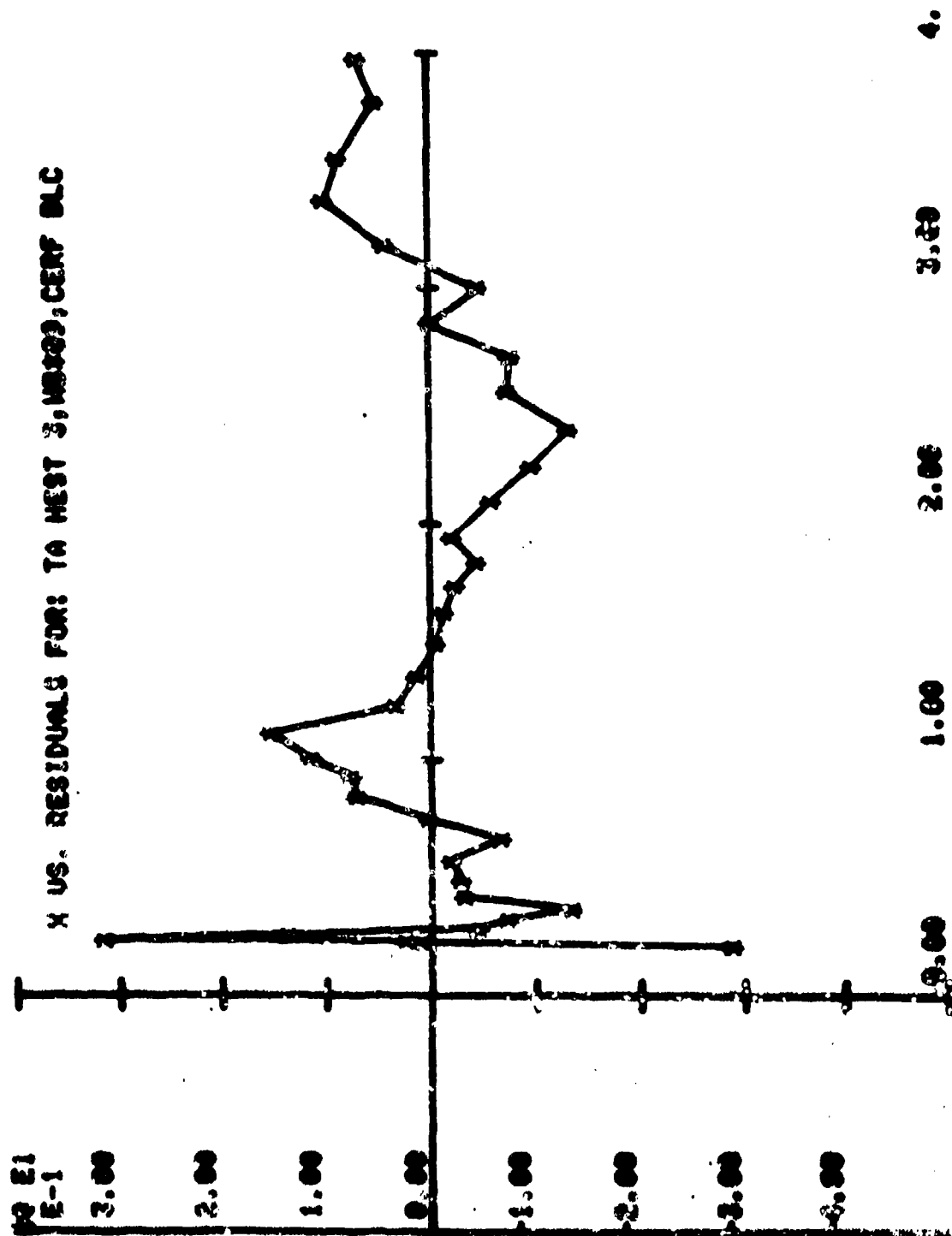


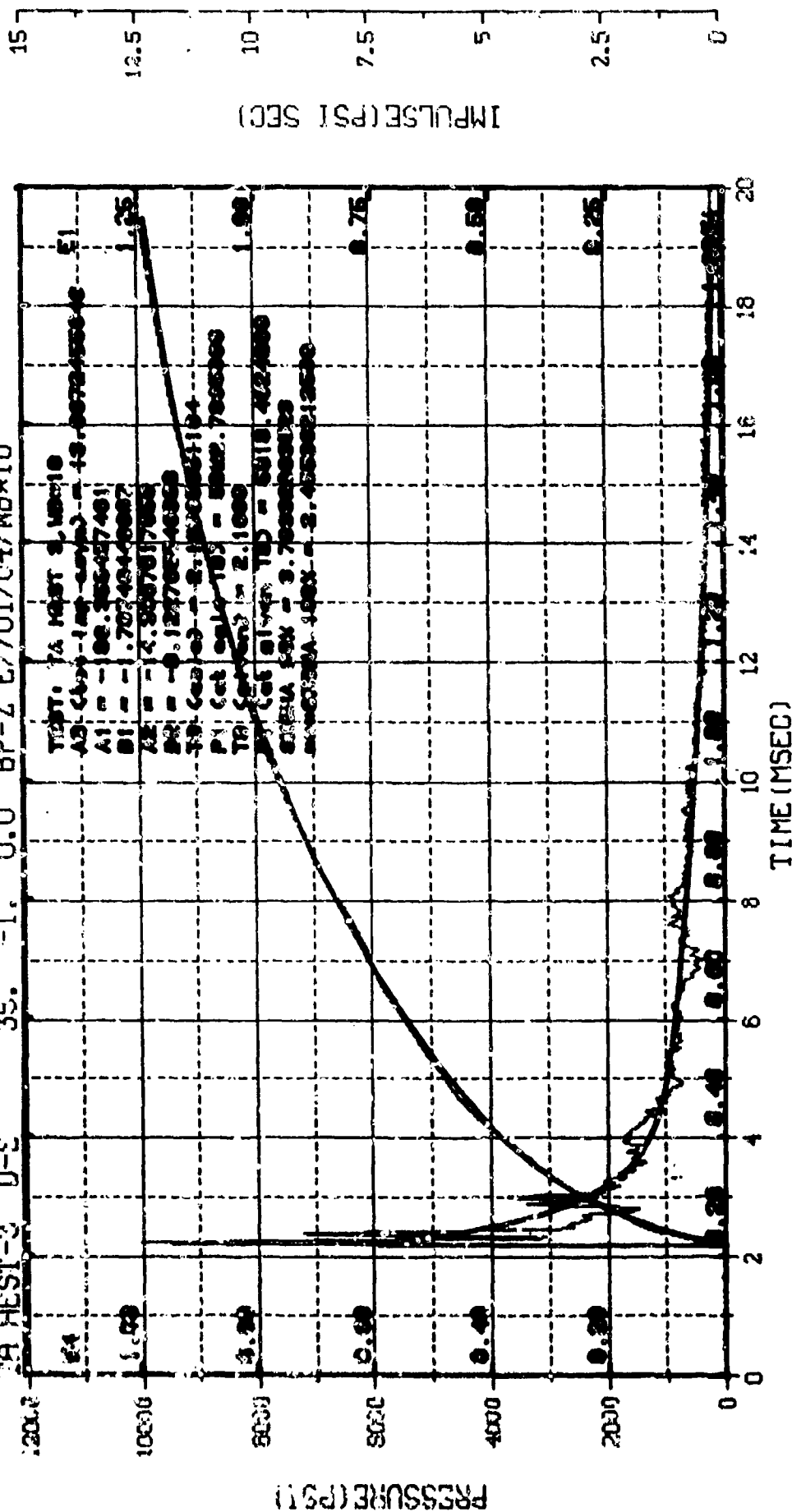
M.N. - 9
TSKIP-12.650
S.R. -100.00 KHZ
E.U. -0.000,6454.000
DIGITS-0.000,831.500
8 50 AM, 2 MAY 78.
VSN-
TAPE22
FILE-44



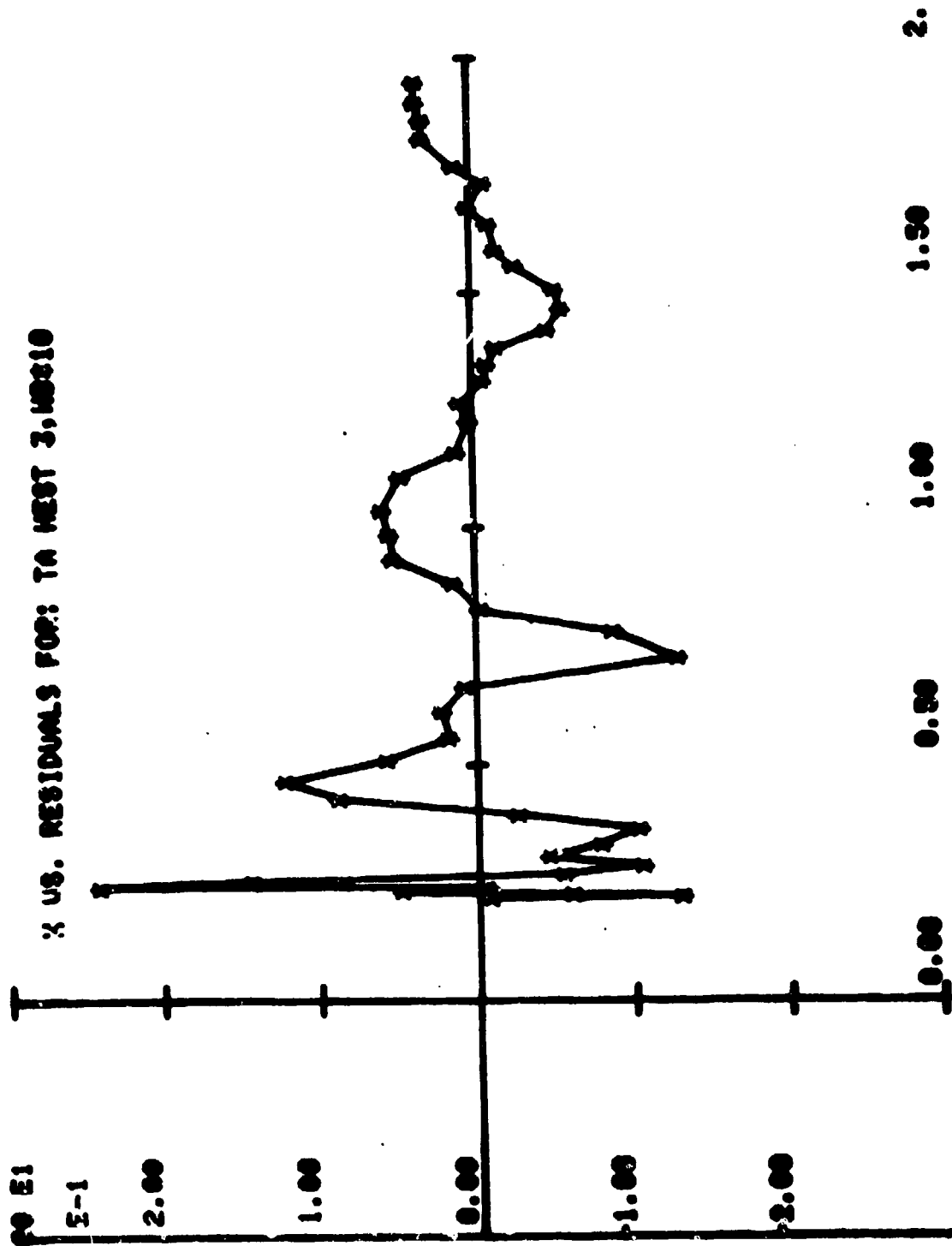


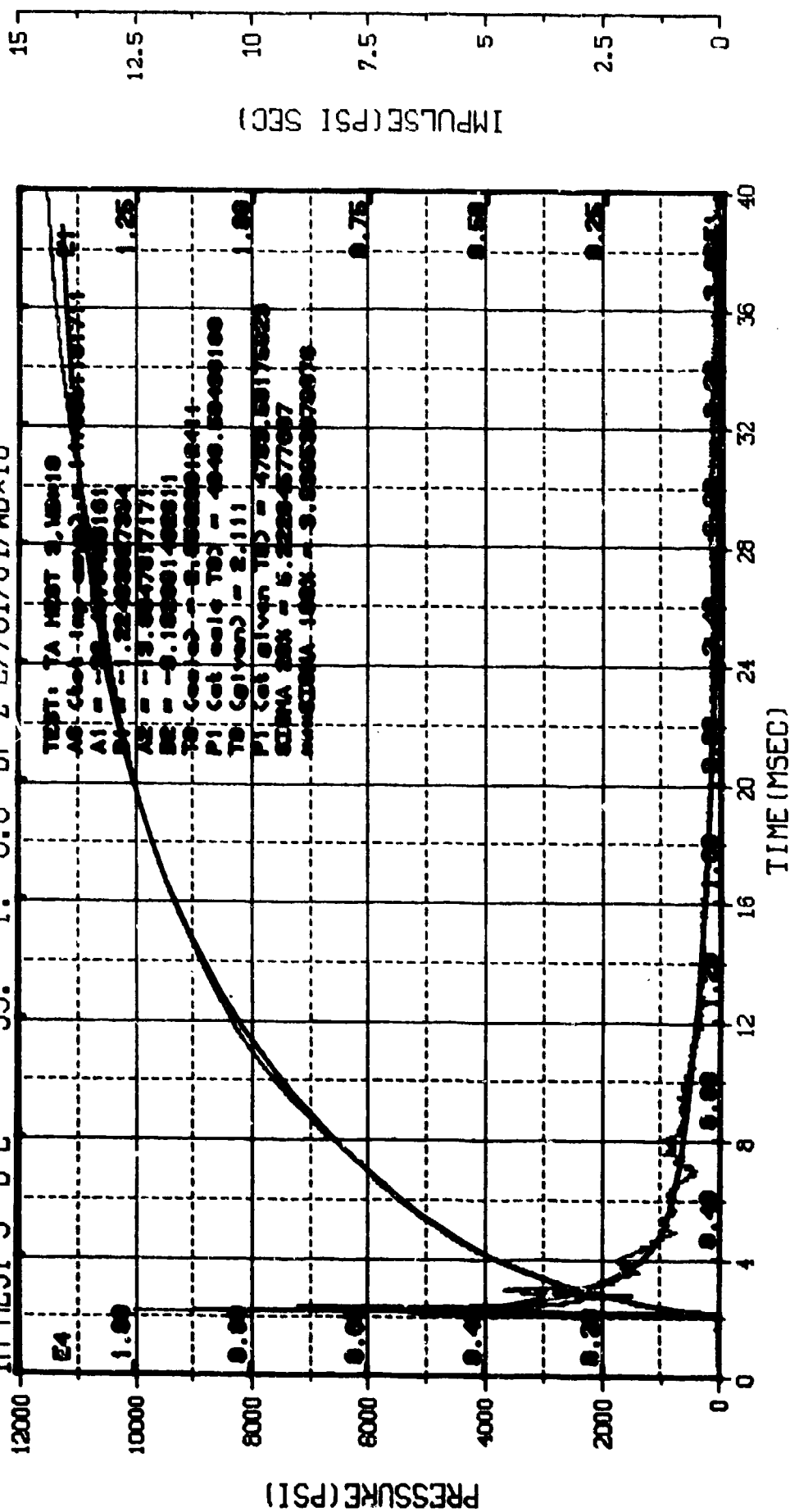
M.N. - 9
TSKIP-12.650
S.R. -100.00 KHZ
E.U. -0.000, 6454.000
DIGITS-0.000, 831.500
8 50 AM, 2 MAY 78.
VSN-
TAPE22
FILE-44



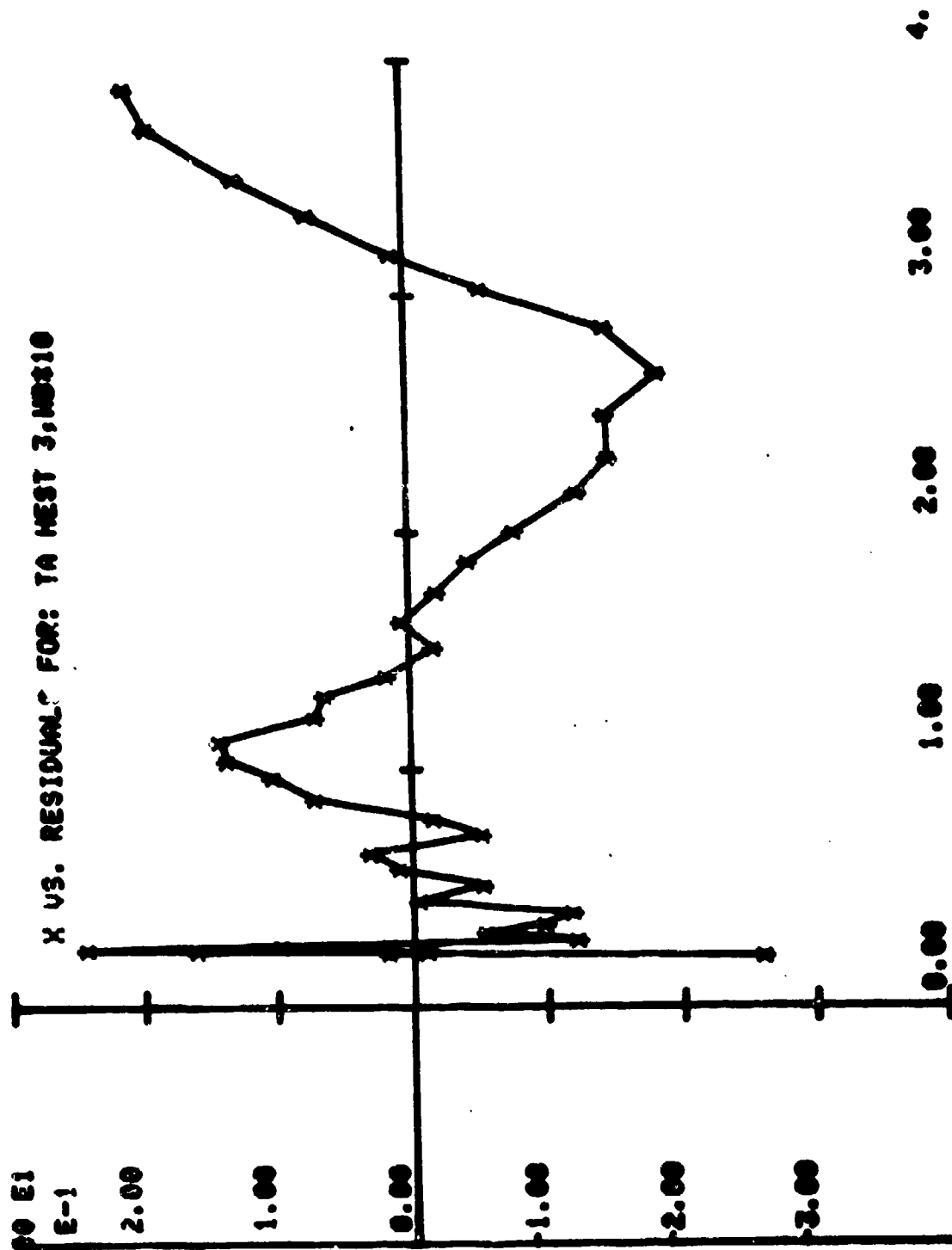


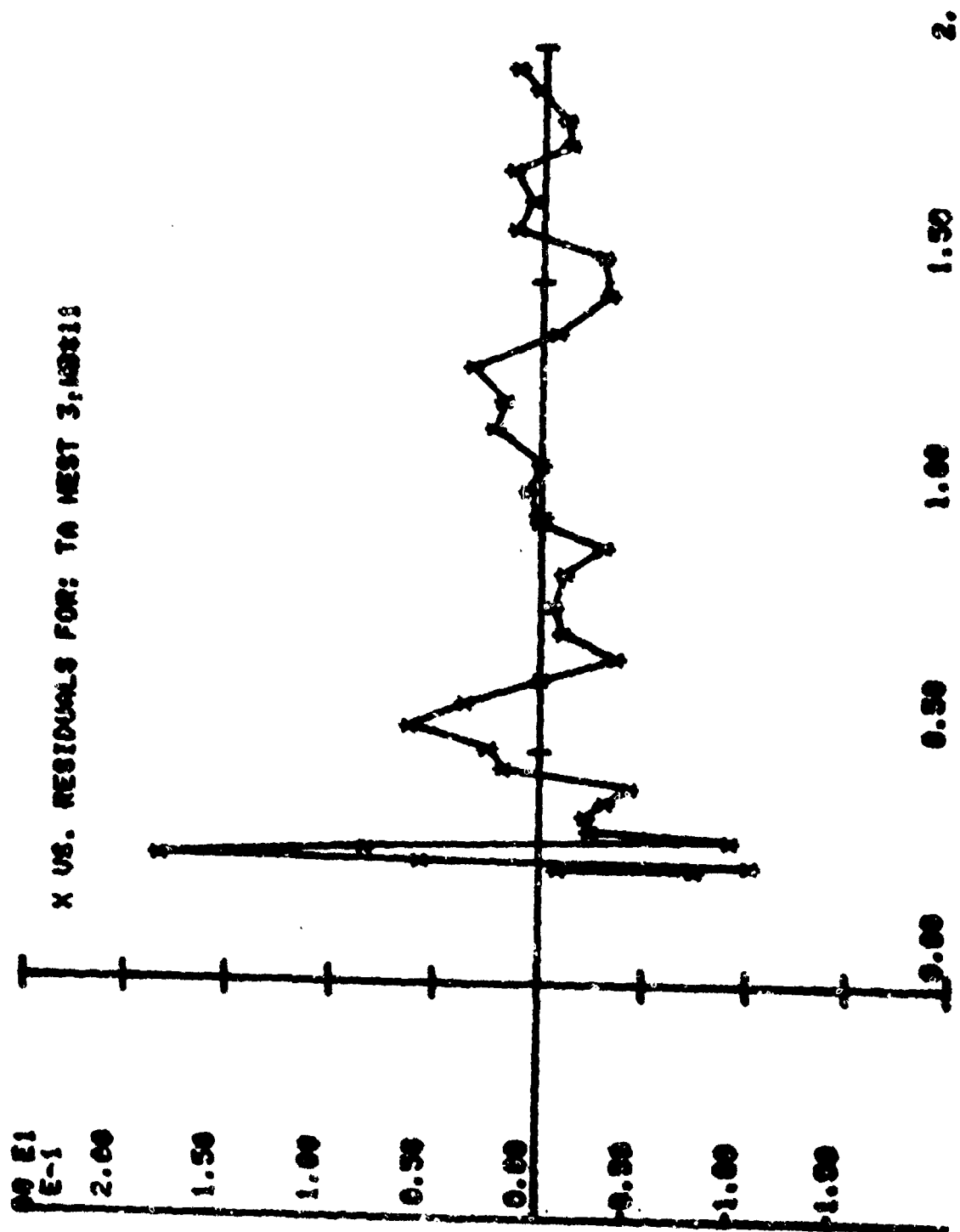
M.N. - 10
TSKIP-12.640
S.R. -100.00 KHZ
E.U. -0.000, 6272.000
DIGITS-0.000, 834.000
8 50 AM, 2 MAY 78.
VSN-
TAPE22
FILE-8

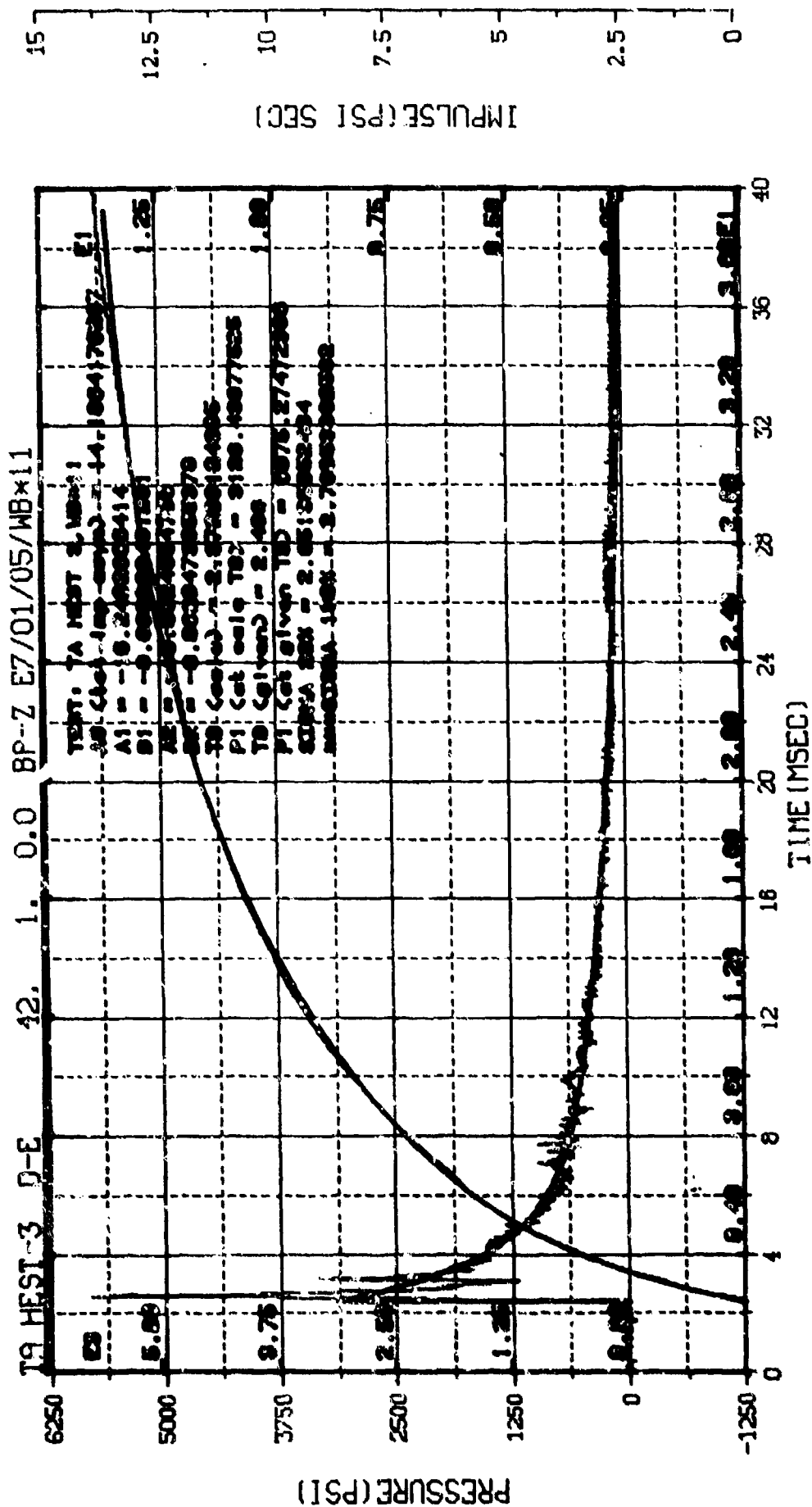




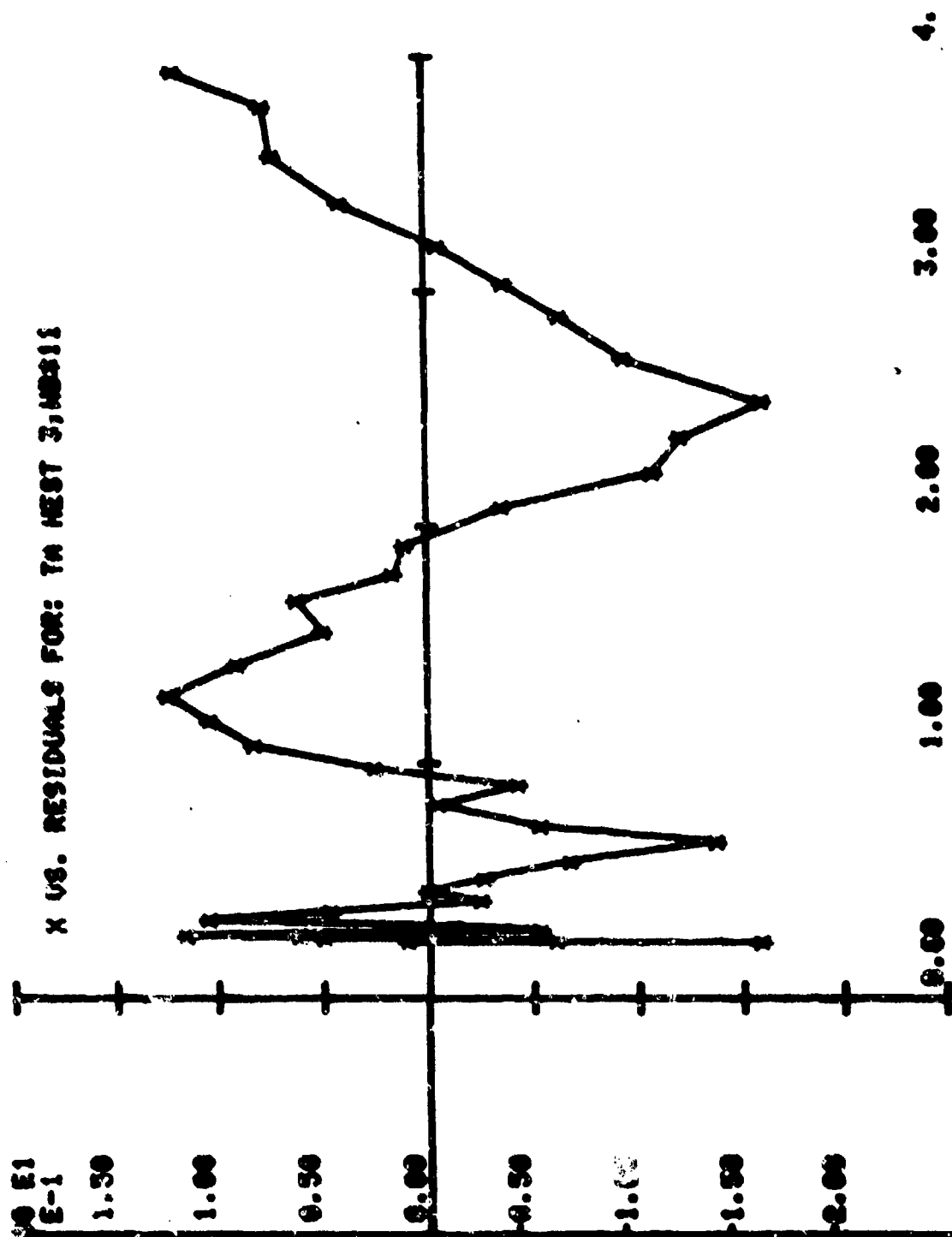
M.N. = 10
TSKIP-12.640
S.R. -100.00 KHZ
E.U. -0.000, 6272.000
DIGITS-0.000, 934.000
3 50 AM, 2 MAY 78.
VSN=
TAPE22
FILE=8

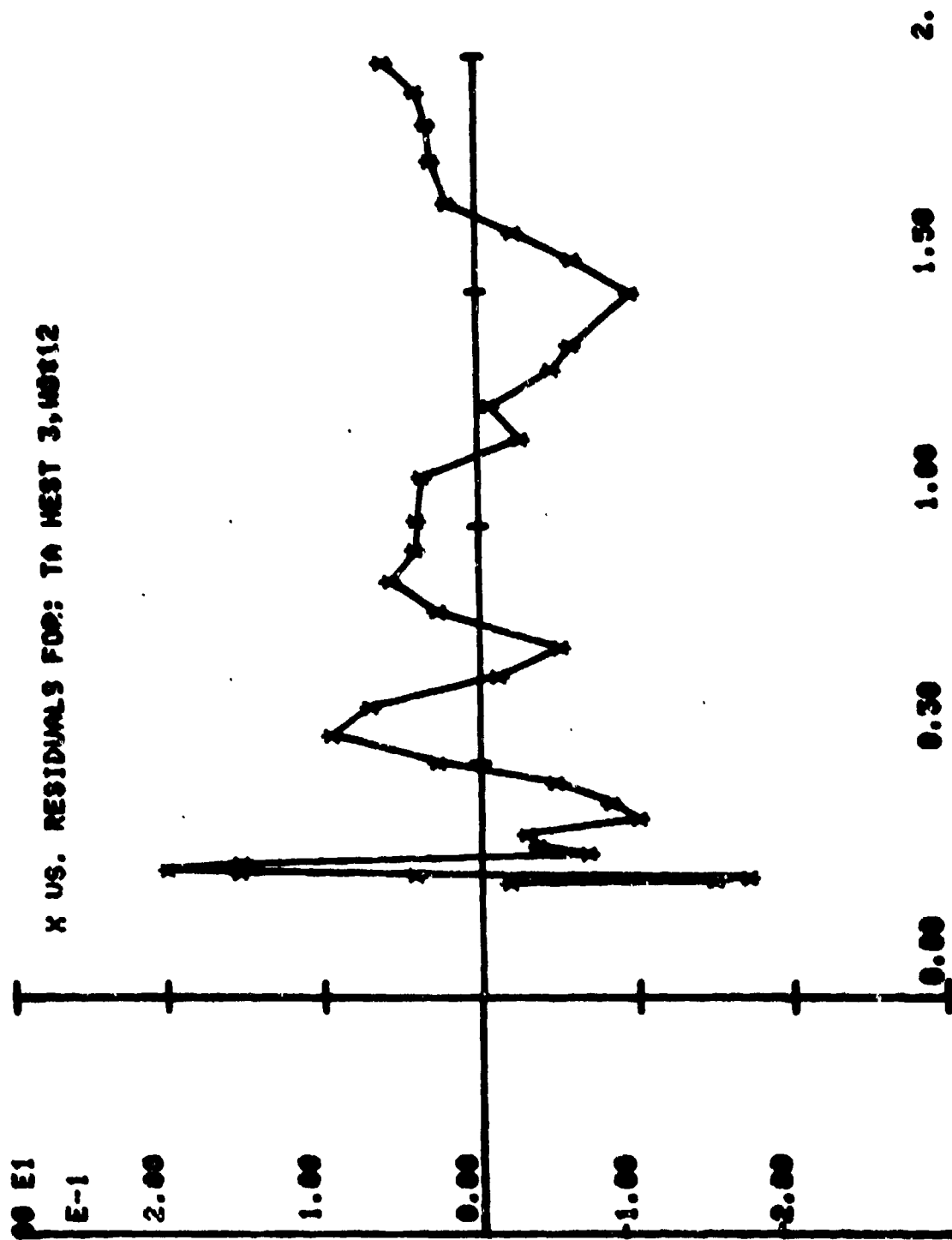




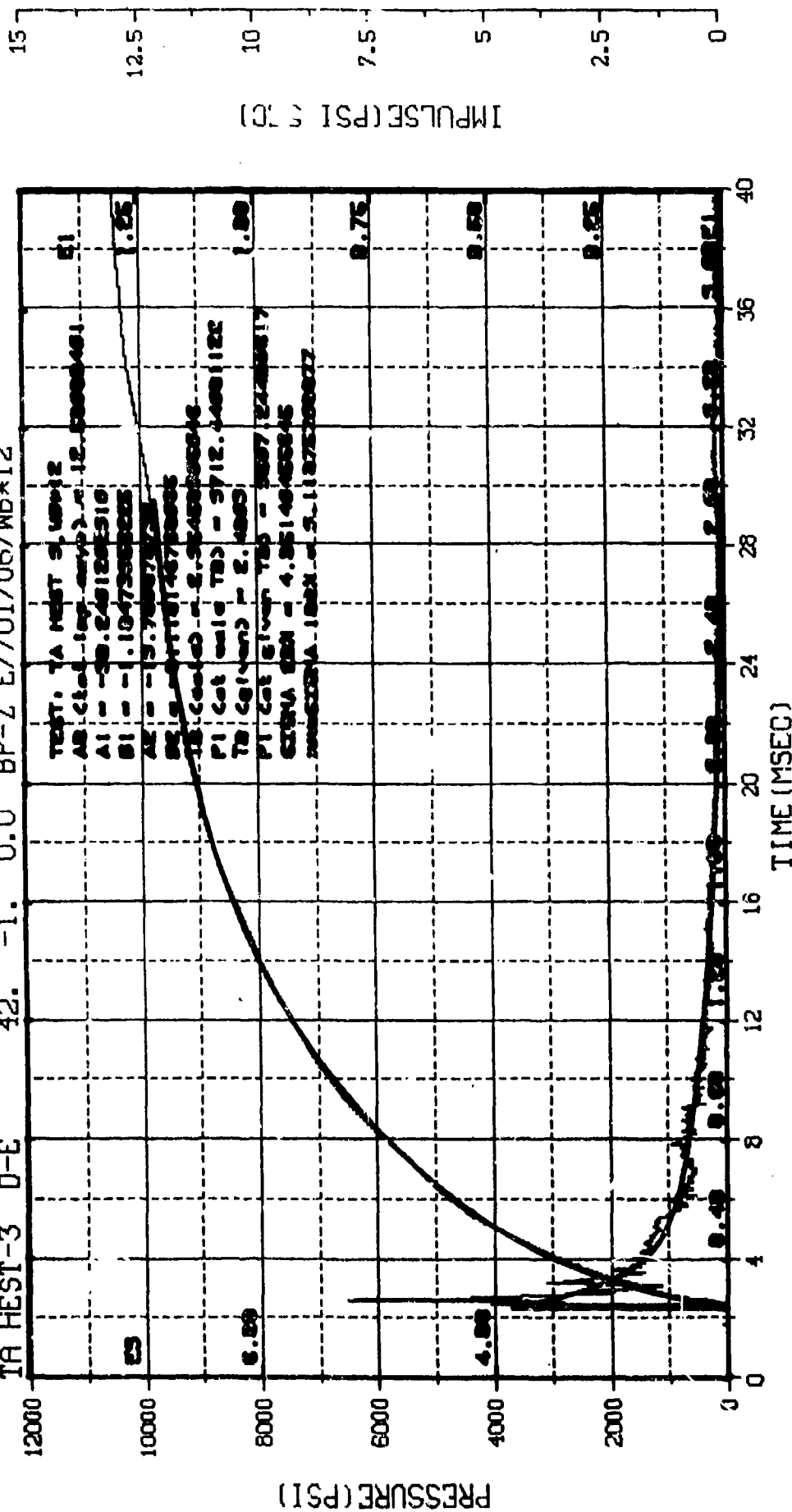


M.N. - 11 E.U. -0.000, 4222.000 VSN=
 TSKIP=12.640 DIGITS=0.000, 602.500 TAPE22
 S.R. -100.00 KHZ 8 50 AM, 2 MAY 78. FILE=10

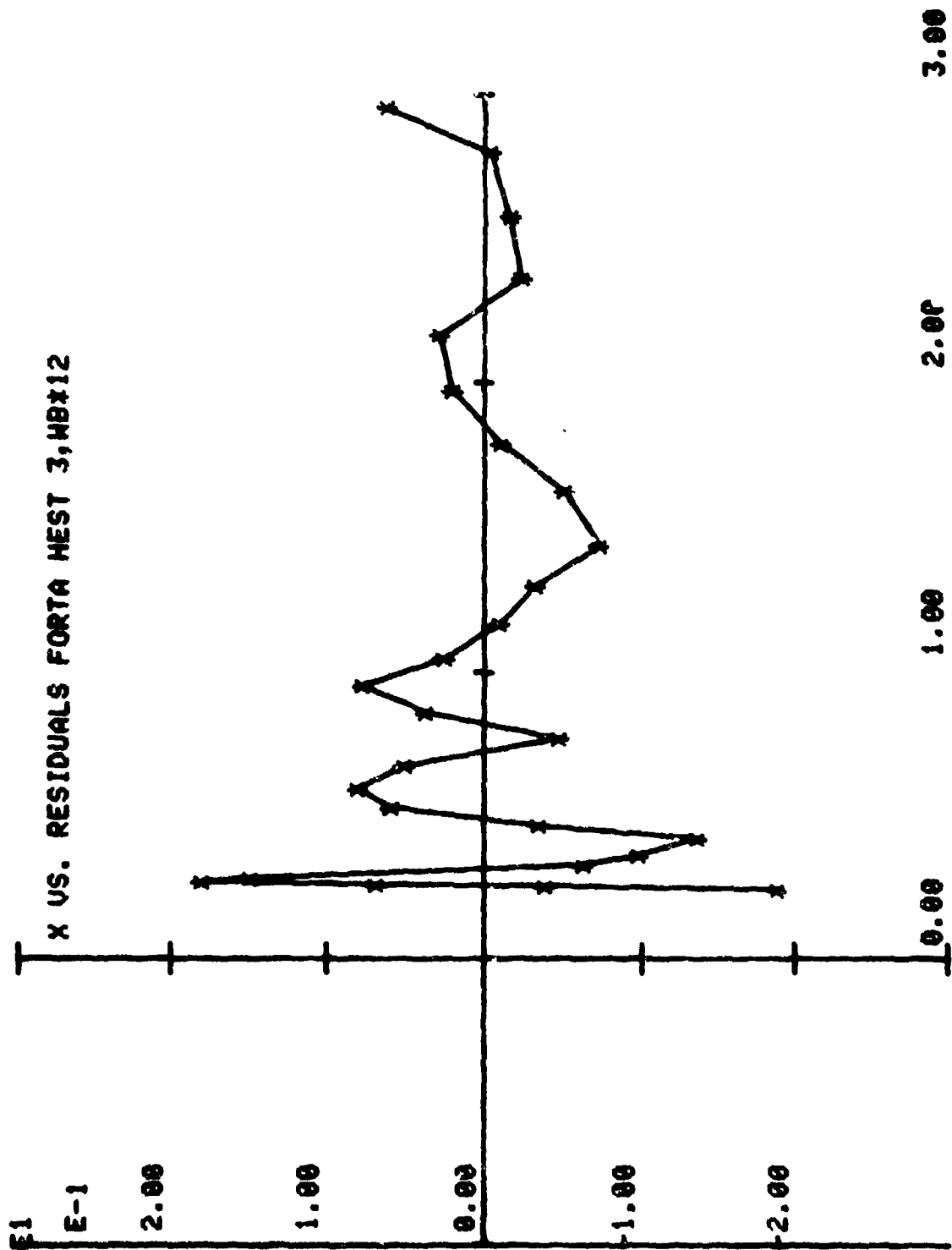


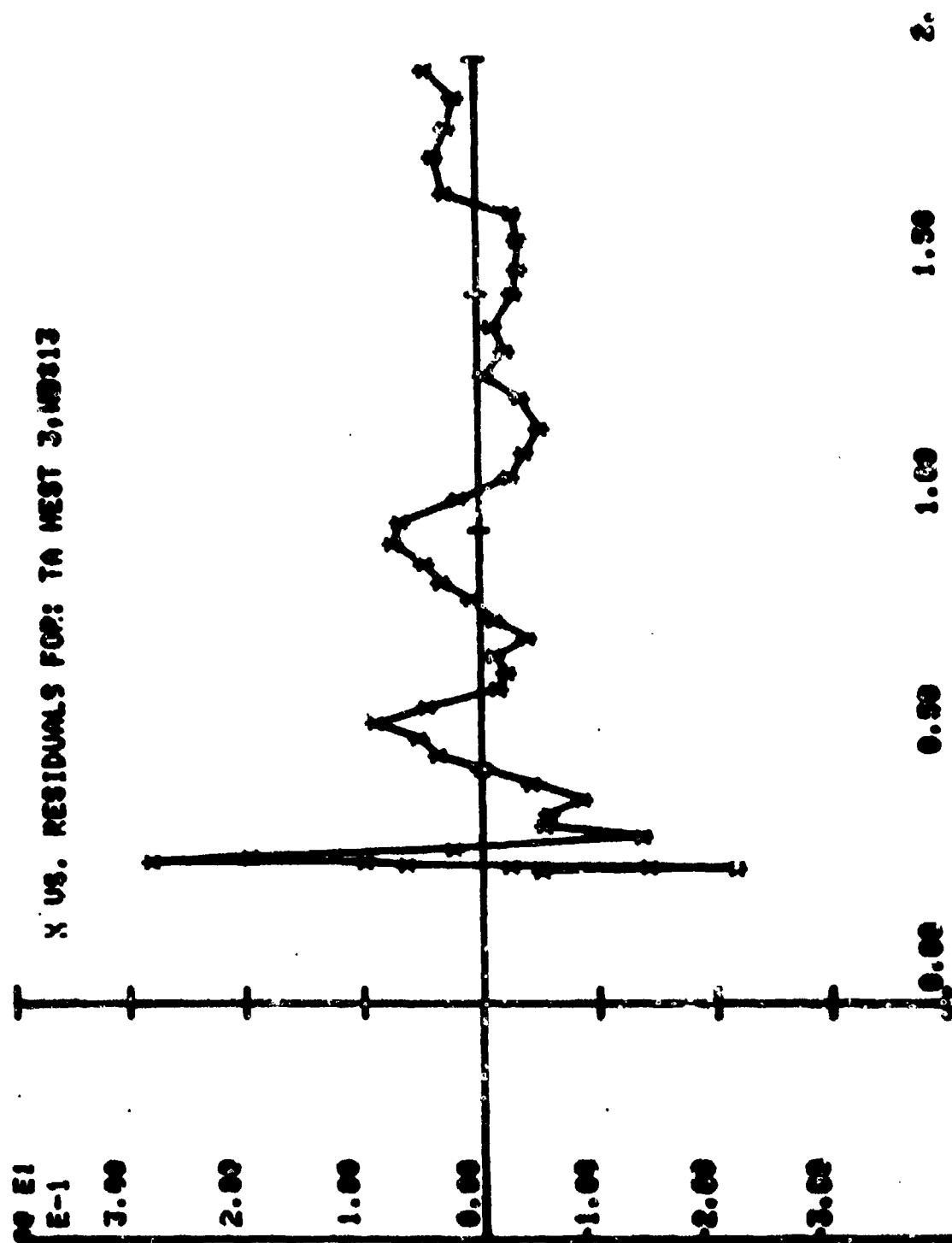


TA HEST-3 D-E 42. -1. 0.0 BP-Z E7/01/06/WBx12

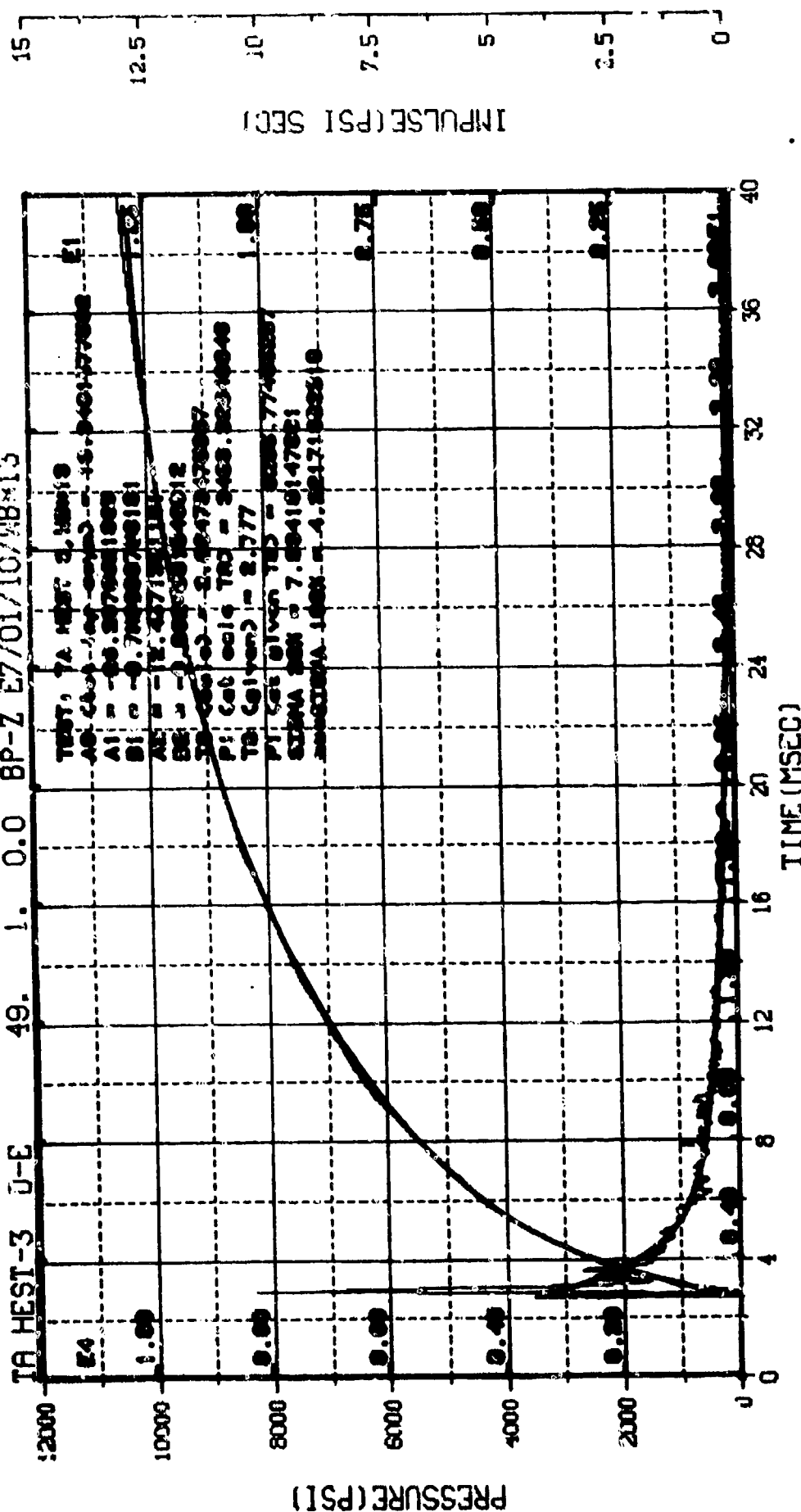


M.N. = 12 E.U. = -0.000,6372.000 VSN=
 TSKIP=12.640 DIGITS=0.000,919.125 TAPE22
 S.R. =100.00 KHZ 8 50 AM, 2 MAY 78. FILE=12

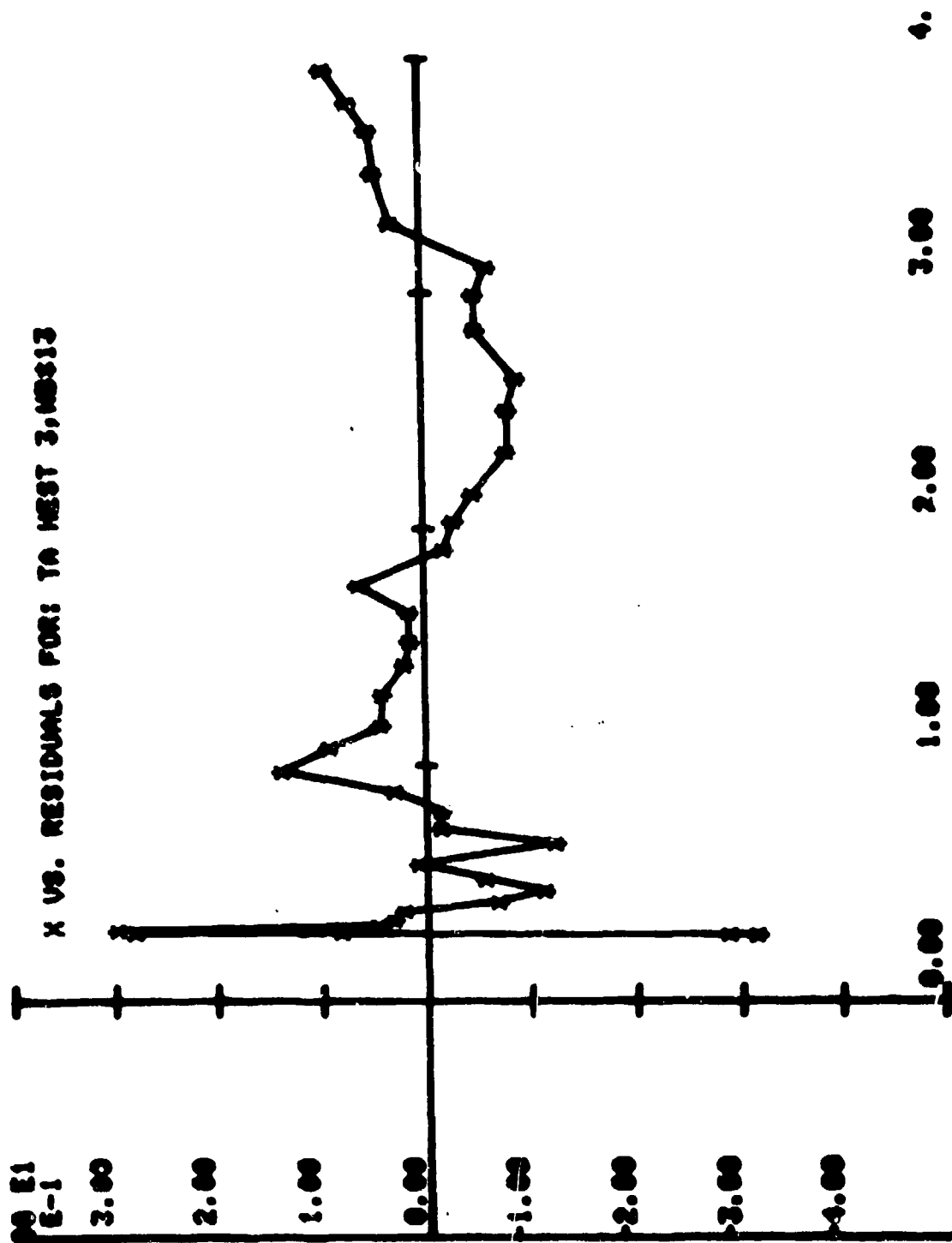


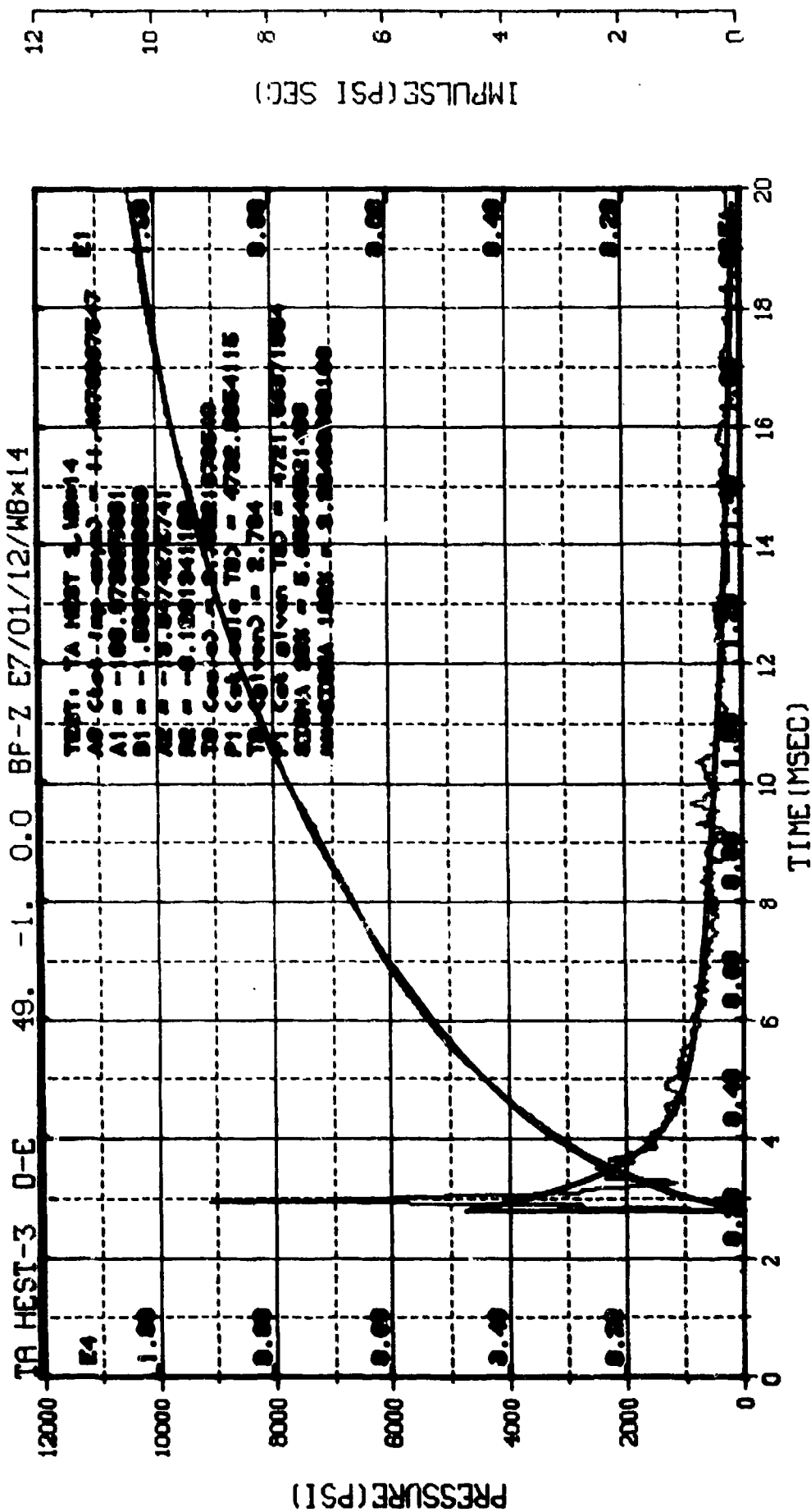


TA HEST-3 U-E 49. 1. 0.0 BP-Z E7/01/10/WB-13

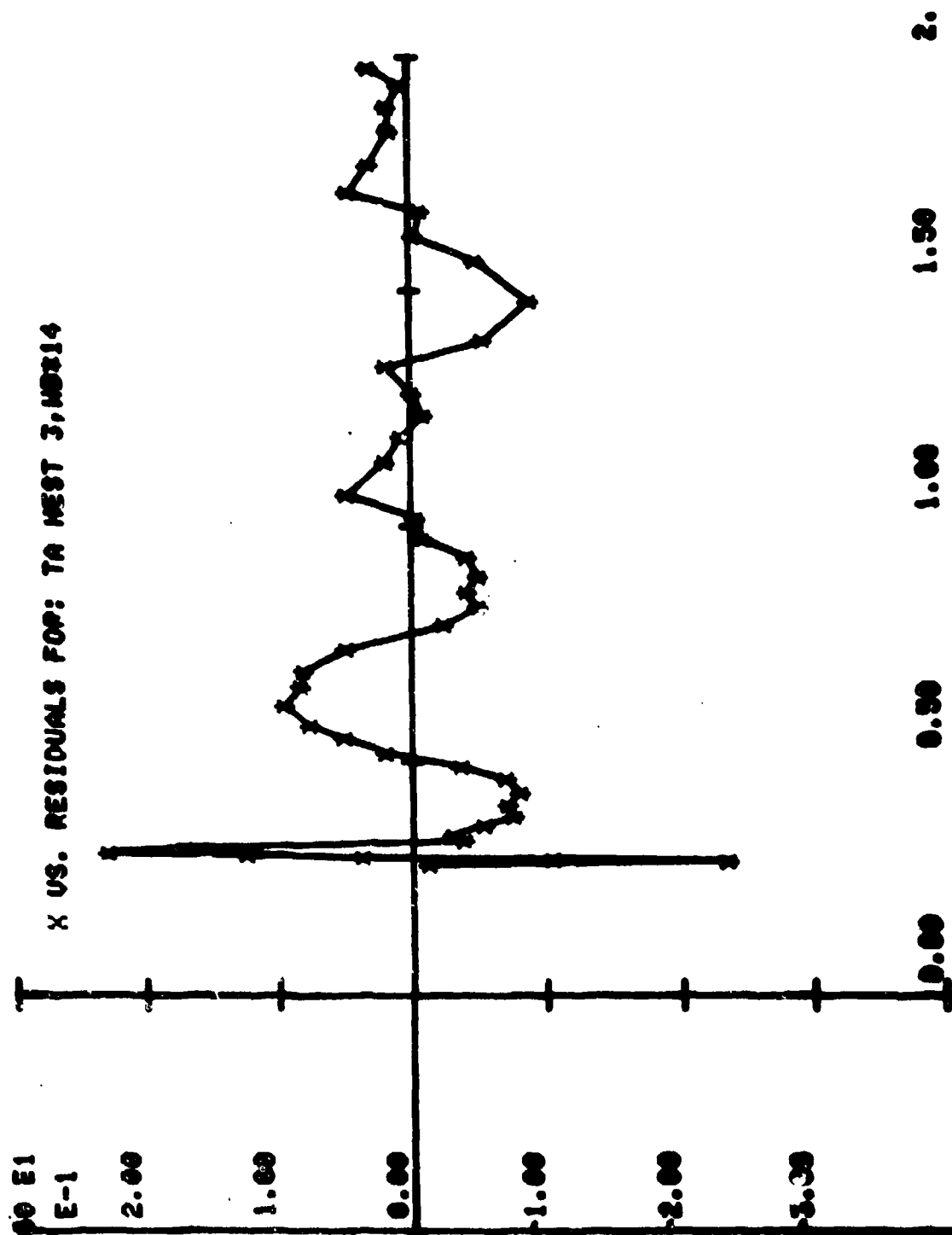


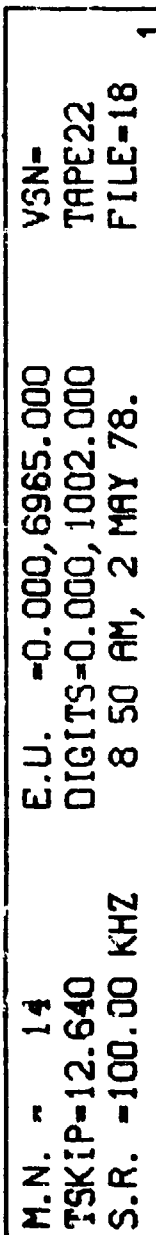
M.N. = 13 E.U. -0.000,6602.000 VSN=
 TSKIP=12.640 DIGITS=0.000,970.000 TAPE22
 S.R. -100.00 KHZ 8 50 AM, 2 MAY 78. FILE=14

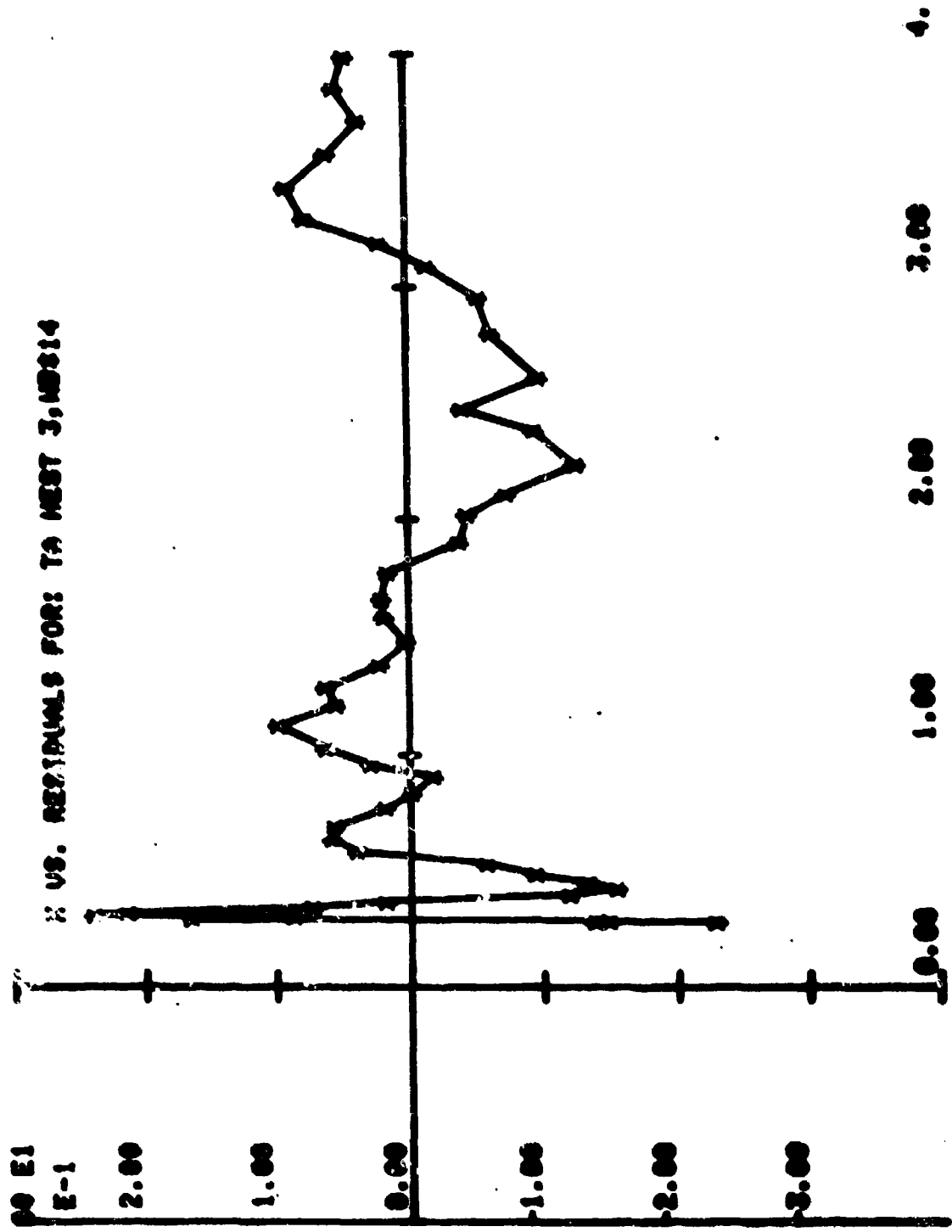


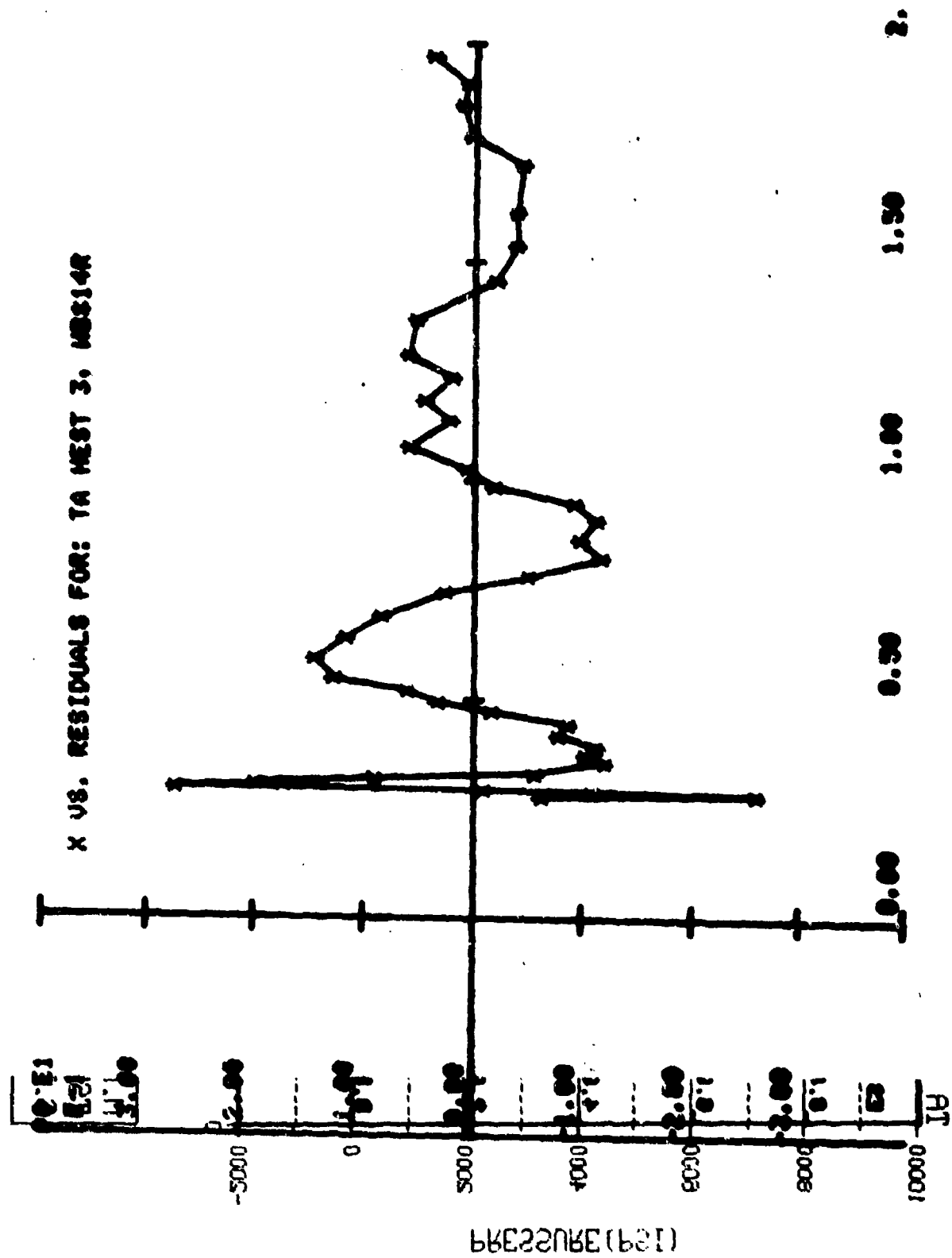


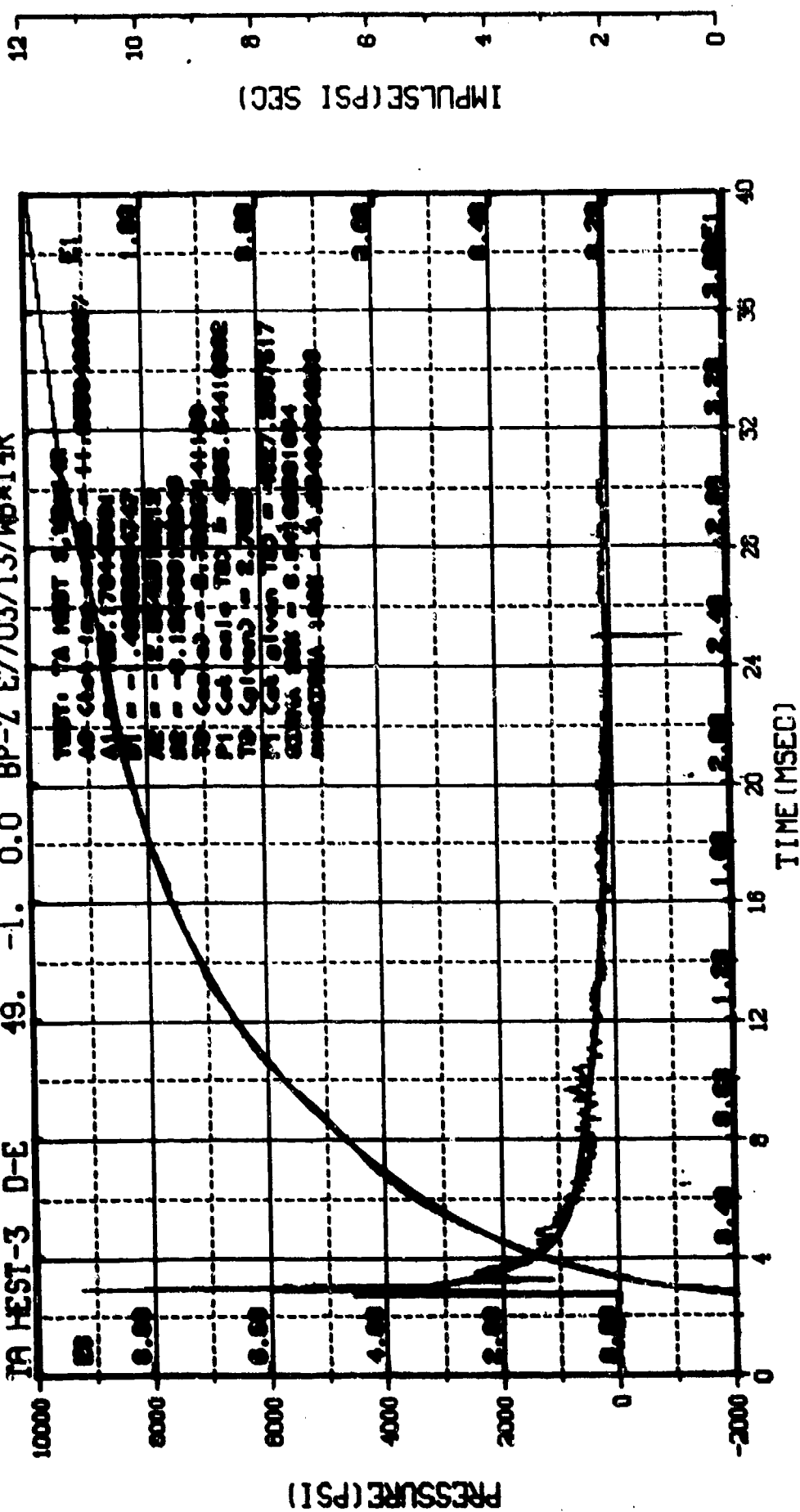
M.N. - 14
TSKIP-12.640
S.R. -100.00 KHZ
E.U. -0.000, 6965.000
DIGITS-0.000, 1002.000
8 50 AM, 2 MAY 78.
VS-
TAPE22
FILE-18



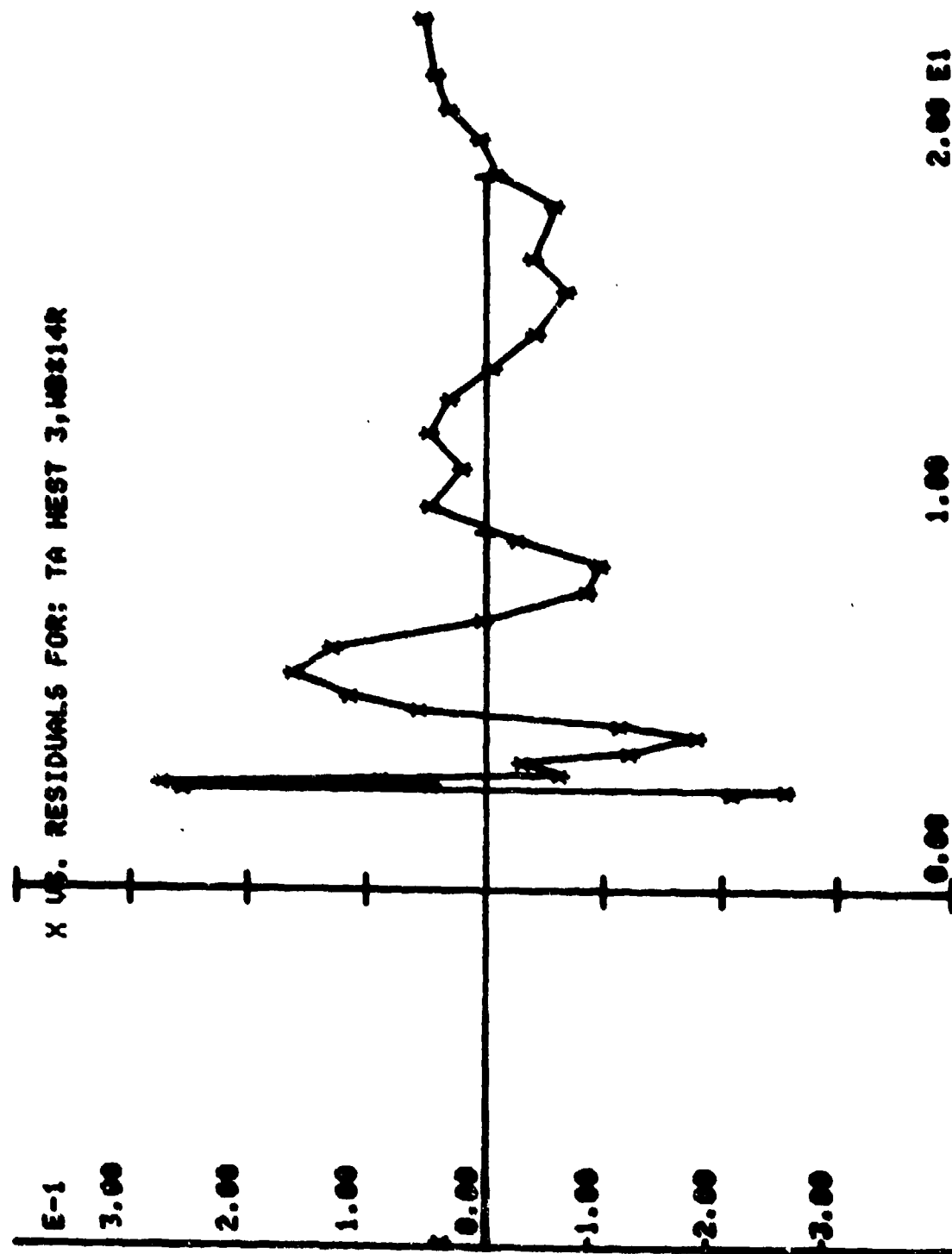




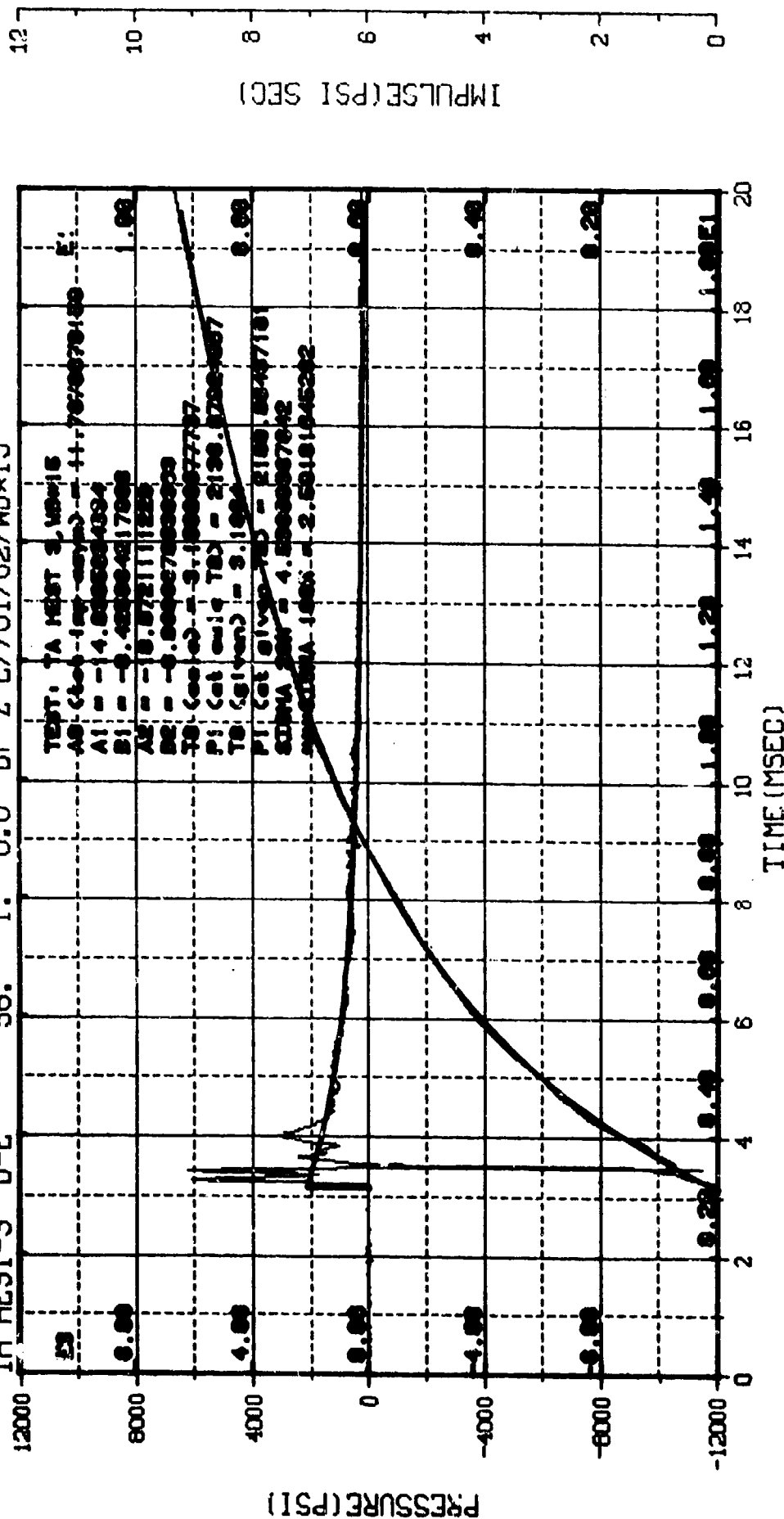




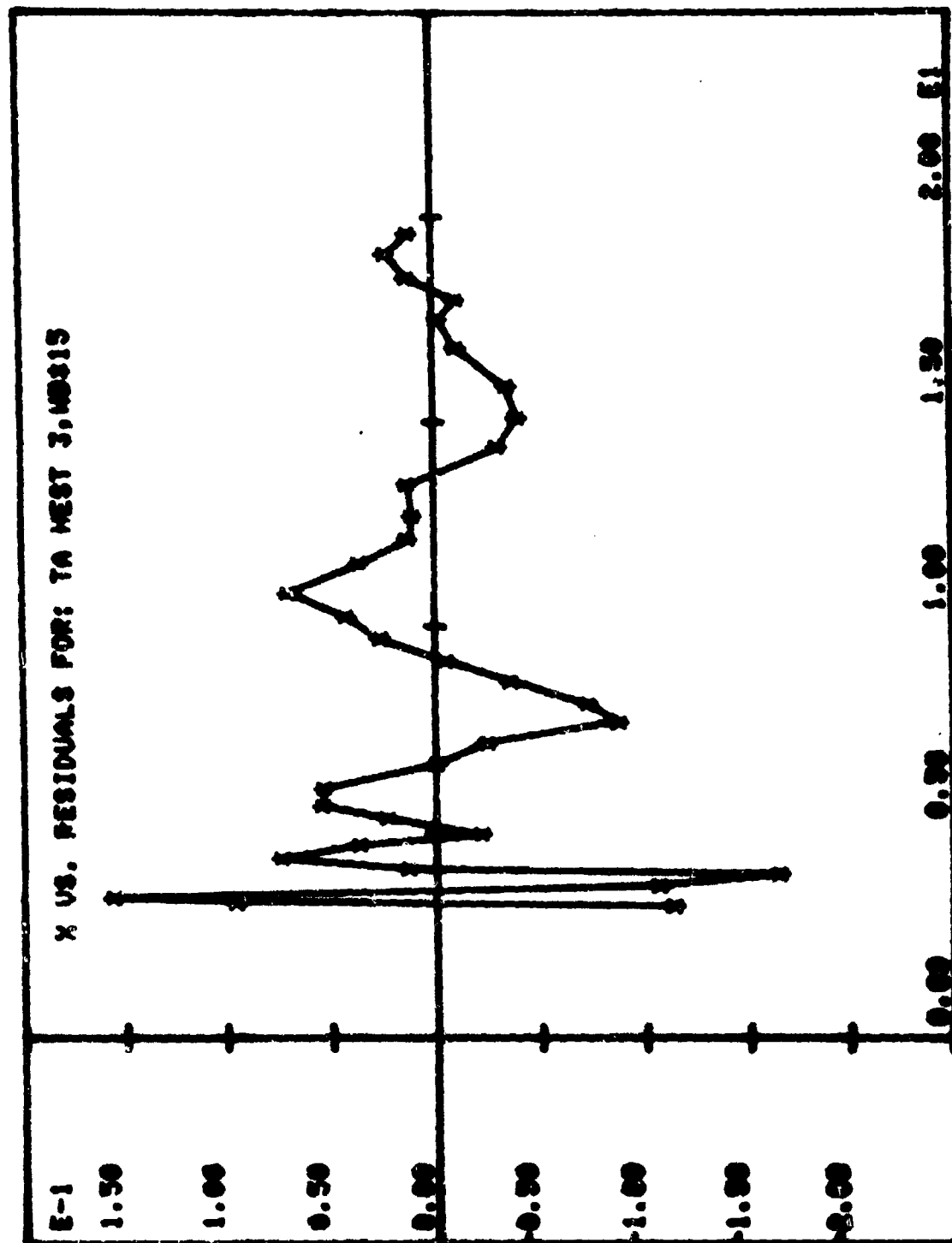
M.N. - 14
TSKIP-12.640
S.R. -100.00 KHZ
E.U. -0.000,6965.000
DIGITS-0.000,614.250
8 50 AM, 2 MAY 78.
VSN-
TAPE22
FILE-28

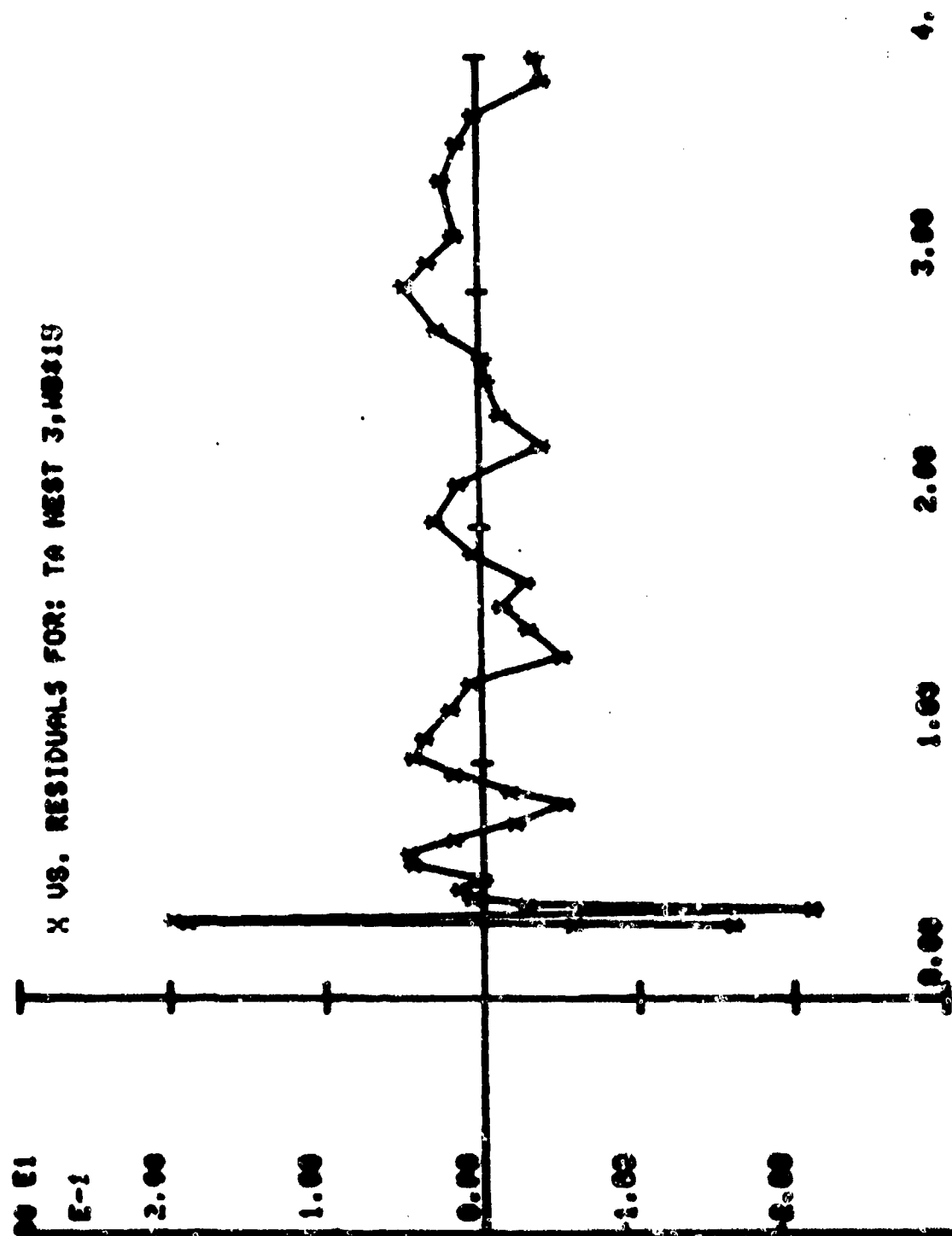


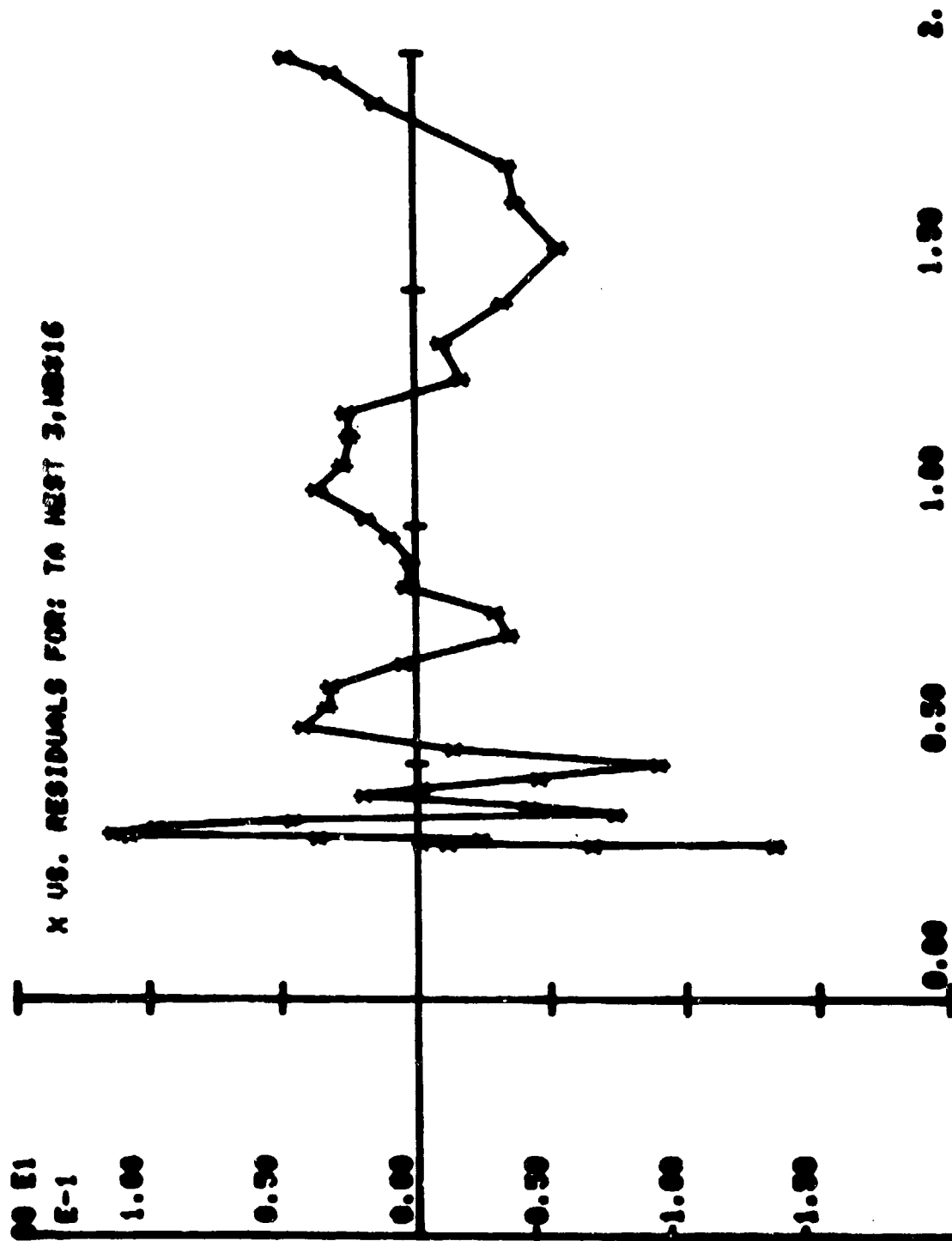
TA HEST-3 D-E 56. 1. 0.0 BP-Z E7/01/02/WB*15



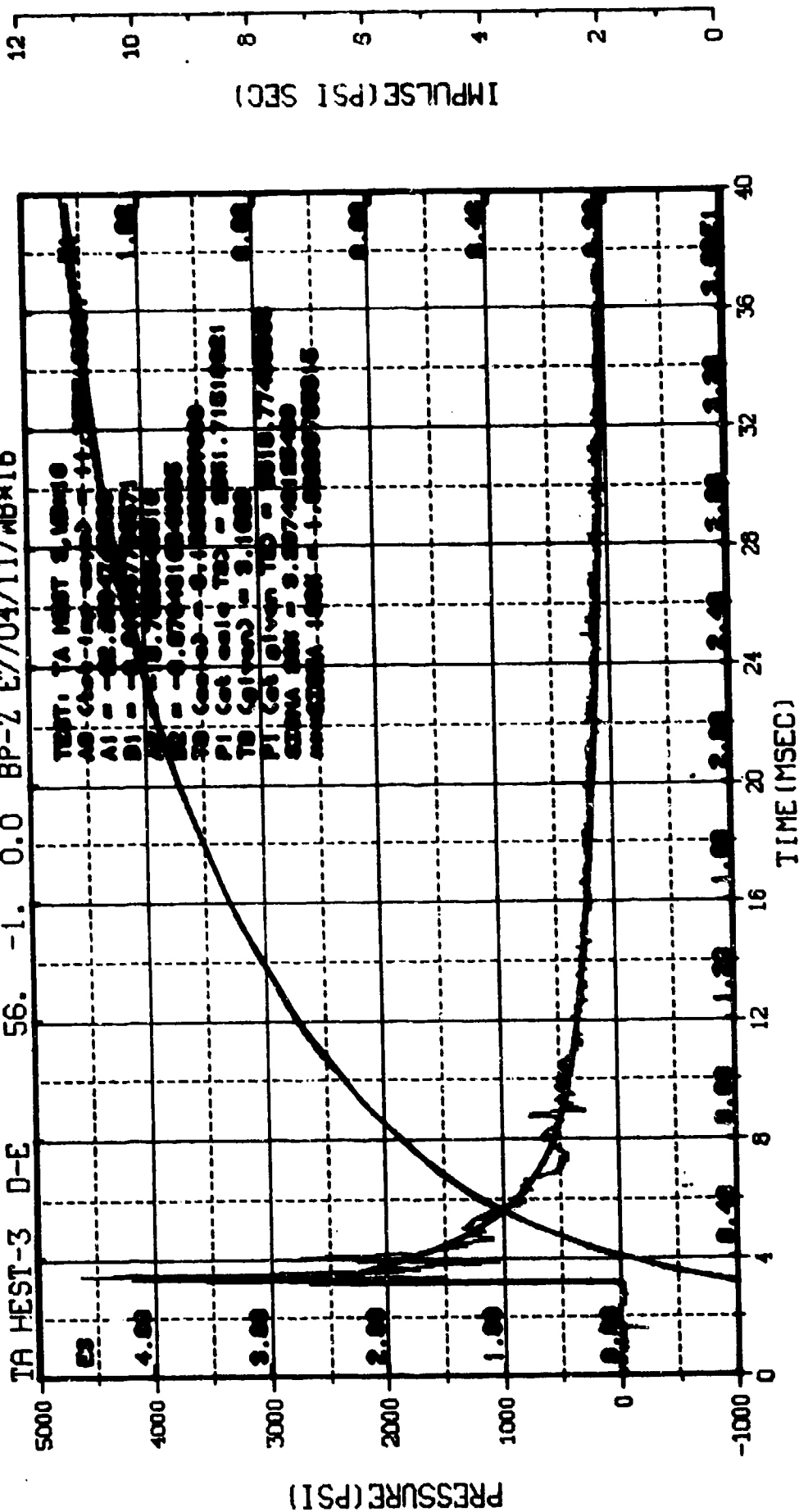
M.N. = 15 E.U. = 0.000,4108.000 VSN=
 TSKIP=12.640 DIGITS=0.000,675.000 TAPE22
 S.R. =100.00 KHZ 8 50 AM, 2 MAY 78. FILE=4



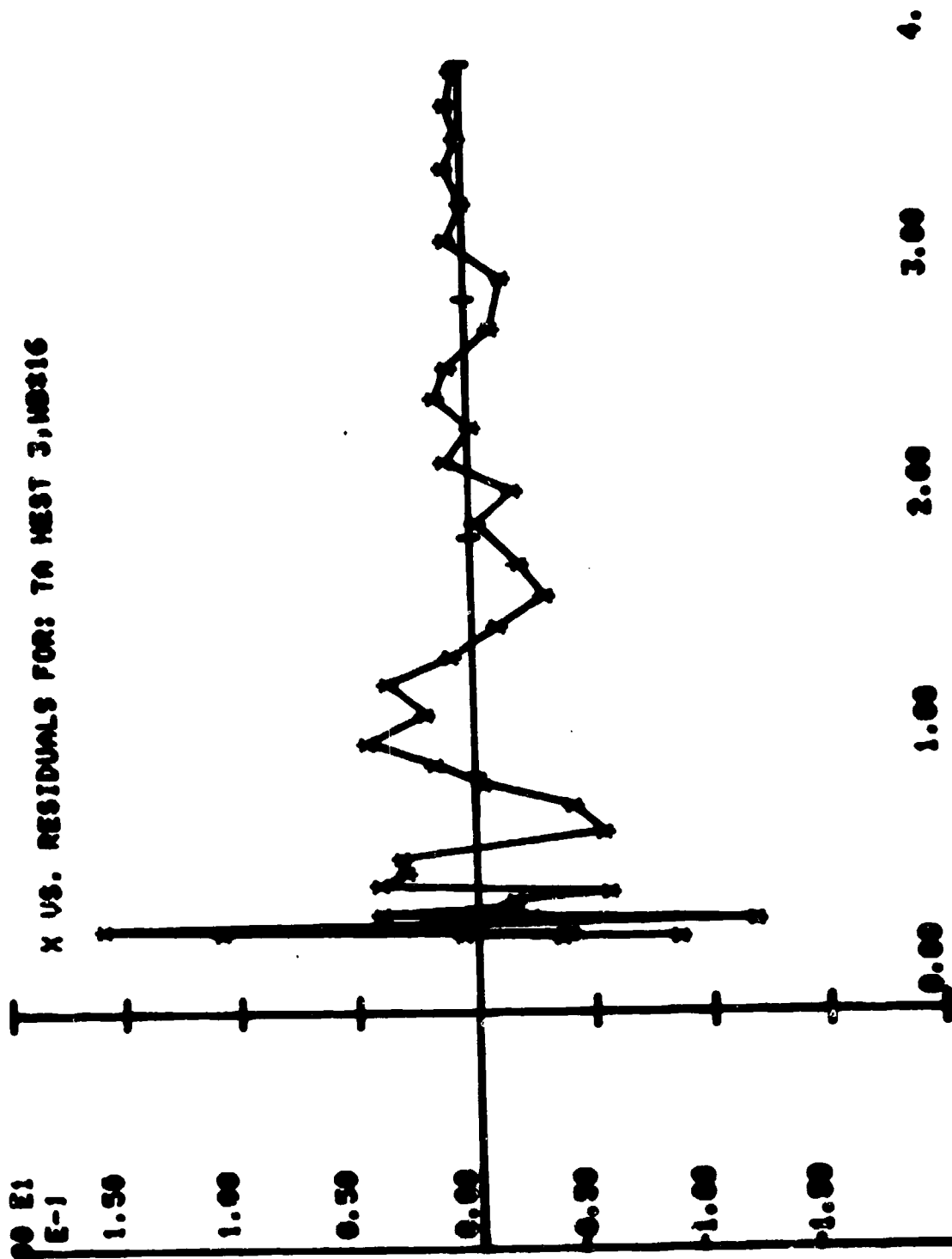


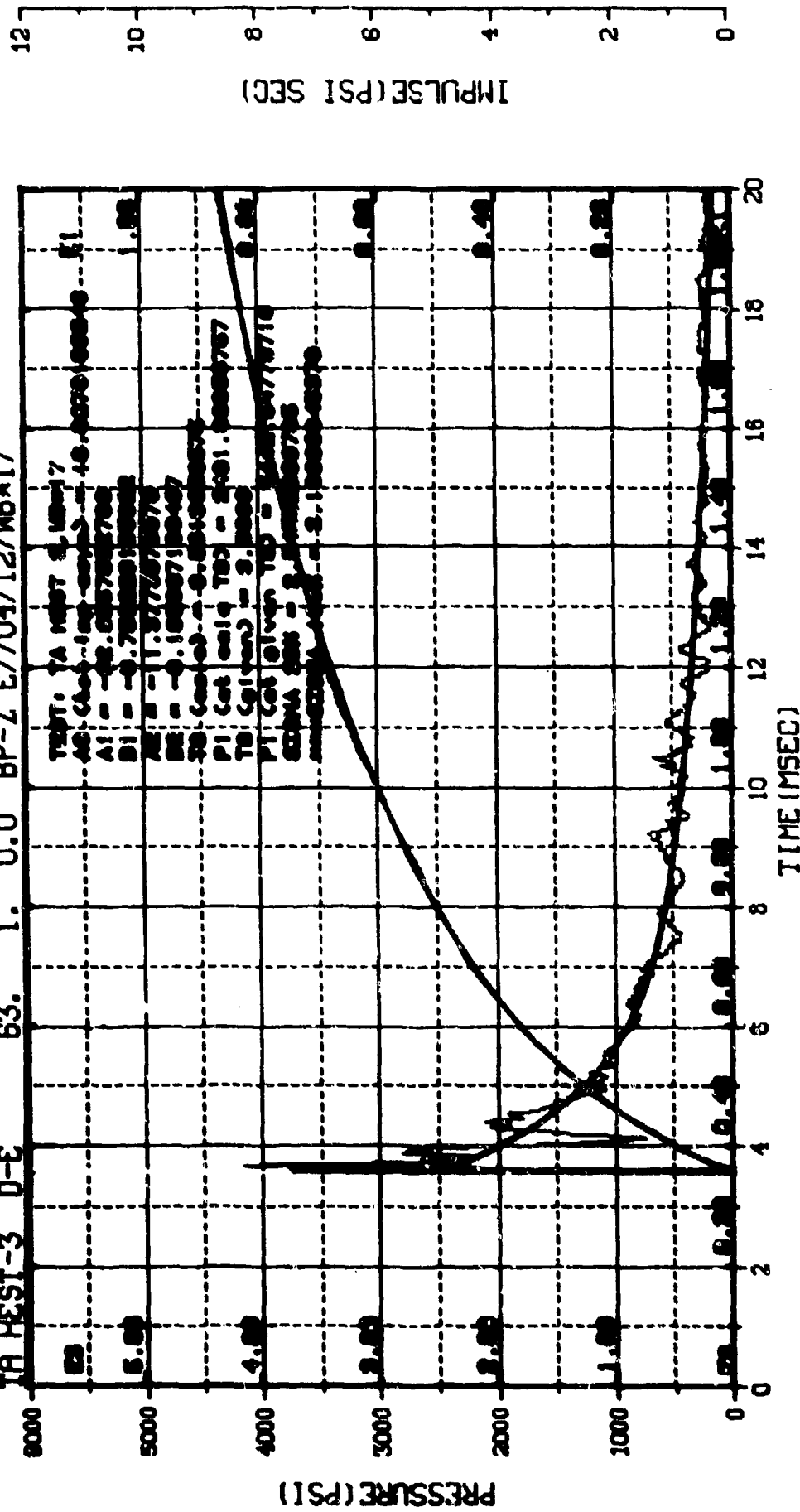


TA HEST-3 D-E -1. 0.0 BP-Z E7/04/11/WBx16



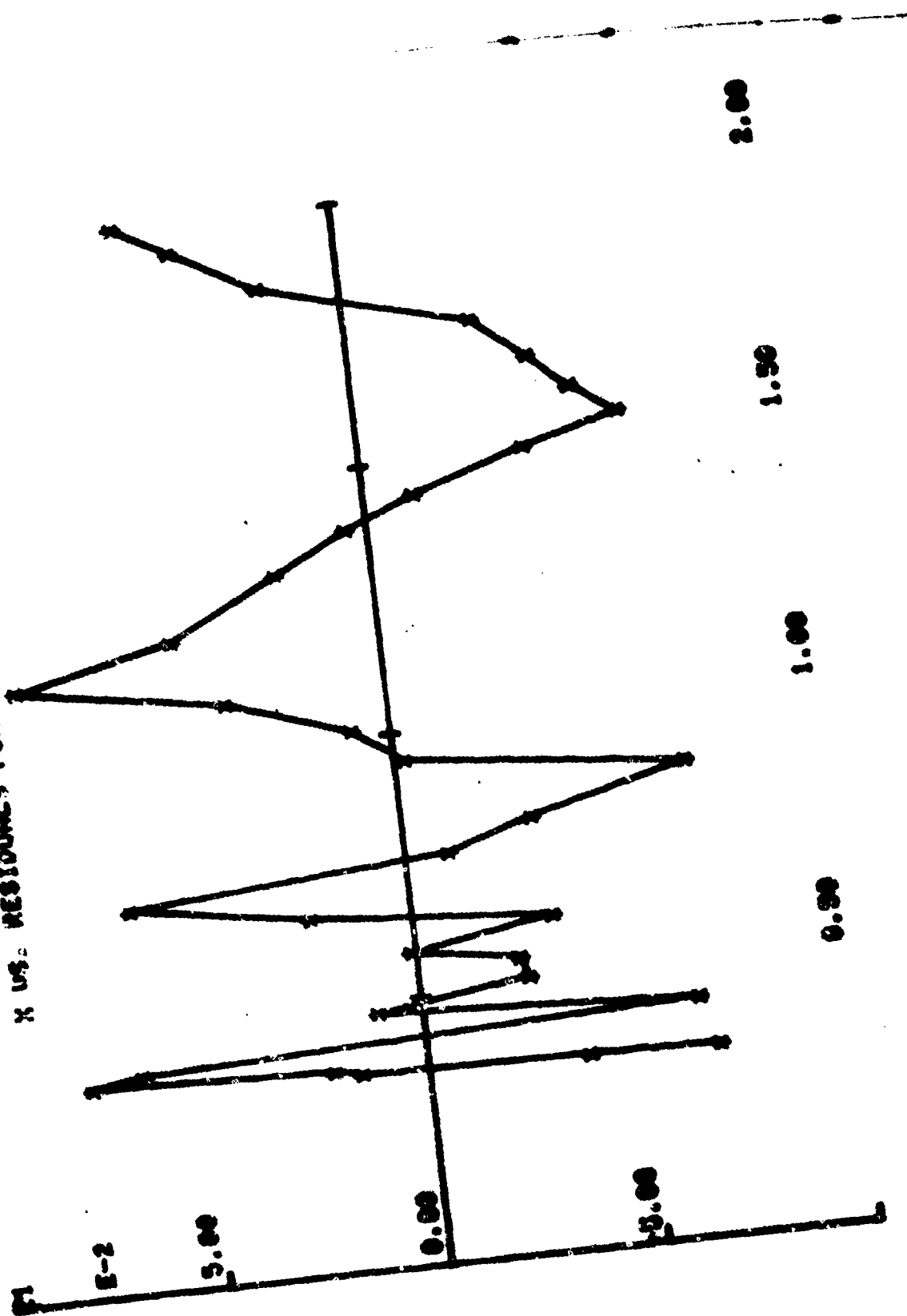
M.N. = 16 E.U. -0.000,4093.000 VSN=
 TSKIP=12.650 DIGITS=0.000,680.000 TAPE22
 S.R. -100.00 KHZ 8 50 AM, 2 MAY 78. FILE=46



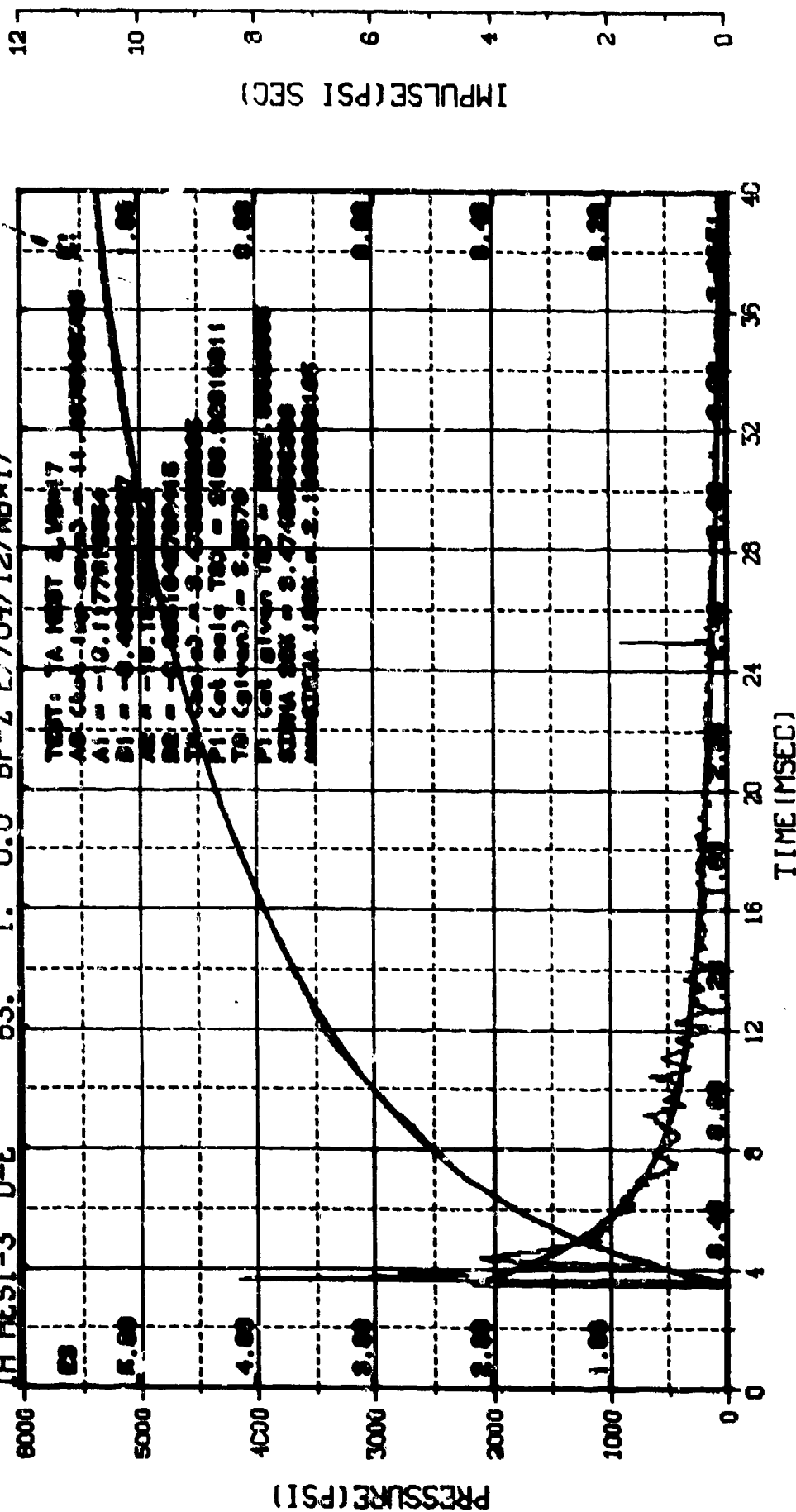


M.N. - 17 E.U. -0.000,4094.000 VSN- ED23
 TSKIP-12.650 DIGITS-0.000,760.750 TAPE22
 S.R. -100.00 KHZ 11 36 AM, 2 MAY 78. FILE-48
 1

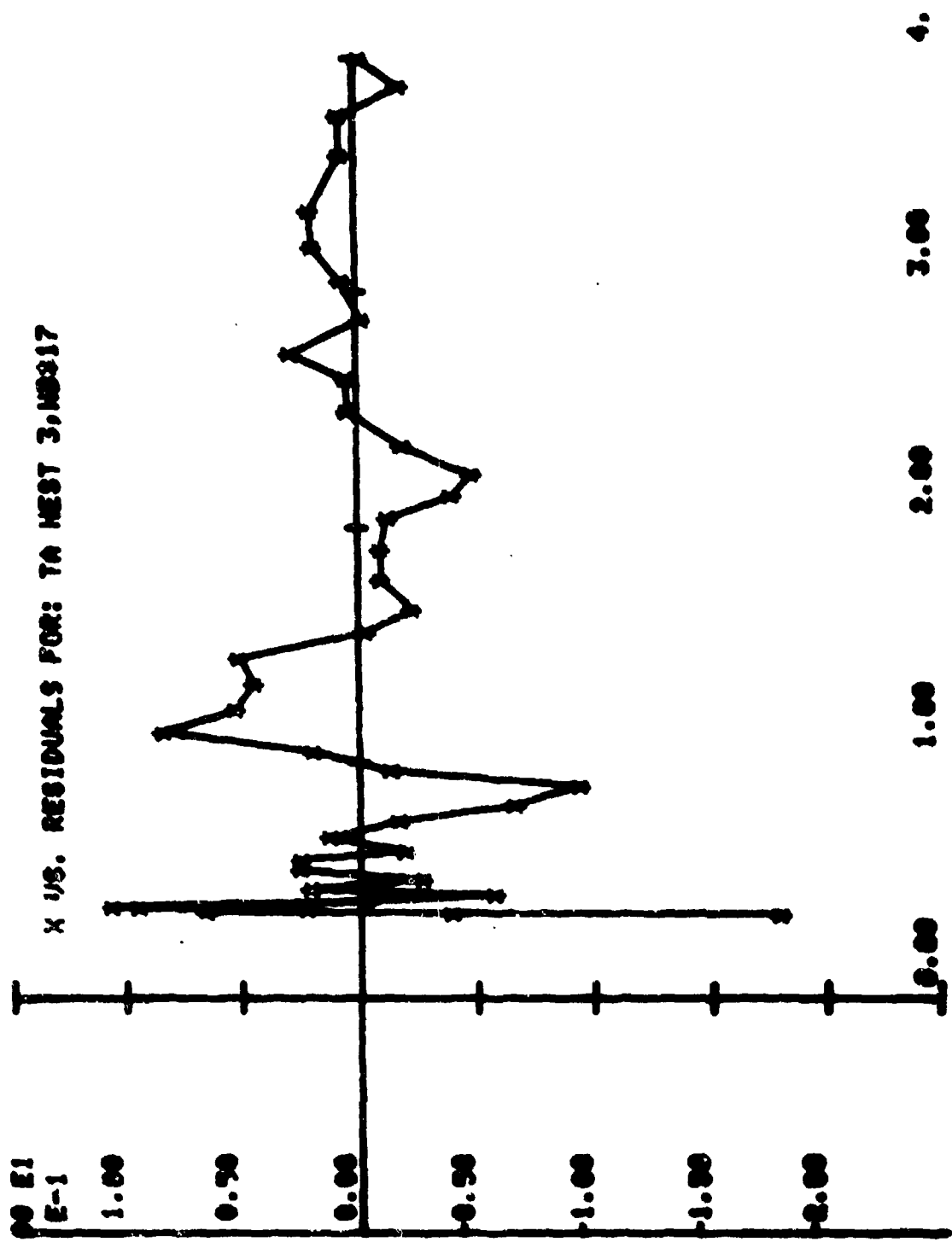
X US: RESIDUALS FOR: TA WEST 3, M0817

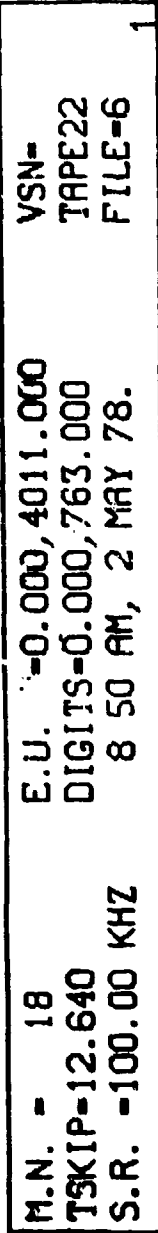


TA HEST-3 D-E 63. 1. 0.0 BP-Z E7/04/12/NB*17

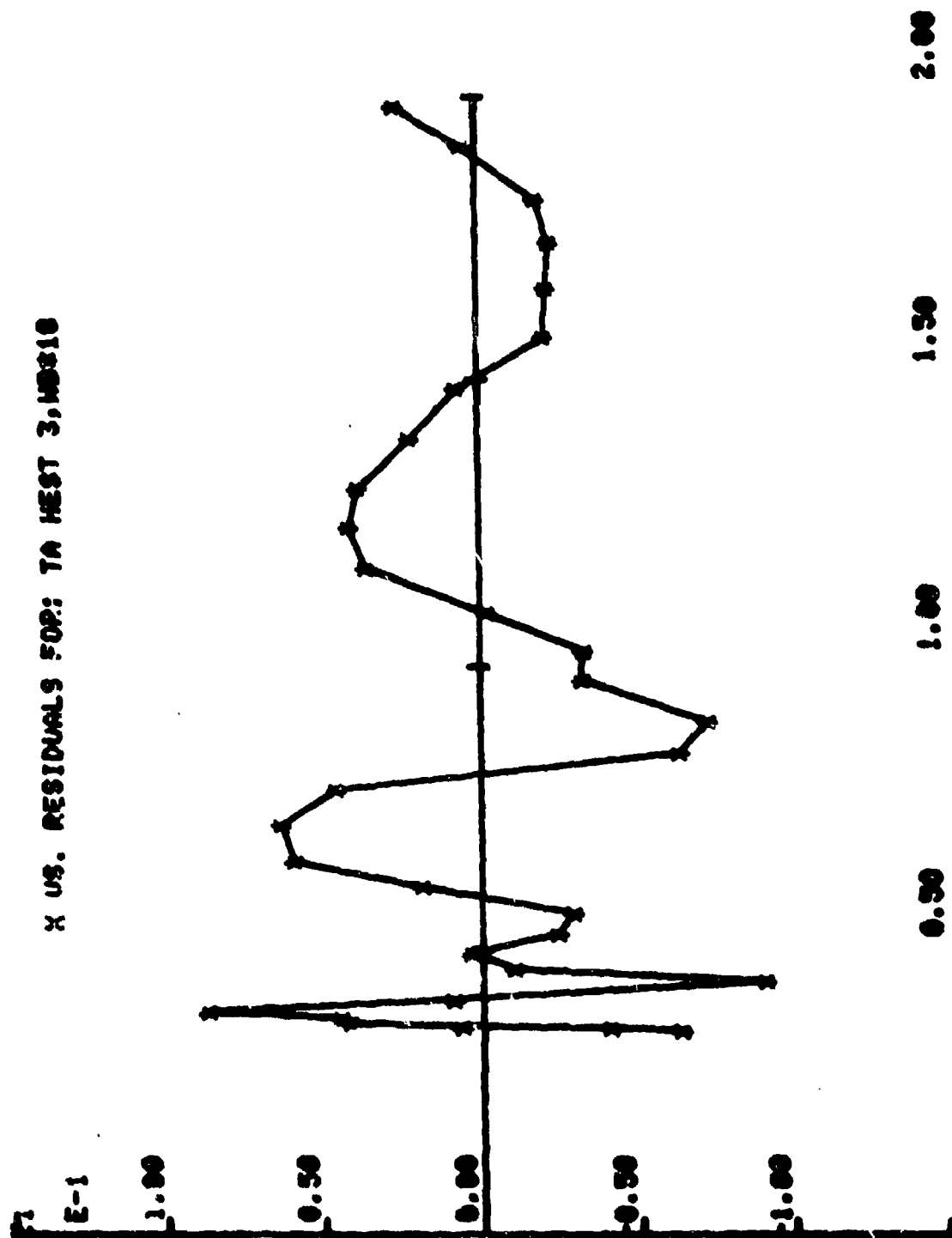


M.N. = 17 E.U. -0.000,4094.000 VSN=
 TSKIP-12.650 DIGITS-0.000,760.750 TAPE22
 S.R. -100.00 KHZ 8 50 AM, 2 MAY 78. FILE=48

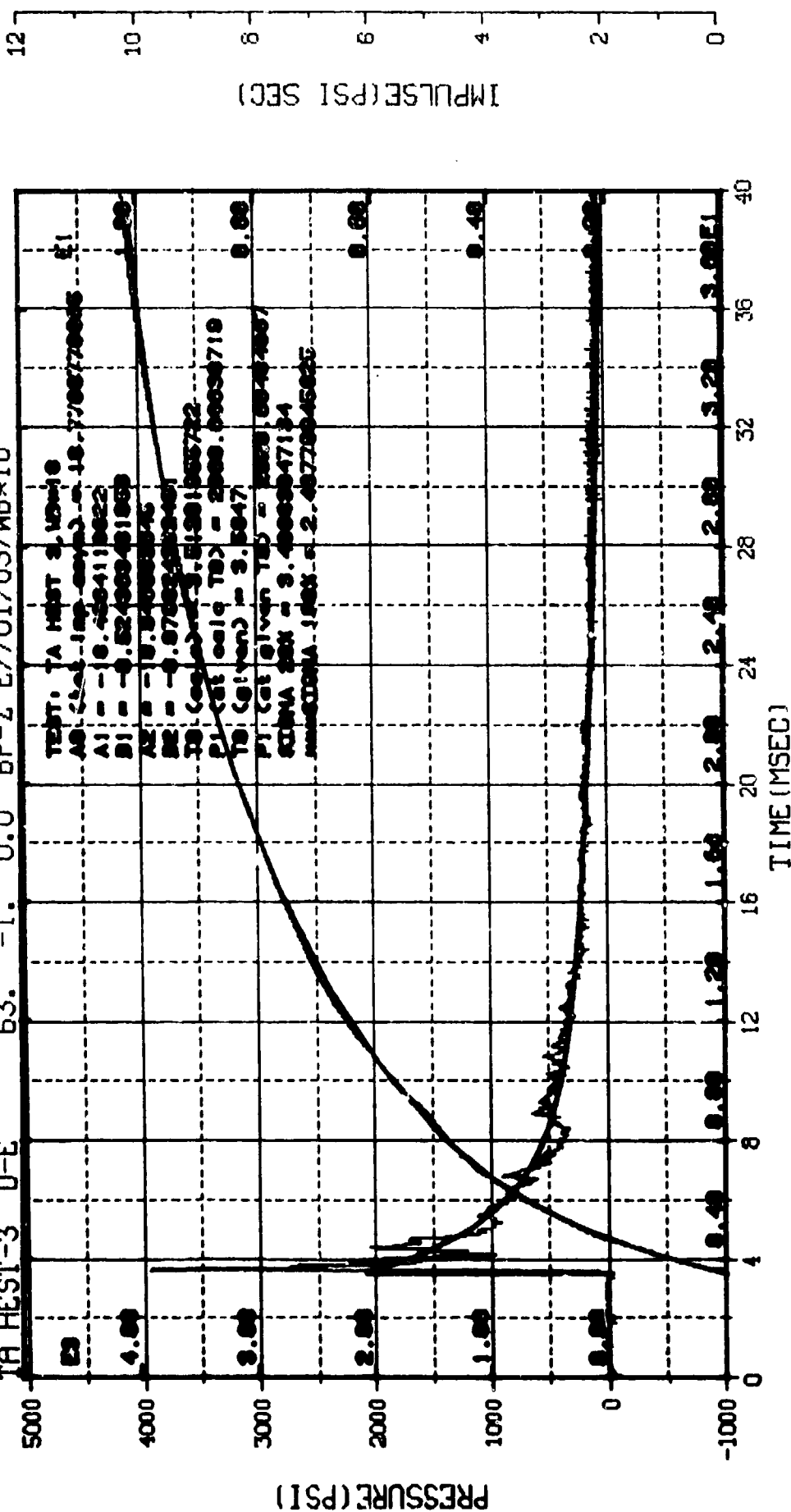




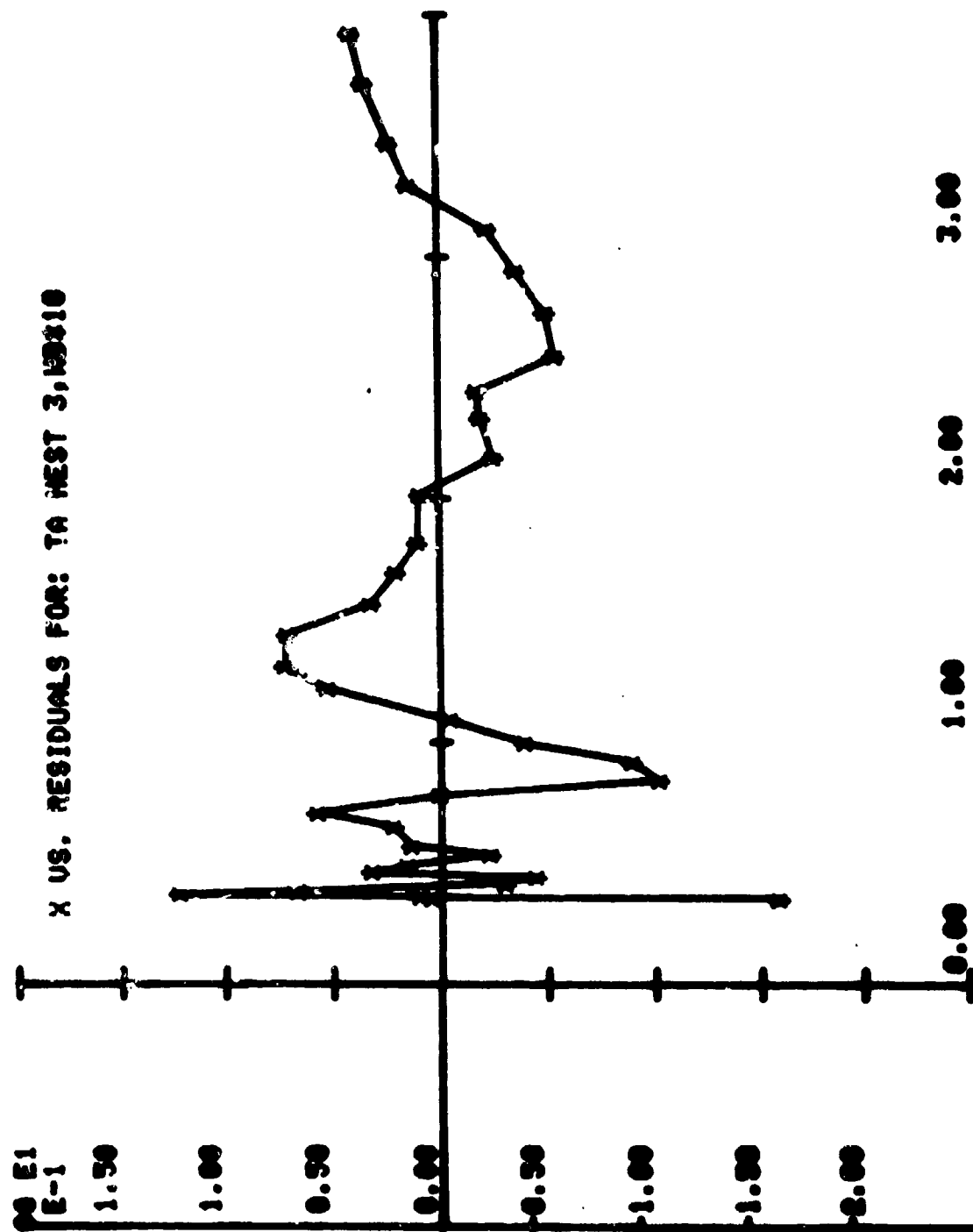
X US. RESIDUALS FOR: TA HEST 3, MD810

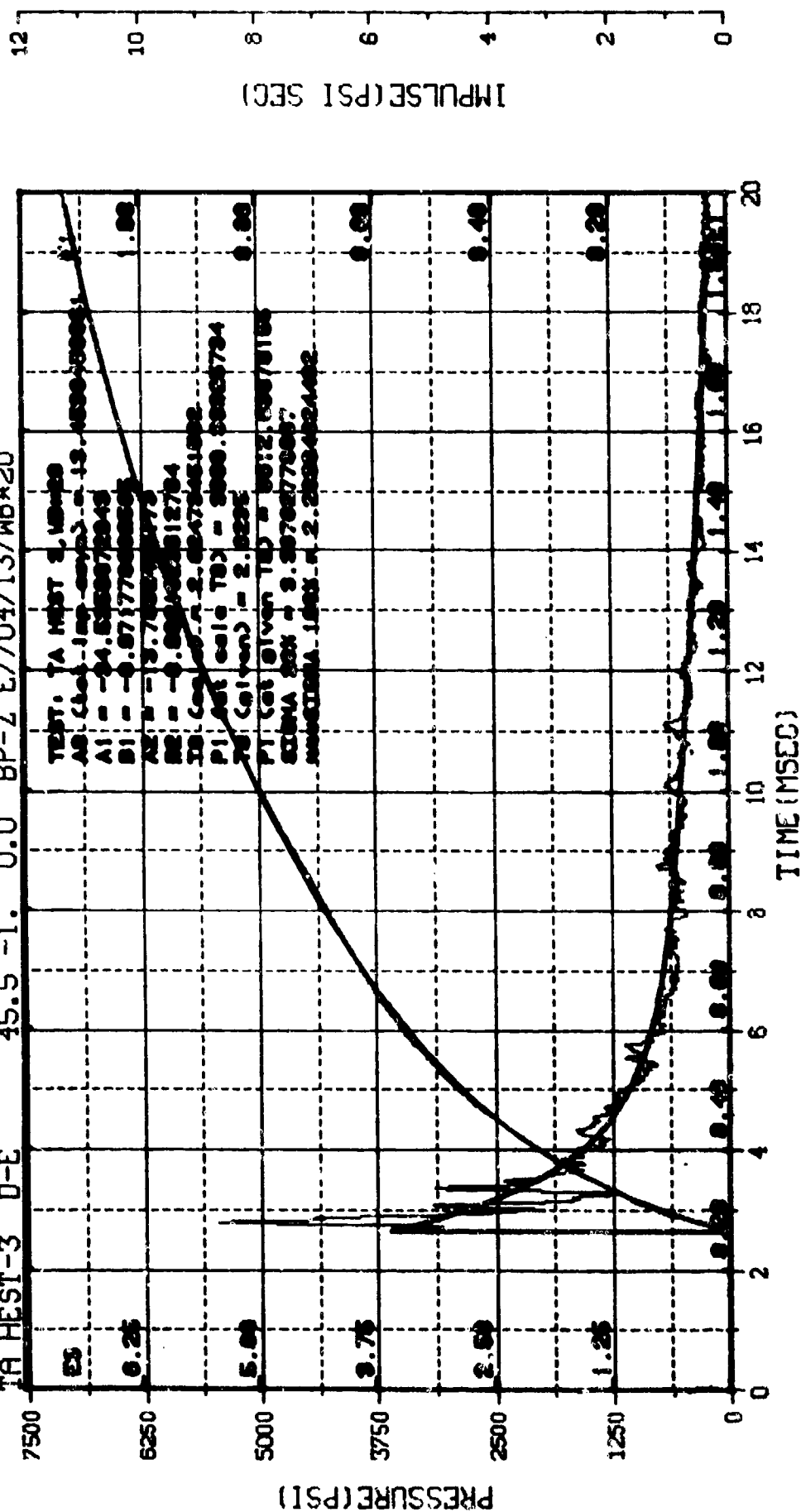


TA HEST-3 0-E 63. -1. 0.0 BP-Z E7/01/03/WB*18

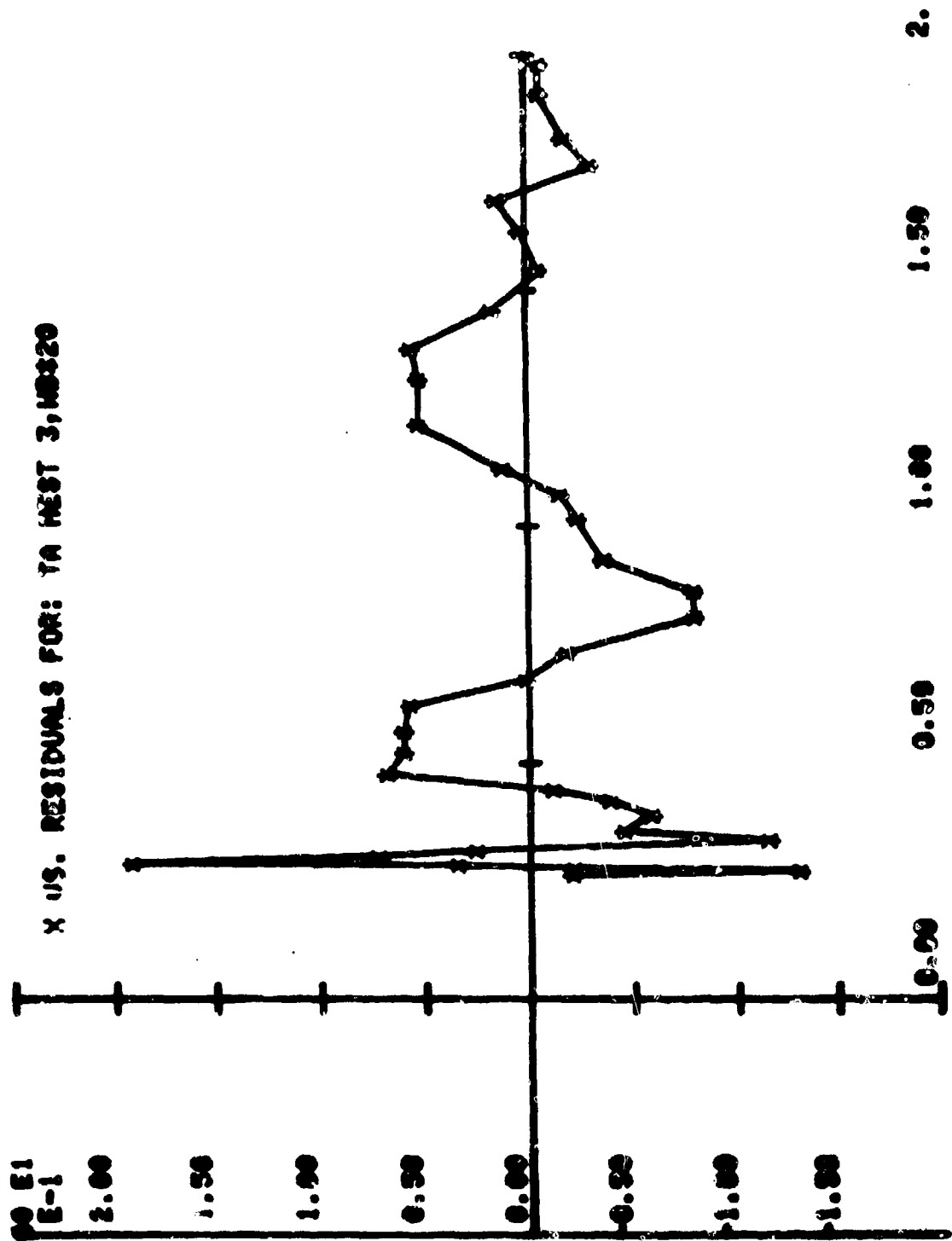


N.N. = 18 E.U. = 0.000,4011.000 VSN=
 TSKIP=12.640 DIGITS=0.000,753.000 TAPE22
 S.R. =100.00 KHZ 8 50 AM, 2 MAY 78. FILE=6

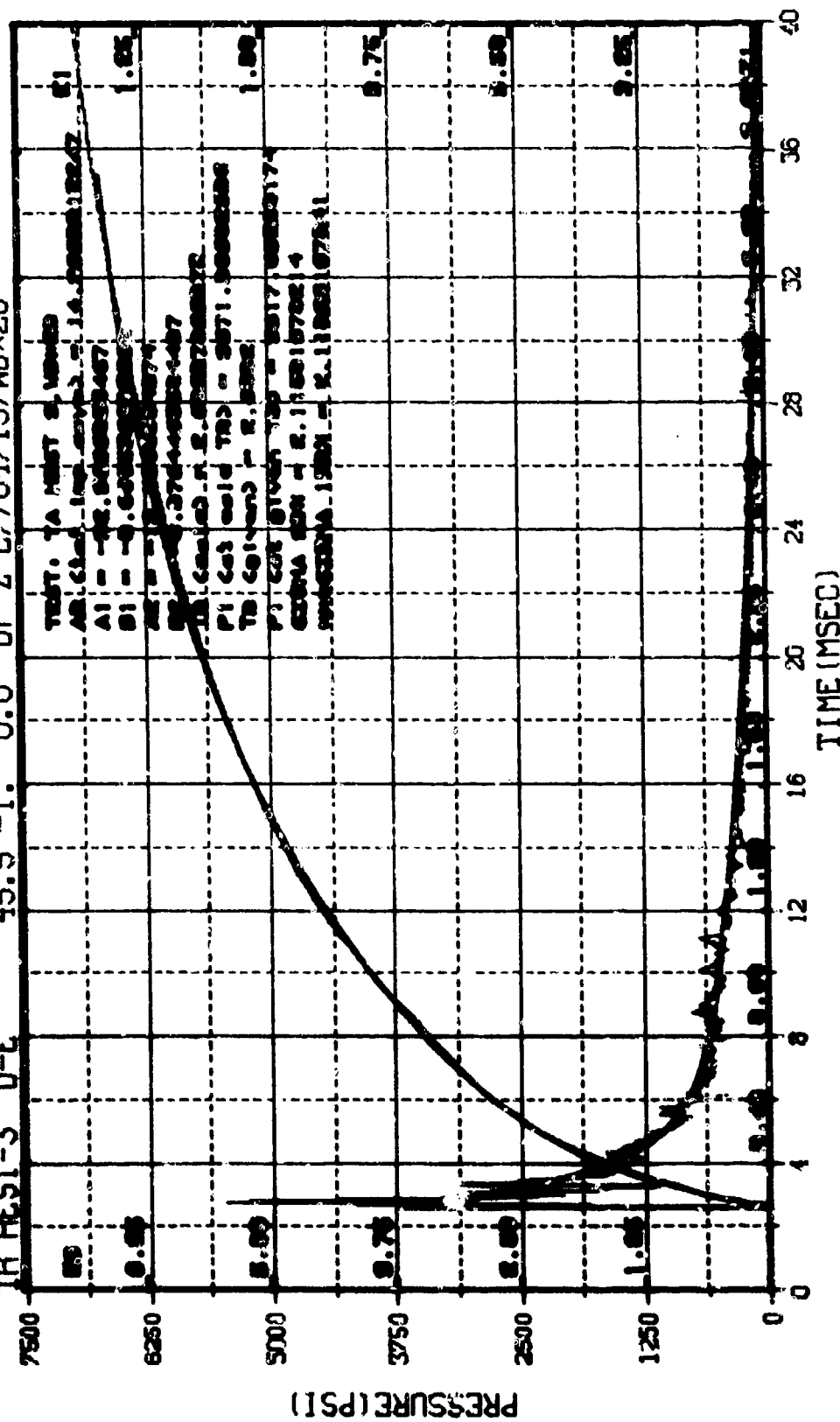




M.N. - 20	E.U. -0.000,4175.000	VSN- ED23
TSKIP-12.650	DIGITS-0.000,614.500	TAPE22
S.R. -100.00 KHZ	11 36 AM, 2 MAY 78.	FILE-50



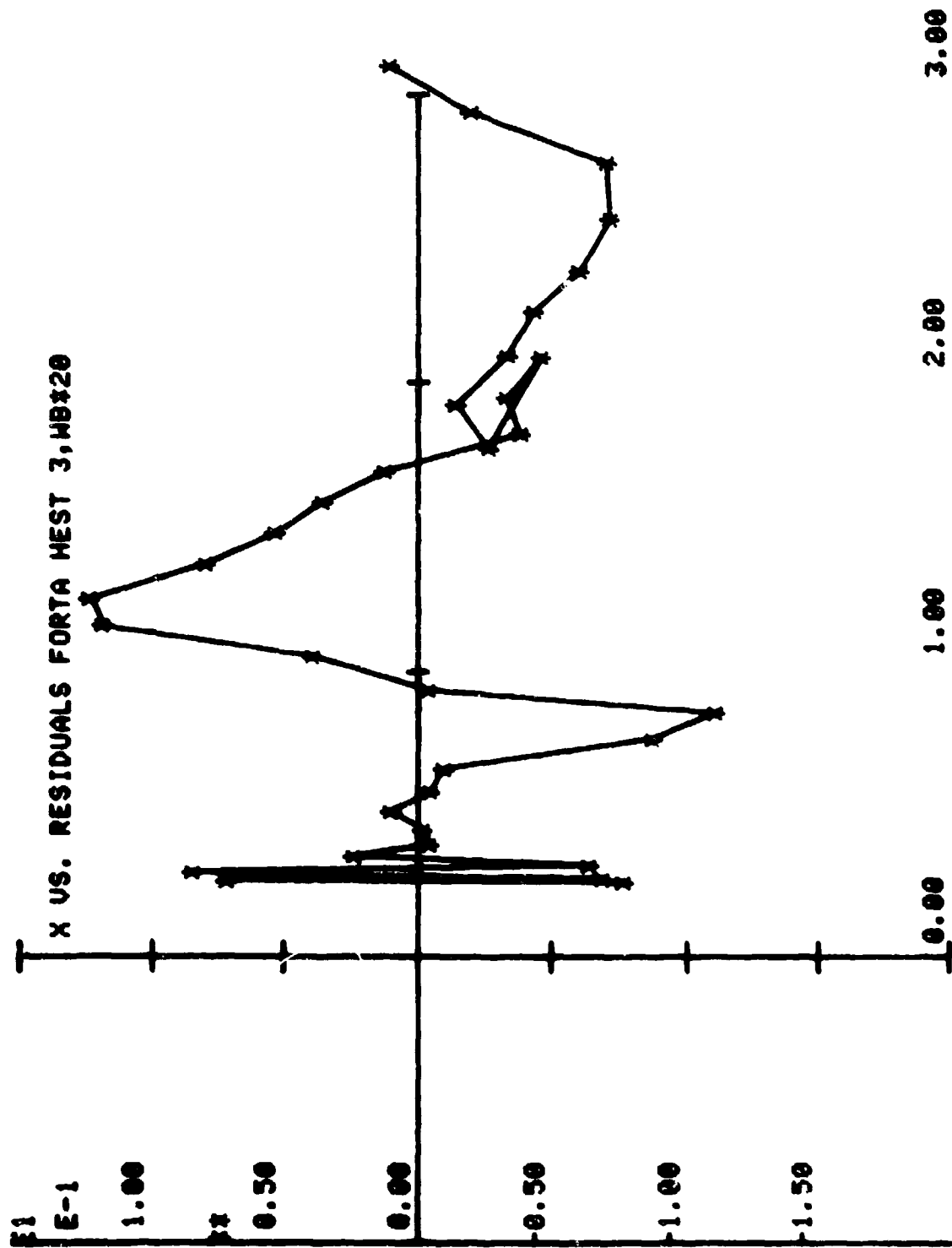
TR HEST-3 0-E 45.5 -1. 0.0 BP-Z E7/04/13/WB*20

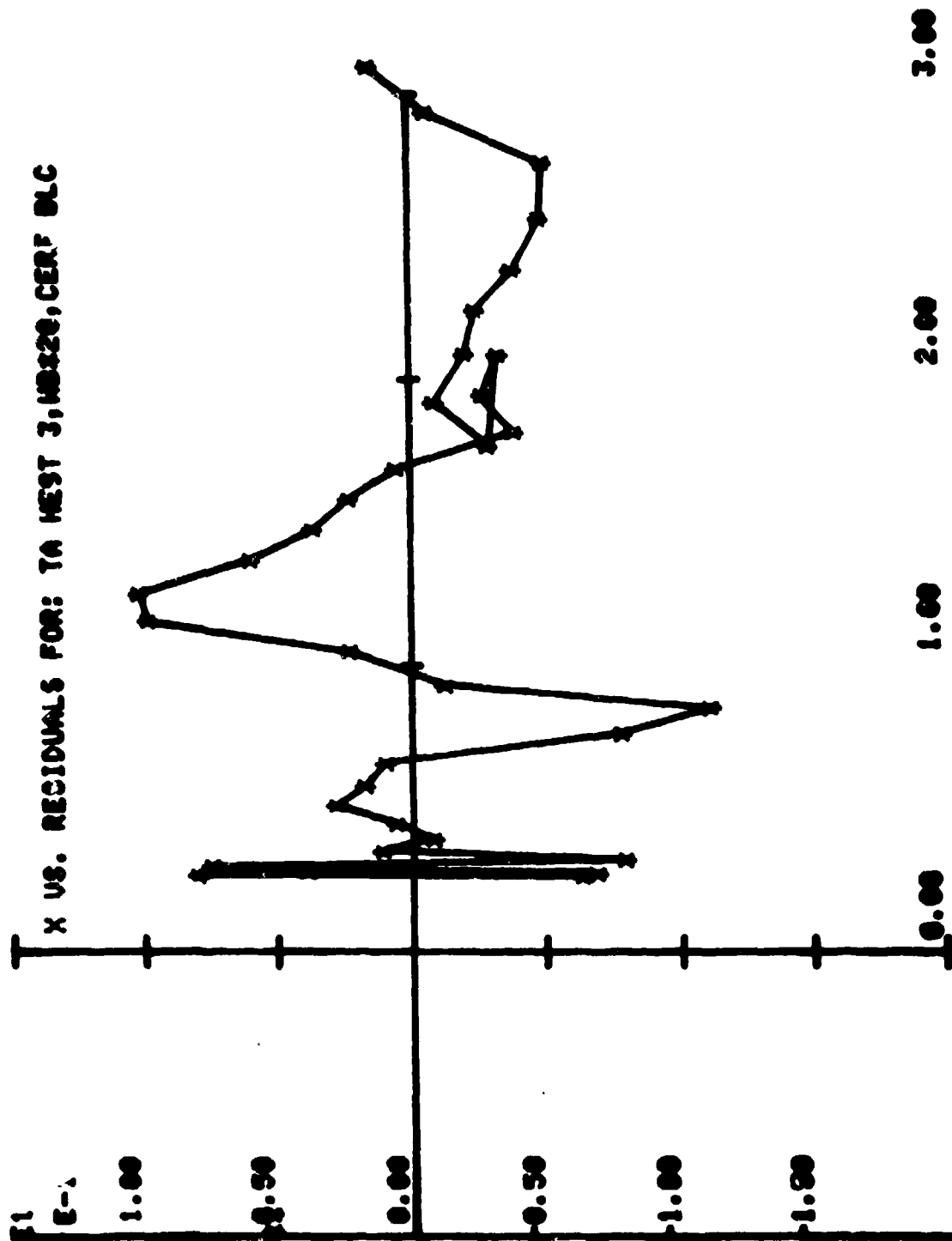


M.N. = 20
 TSKIP=12.650
 S.R. =100.00 KHZ

E.U. =0.000,4175.000
 DIGITS=0.000,614.500
 8 50 AM, 2 MAY 78.

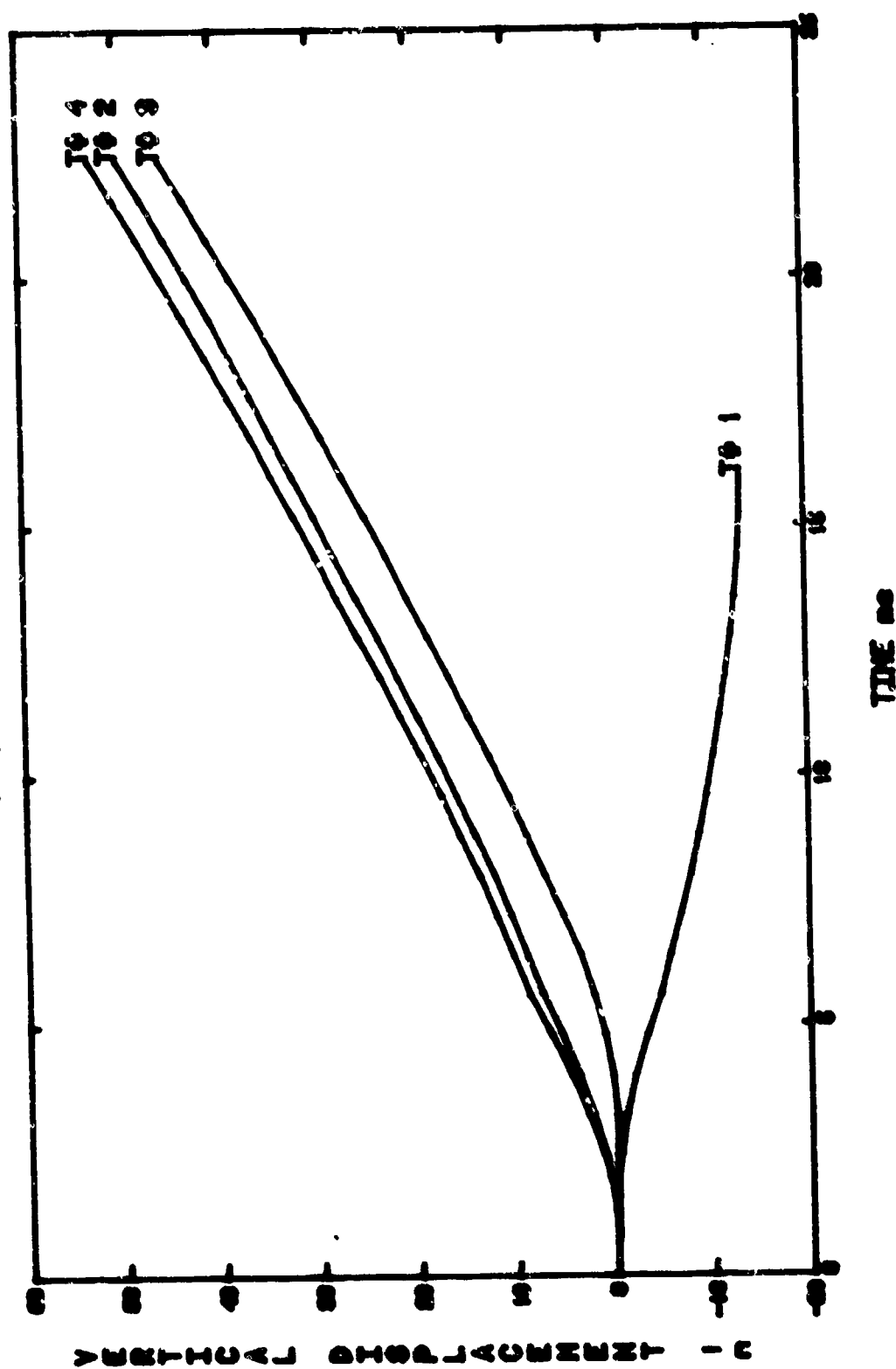
VSN=
 TAPE22
 FILE-50



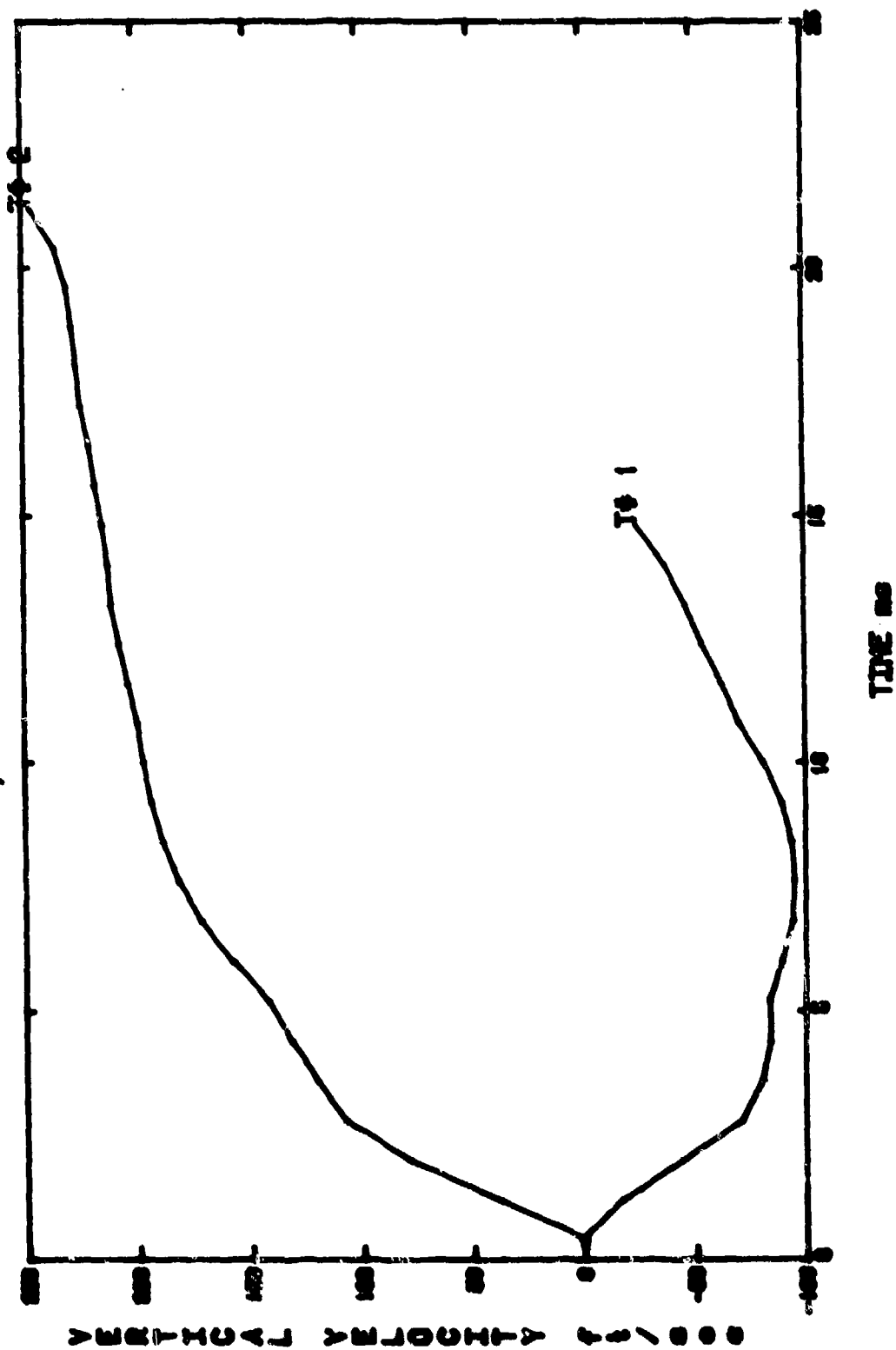


APPENDIX C
PLOTTED PHOTPOLE DATA

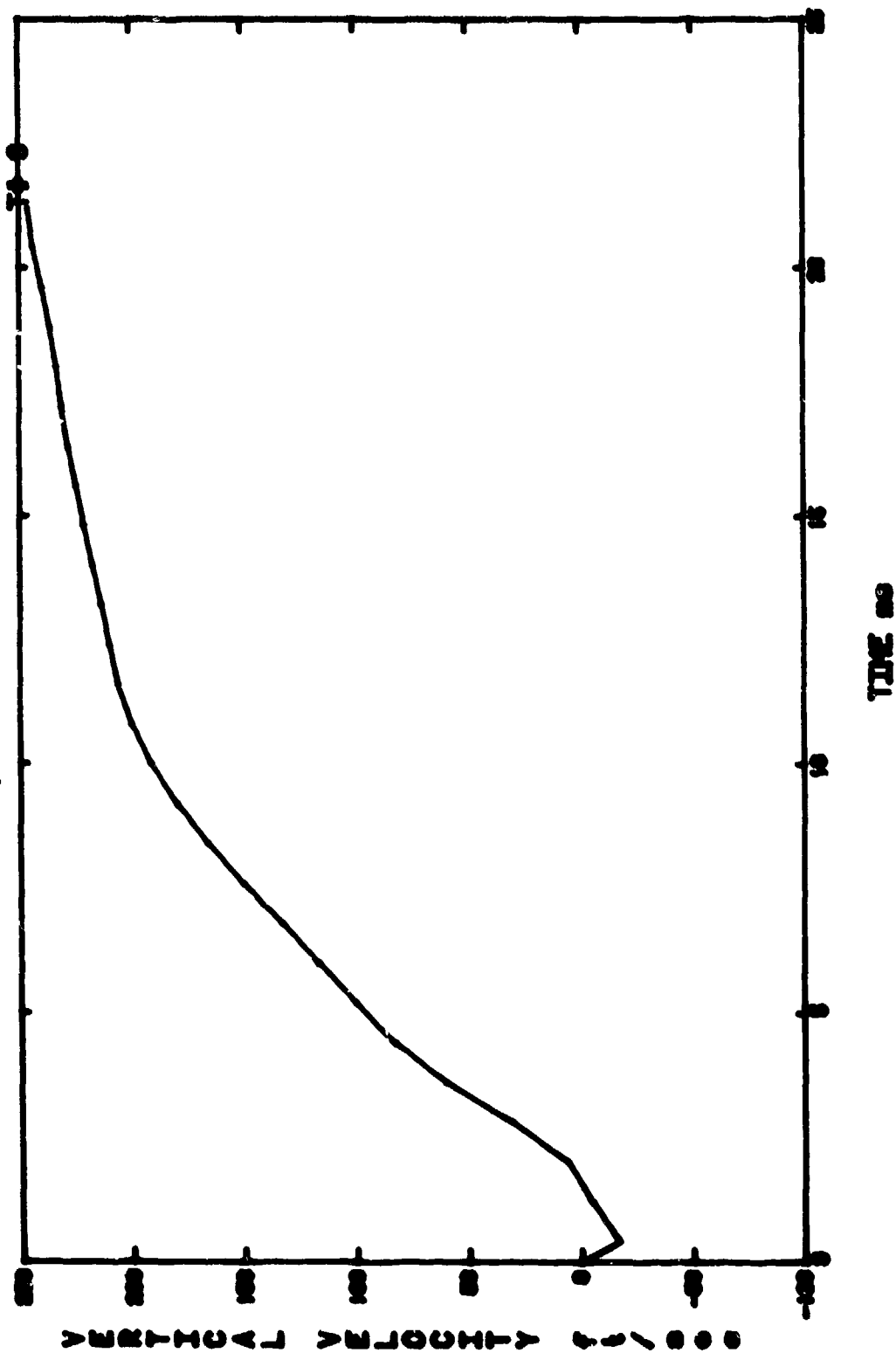
1000/1000 FILM READER
 TA TEST 1, 1200 fr/sec
 Y vs T SMOOTH



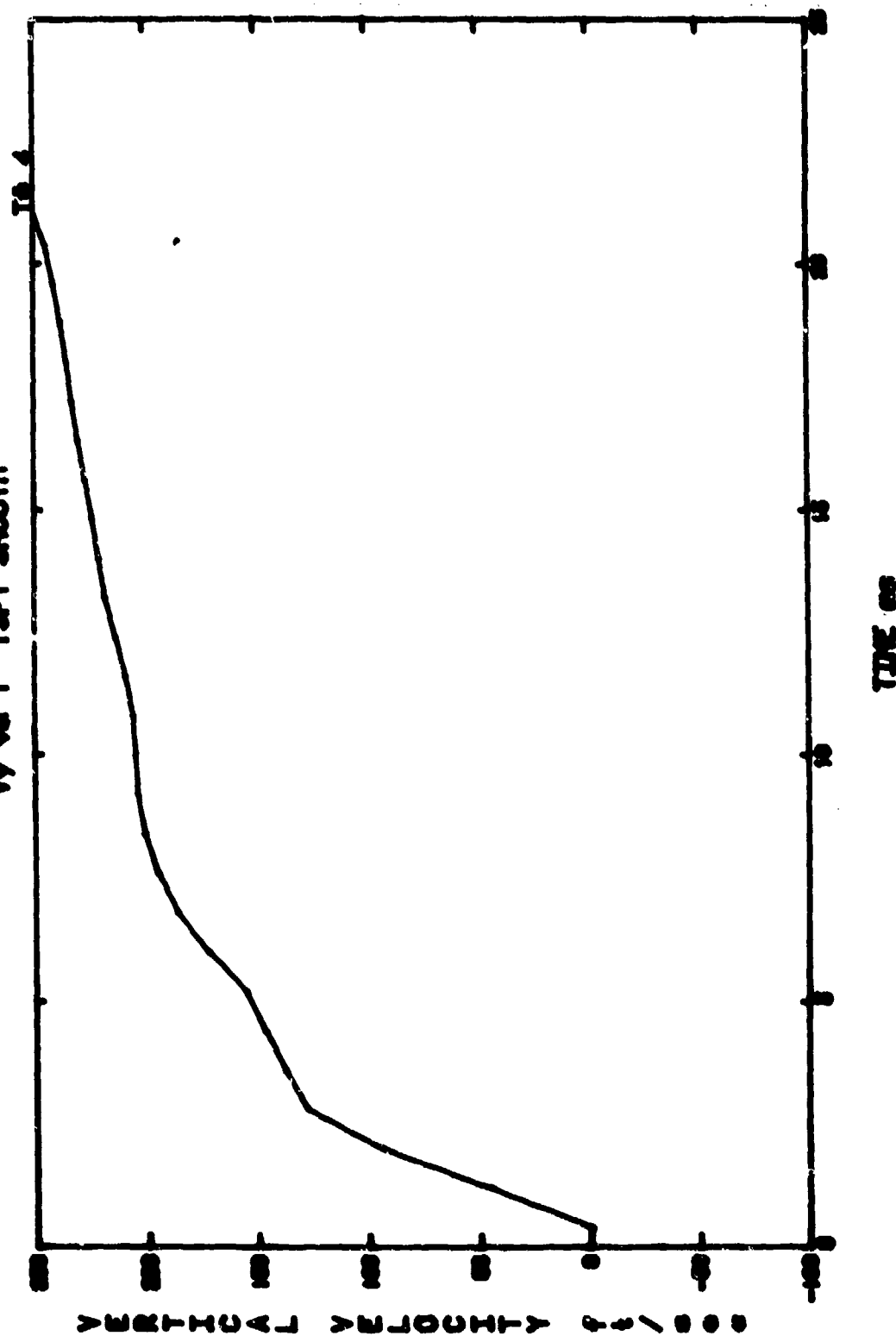
UNIV/CERF FILM READER
 TA TEST 1, 1250 fr/sec
 Vy vs T, 13PT SMOOTH



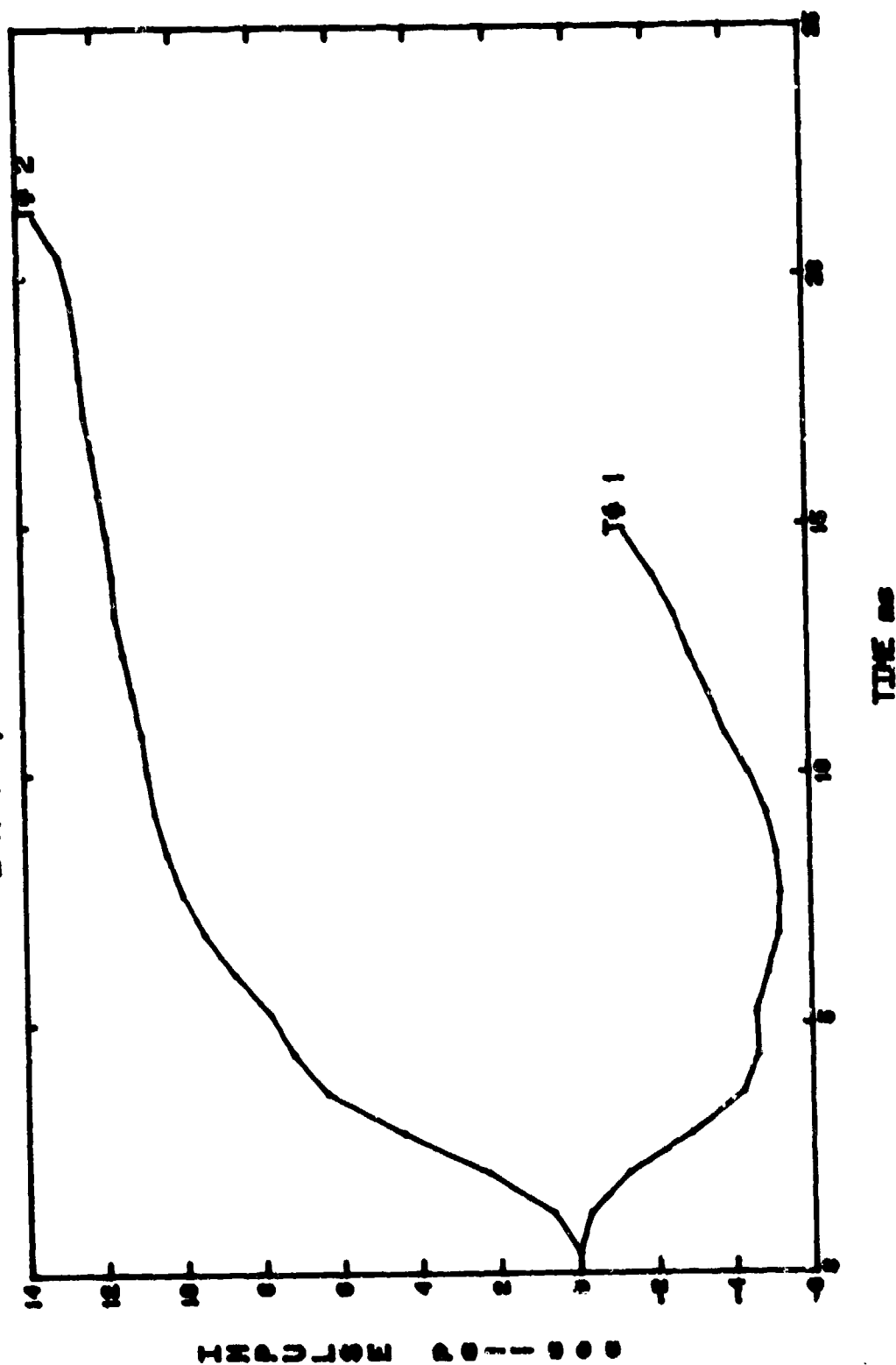
MONTAG/CERT FILM READER
 TA TEST 1, 1250 fr/sec
 Vy vs T, 12PT SMOOTH



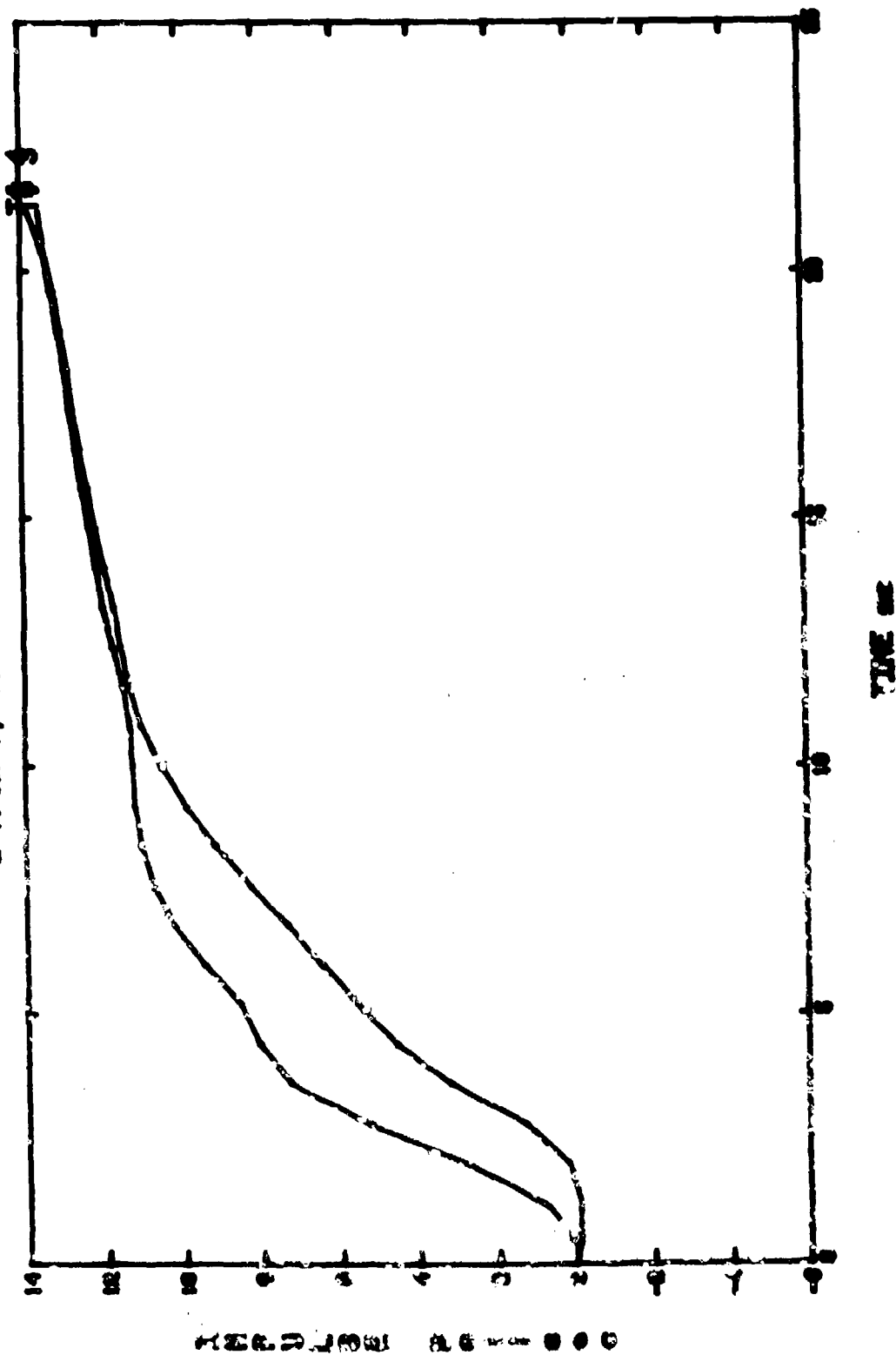
MONTANA/CENT FILM READER
 TA TEST 1, 1280 fr/sec
 Vy vs T 18PT SMOOTH



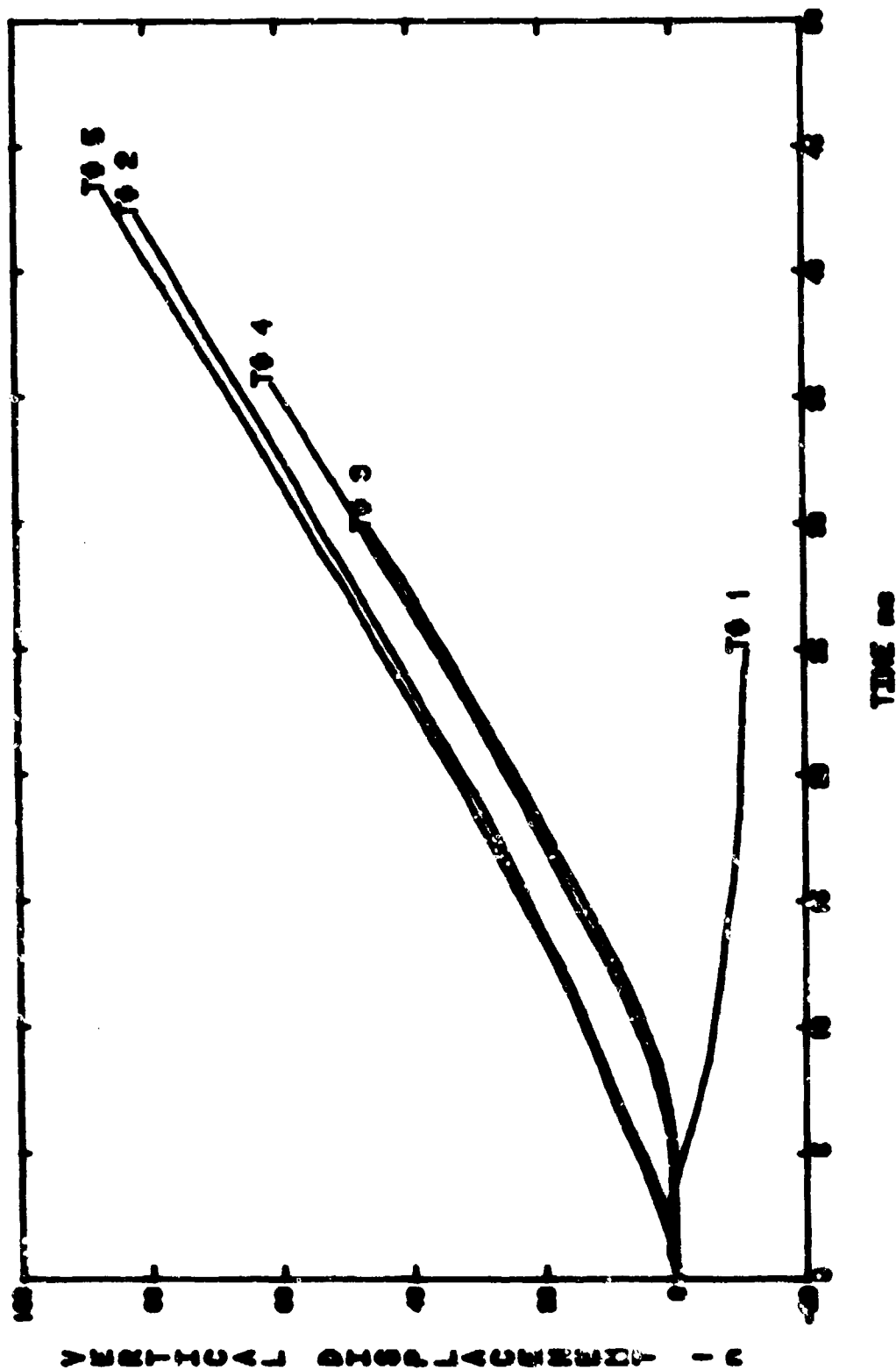
WINDUN/CENT FILM / ZADERMAN
 TA TEST 1, 1250 ft/sec
 I from Vy vs T 12PT SMOOTH



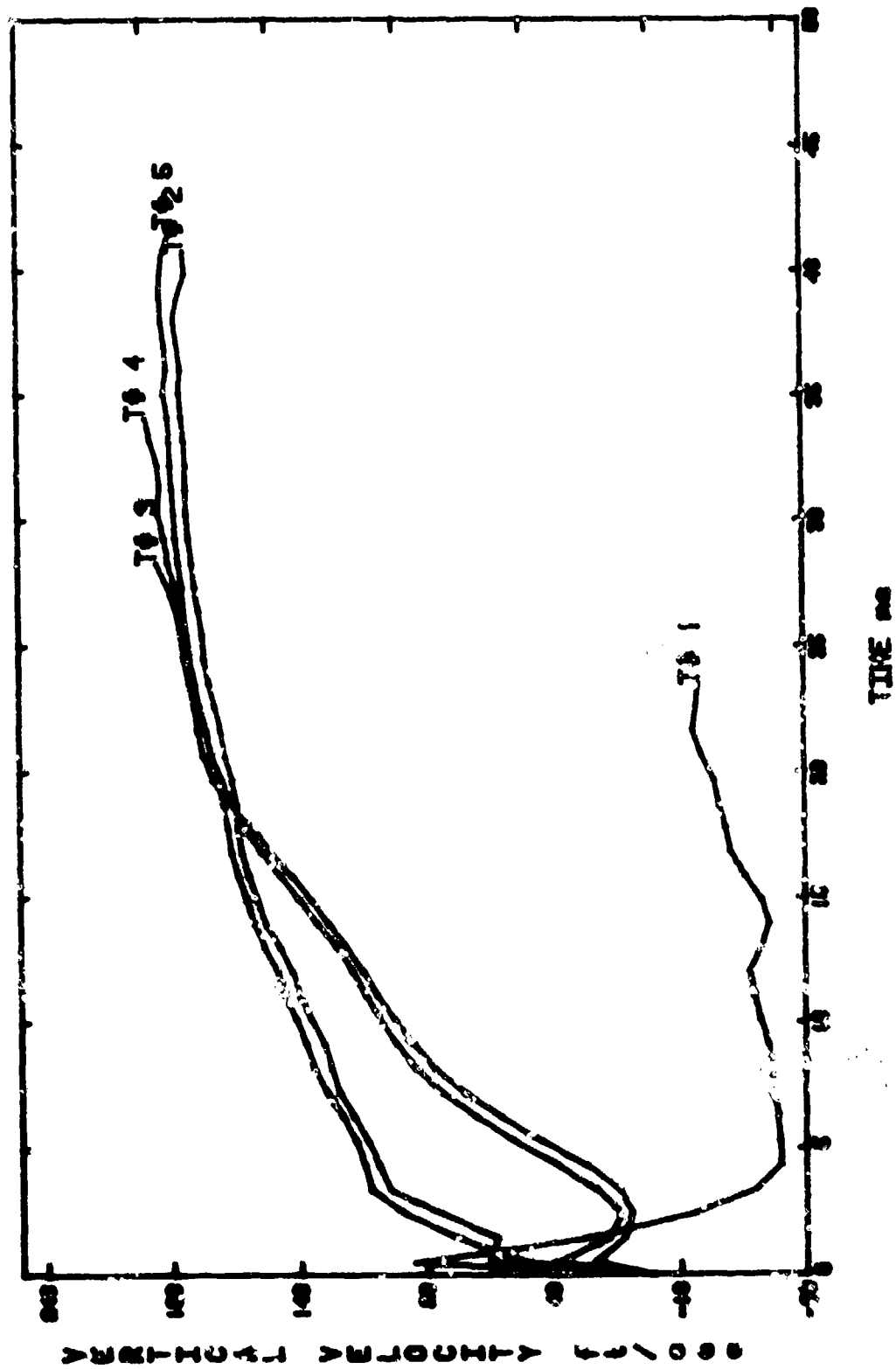
MUMUK/CENF FILM READER
 TA TEST 1, 1250 ft/sec
 I from Vy vs T 13PT SMOOTH



DODGSON/CENT FILM READER
 TA TEST 2
 Y vs T EPT SMOOTH



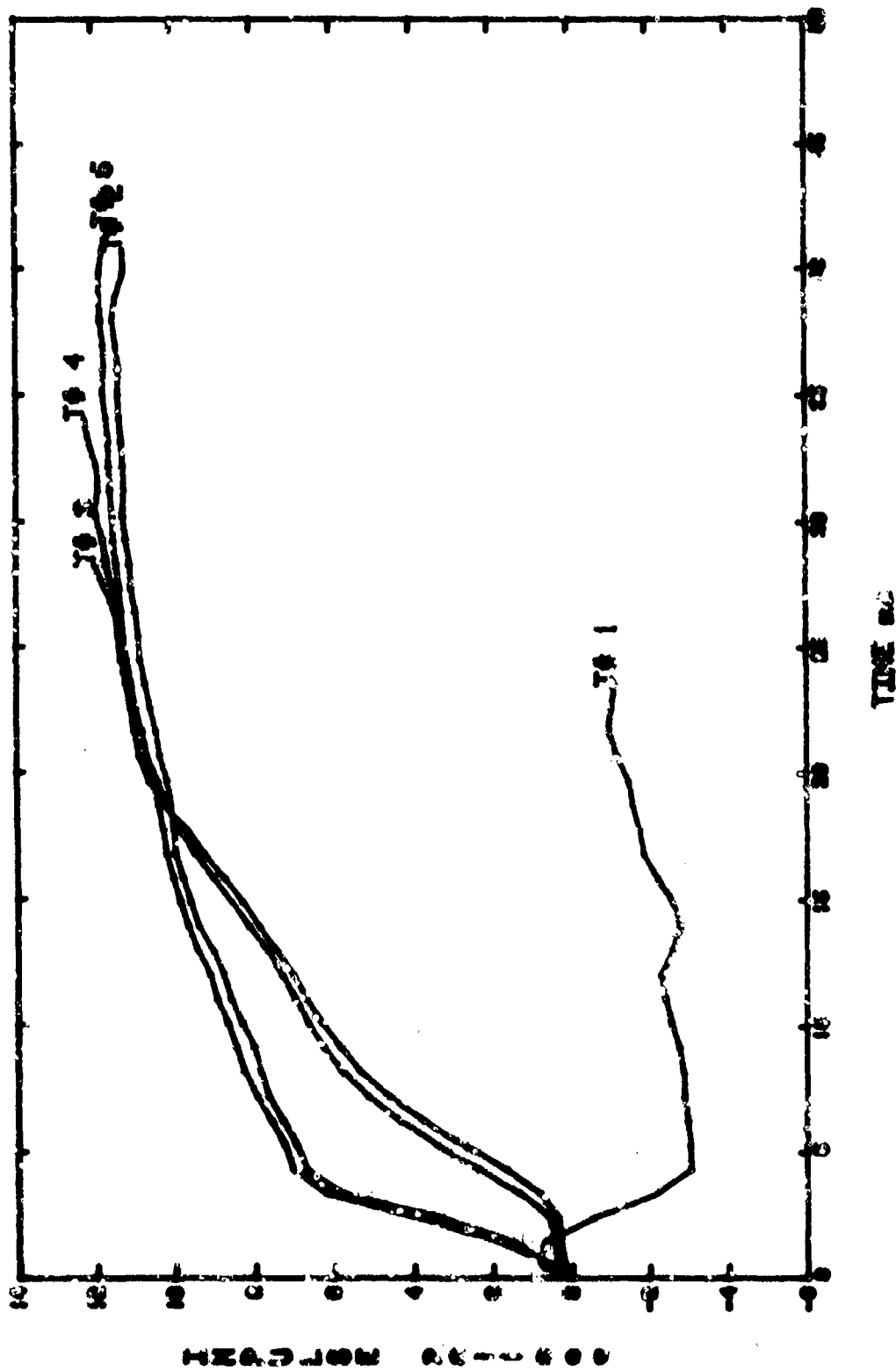
COMMUN/CENT FILM READER
 TA TEST 2
 Vy vs T 27PT SMOOTH



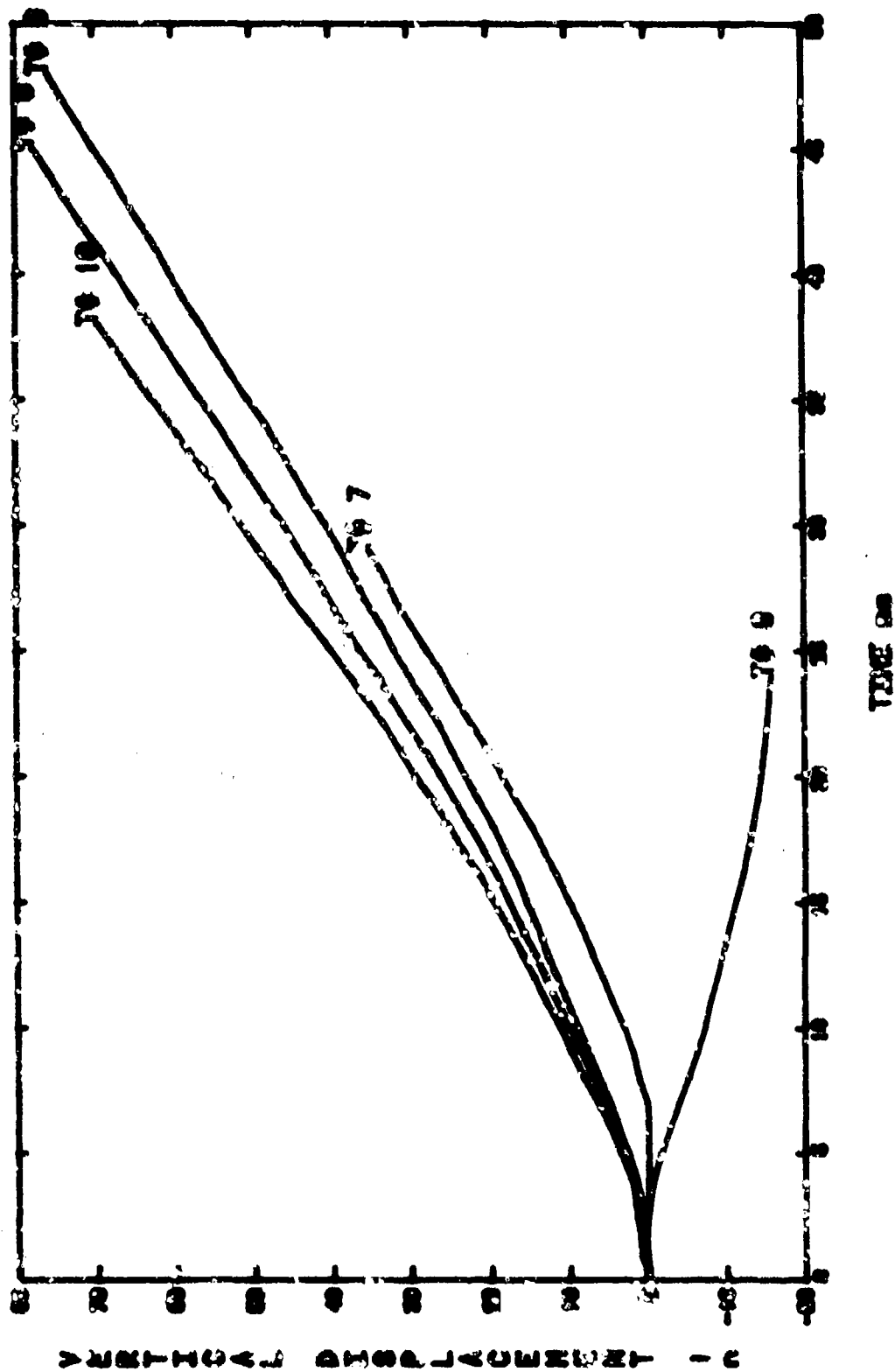
UNION/CENT FILM HEADERS

TA TEST 2

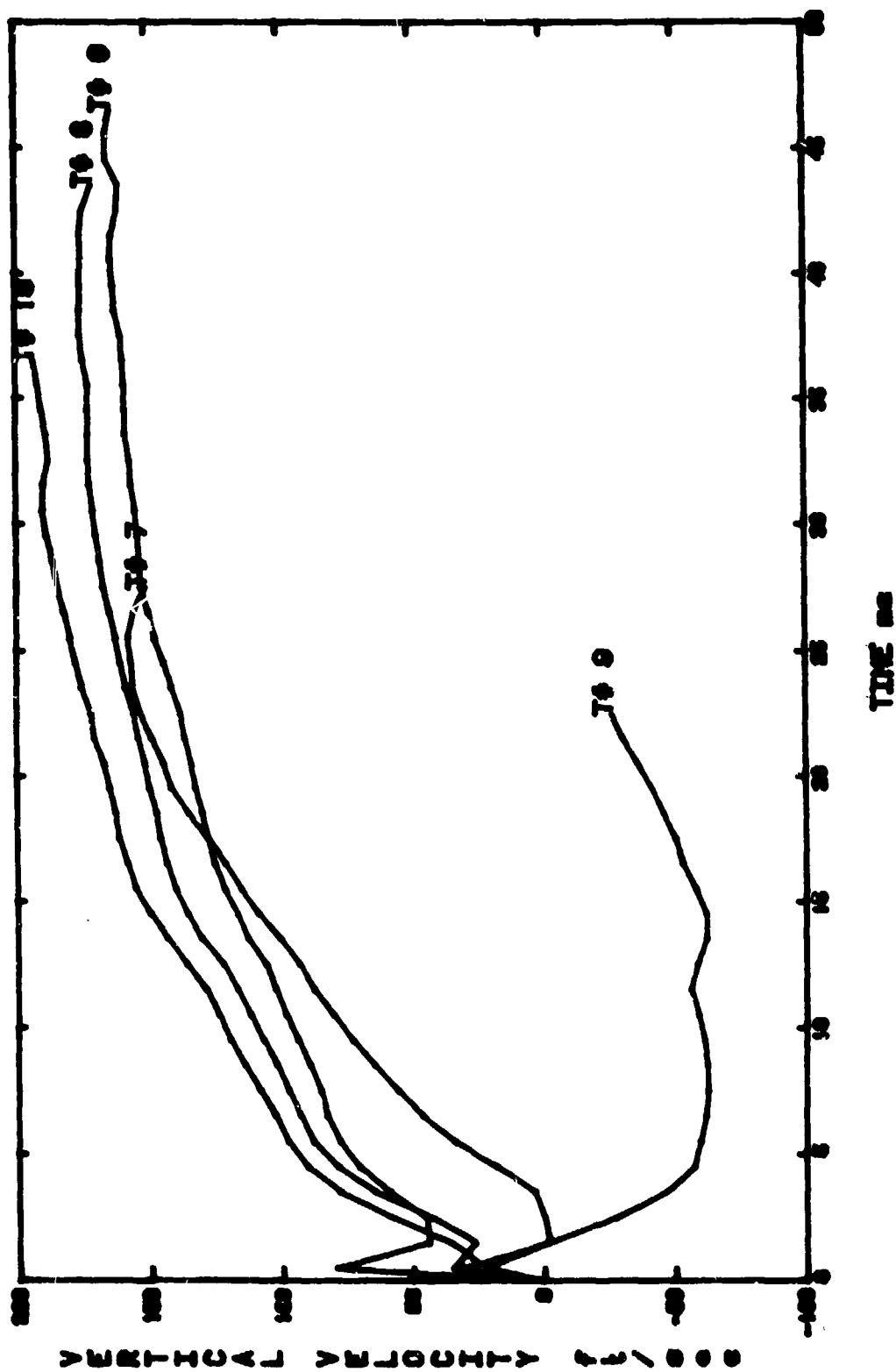
I from Vy vs T 27PT SMOOTH



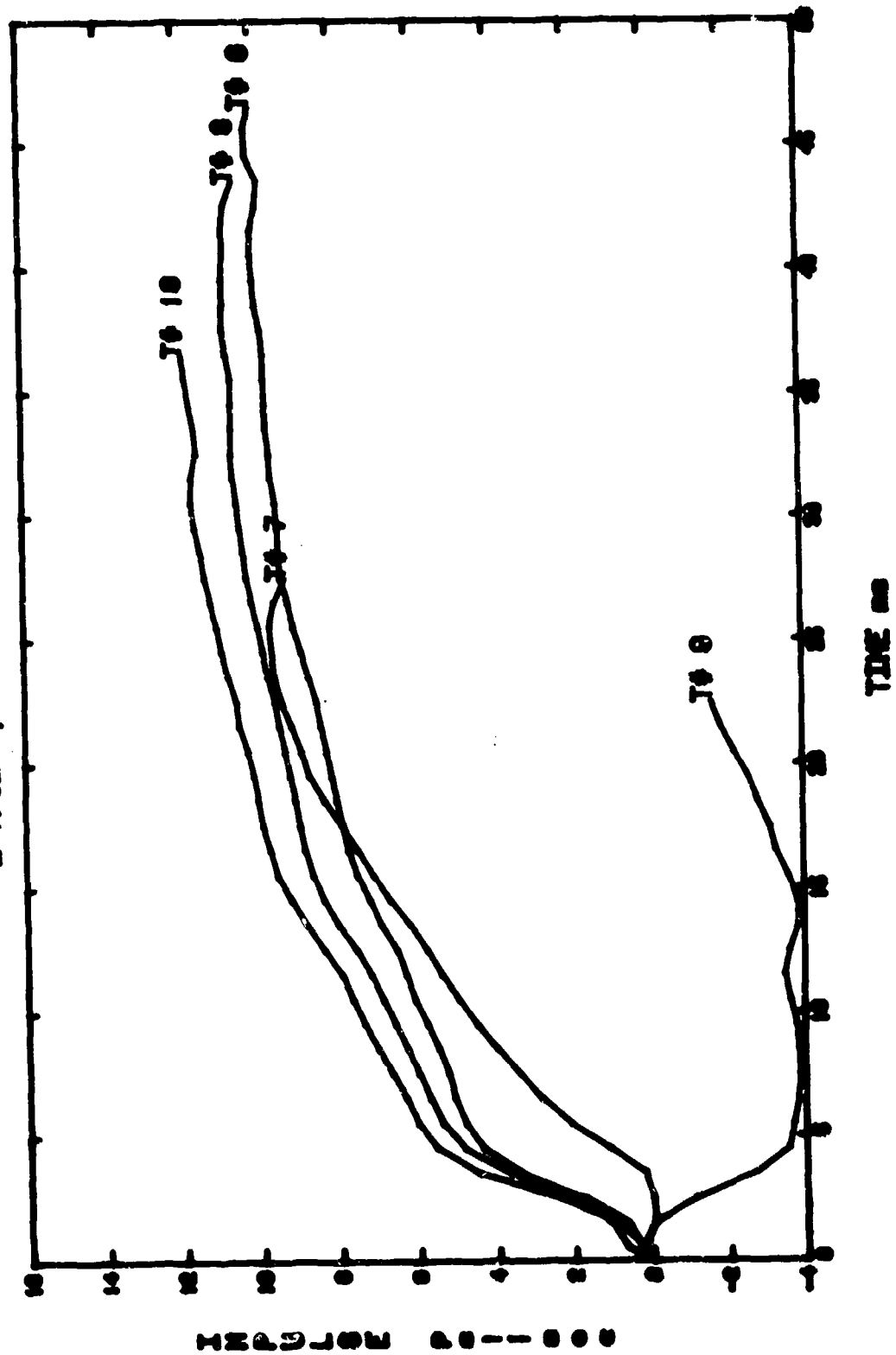
WIND-INDUCED FLIN RESPONSE
 1A HERTZ EAST END
 Y VS T EPT 2000TH



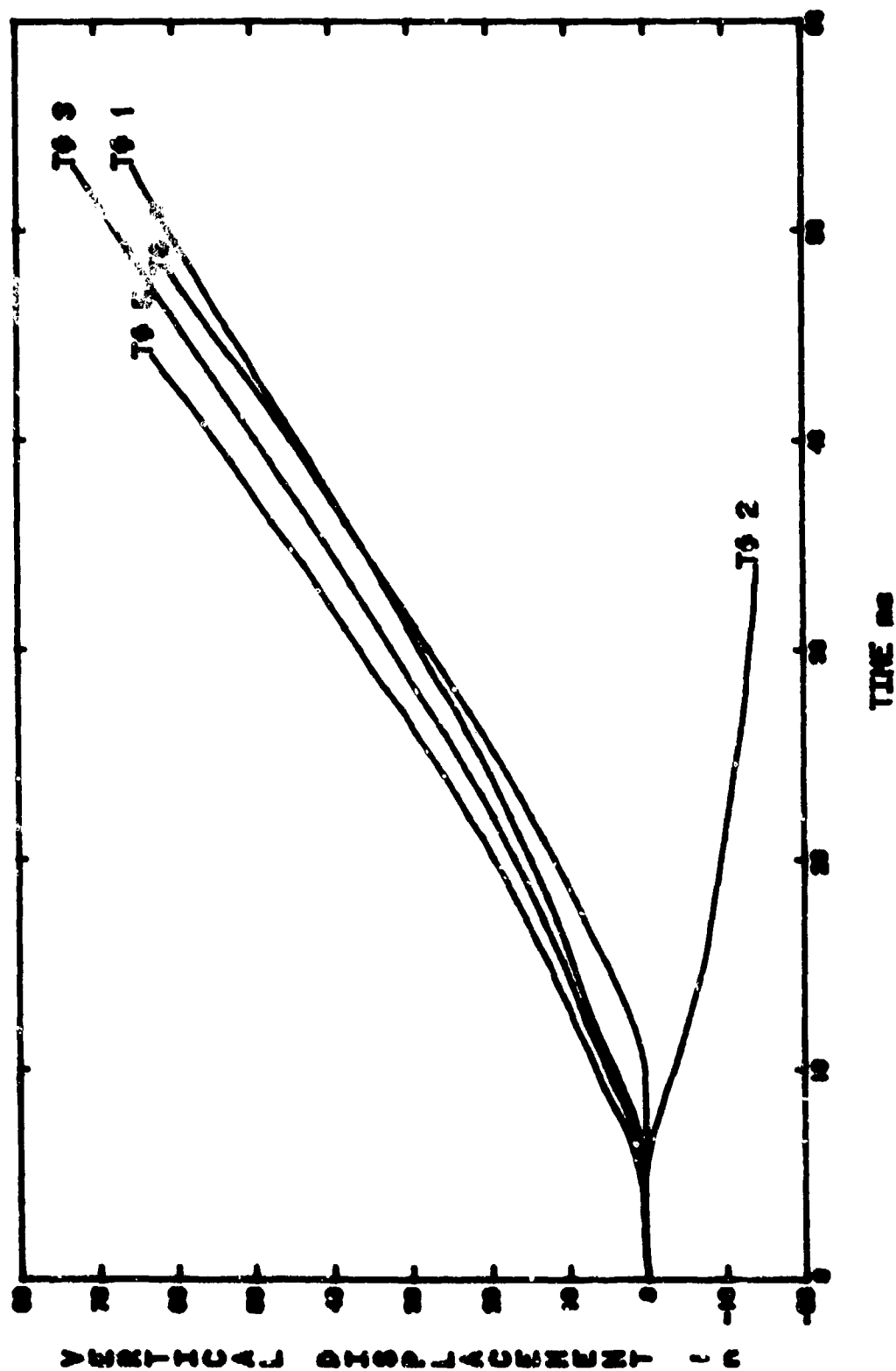
UNION/CENT FILM READER
 TA HEST 9, EAST END
 Vy vs T 28PT SMOOTH



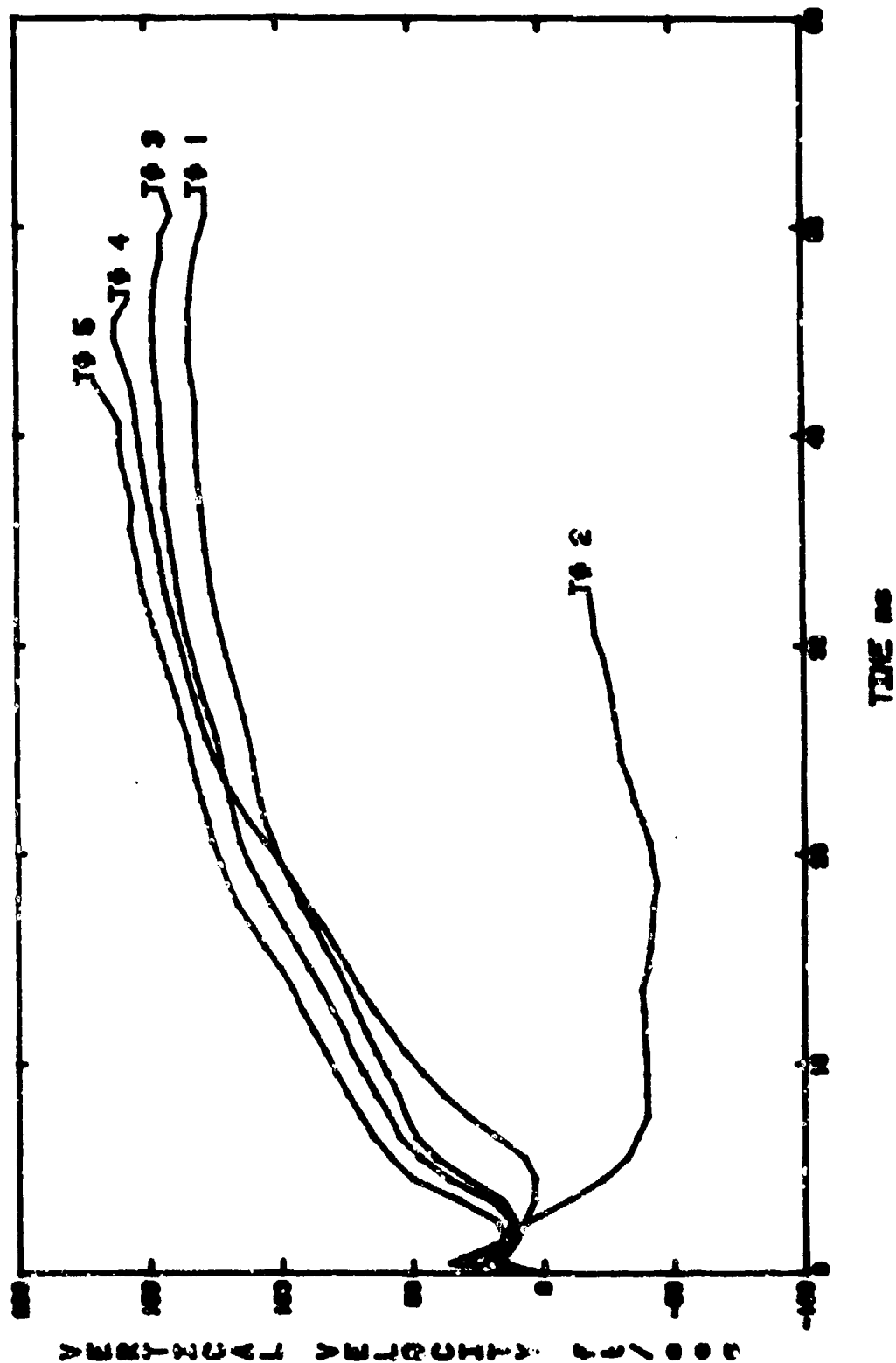
UNIV/CERF FILM READER
 TA HEST 3, EAST END
 I from Vy vs $\frac{1}{T}$ 25PT SMOOTH



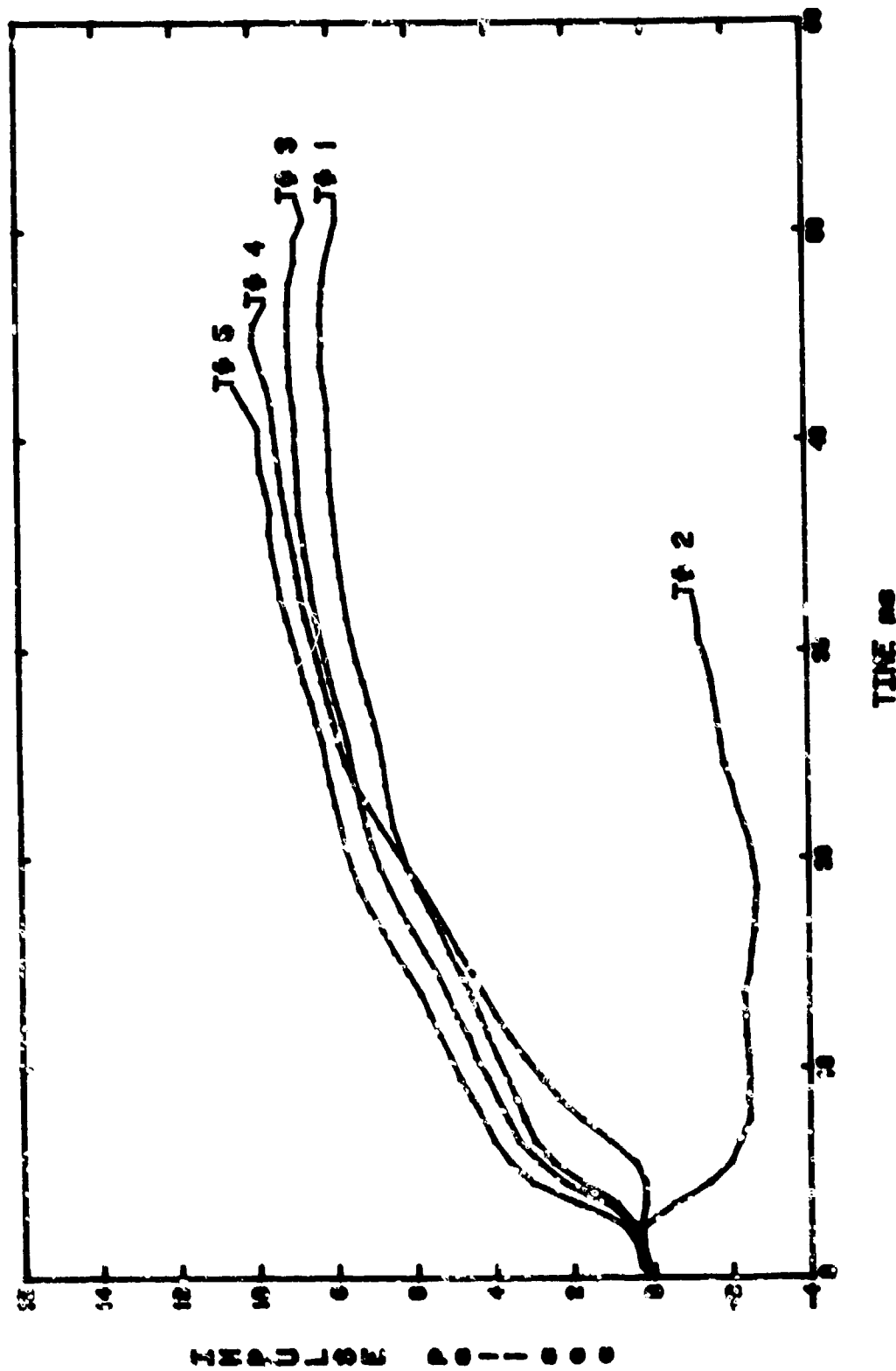
MILLIN/CENT FILM READER
 TA TEST 3, WEST END
 Y vs T SPT SMOOTH



WILSON/CENT FILM READER
 TA TEST 3, WEST END
 Vy vs T 27FT SMOOTH



000134/CENT FILM HEADERS
 TA TEST 3 WEST END
 I from Vy vs T 27PT SMOOTH



APPENDIX D

TEST INSTRUMENTATION DETAILS

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TIME-OF-ARRIVAL MEASUREMENTS	525
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TIME-OF-ARRIVAL MEASUREMENTS	527

Test: TA HEST 1 - Blast Pressure Measurements
Date: February 24, 1978

Measurement Number	Gage Number	Gage Type	Debris Shield	Locations							Posttest Elevation Change (ΔZ), in
				As Planned, in			As Built, in				
				X	Y	Z	X	Y	Z		
1	2-7	Kulite 30K	10	+2	+12	0	+2	+12-1/4	0	-12.06	
2	4-1	Kulite 20K	18	-36	+60	0	-36	+60-1/4	0	-11.04	
3	4-6	Kulite 20K	18	-36	-36	0	-35-3/4	-36-3/8	+3/16	-11.04	
4	5-22	Kulite 20K	18	-36	-36	0	+36-1/2	-36-3/8	+1/8	-11.46	
5	351	Bar 5K	None	+2	-6	0	+2-1/8	-6-1/8	+1/16	-11.88	
6	353	Bar 6K	None	+1-3/8	-18	0	+15/16	-18	+1/16	-11.64	
7	357	Bar 6K	None	+3/4	-30	0	+3/4	-30-1/4	+3/16	-11.04	
8	362	Bar 6k	None	0	-42	0	-1/4	-42-1/2	+3/16	-10.62	
Average = -11.35											

TA HEST 1 - Time-of-Arrival (TOA) Measurements

Measurement Number	Gage Type ^a	Locations, in			TOA ^b , ms
		X	Y	Z	
1		+72	+24	+3-3/4	
2		+36	0	+3-3/4	
3		0	+24	+3-3/4	
4		-36	0	+3-3/4	
5		-72	+24	+3-3/4	
6		+72	-72	+3-3/4	
7		+36	-48	+3-3/4	
8		0	-72	+3-3/4	
9		-36	-48	+3-3/4	
10		-72	-72	+3-3/4	
11		0	+12	+3-3/4	
12		0	0	+3-3/4	
13		0	-12	+3-3/4	
14		+72	+72	+5-3/8	
15		+36	+48	+5-3/8	
16		0	+72	+5-3/8	
17		-36	+48	+5-3/8	
18		-72	+72	+5-3/8	
19		+72	-24	+5-3/8	
20		+36	-48	+5-3/8	
21		0	-24	+5-3/8	
22		-36	-40	+5-3/8	
23		-72	-24	+5-3/8	

^aAll gages were crystal type.

^bData unavailable due to pin box failure.

Test: TA WEST 2 - Blast Pressure Measurements
Date: March 24, 1978

Measurement Number	Gage Number	Gage Type	Debris Shield	Locations						Posttest Elevation Change (ΔZ), in
				As Planned, in			As Built, in			
				X	Y	Z	X	Y	Z	
1	4-1	Kulite 20K	18	+57	0	0	+57	0	+1/8	-8.52
2	4-5	Kulite 20K	12	+36	+12	0	+35-1/2	+12	+3/16	-8.16
3	5-22	Kulite 20K	18	+21	-48	0	+21	-48	+3/16	-6.54
4	2-7	Kulite 30K	10	0	0	0	0	0	0	-7.38
5	5-23	Kulite 20K	18	-21	+48	0	-21-3/8	+48	0	-6.90
6	5-37	Kulite 20K	18	-36	-12	0	-36	-11-3/4	+1/16	-6.72
7	355	Bar 6K	None	+12	0	0	+12-5/16	0	+1/16	-7.38
Average = -7.37										

TA HEST 2 - Time-of-Arrival (TOA) Measurements

Measurement Number	Gage Type ^a	Location, in			TOA, ms
		X	Y	Z	
1		+72	+24	+3-3/4	0.523
2		+36	0	+3-3/4	0.687
3		0	+24	+3-3/4	0.842
4		-36	0	+3-3/4	1.006
5		-72	+24	+3-3/4	1.162
6		+72	-72	+3-3/4	0.522
7		+36	-48	+3-3/4	0.683
8		0	-72	+3-3/4	0.849
9		-36	-48	+3-3/4	1.010
10		-72	-72	+3-3/4	1.165
11		0	+12	+3-3/4	0.934
12		0	0	+3-3/4	1.153
13		0	-12	+3-3/4	Failed
14		+72	+72	+5-3/8	0.532
15		+36	+48	+5-3/8	0.692
16		0	+72	+5-3/8	0.946
17		-36	+48	+5-3/8	1.020
18		-72	+72	+5-3/8	Failed
19		+72	-24	+5-3/8	0.531
20		+36	-48	+5-3/8	0.683
21		0	-24	+5-3/8	0.857
22		-36	-48	+5-3/8	1.019
23		-72	-24	+5-3/8	1.160

^aAll gages were crystal type.

Test: TA HEST 3 - Blast Pressure Measurements
Date: April 27, 1978

Measurement Number	Gage Number	Gage Type ^a	Debris Shield	Locations							Posttest Elevation Change (ΔZ), in
				As Planned, ft			As Built, ft				
				X	Y	Z	X	Y	Z		
1	2-2	30K	10	+7.0	+1	0	6.968	+1	0.00	-18.12	
2	2-4	30K	10	+7.0	-1	0	6.974	-1	+0.03	-17.40	
3	2-5	30K	10	+14.0	+1	0	14.000	+1	0.00	-15.36	
4	2-9	30K	10	+14.0	-1	0	14.000	-1	+0.02	-15.24	
5	2-11	30K	10	+21.0	+1	0	21.000	+1	+0.02	-13.92	
6	2-12	30K	10	+21.0	-1	0	20.989	-1	+0.02	-12.72	
7	4-3	20K	18	+28.0	+1	0	28.000	+1	-0.04	-12.42	
8	4-4	20K	18	+28.0	-1	0	28.000	-1	-0.01	-11.88	
9	4-6	20K	18	+35.0	+1	0	34.989	+1	-0.07	-12.00	
10	4-7	20K	18	+35.0	-1	0	34.979	-1	-0.05	-10.92	
11	4-9	20K	18	+42.0	+1	0	42.000	+1	-0.09	-12.84	
12	4-11	20K	18	+42.0	-1	0	42.000	-1	-0.03	-11.52	
13	4-14	20K	18	+49.0	+1	0	49.000	+1	-0.07	-13.20	
14	4-27	20K	18	+49.0	-1	0	48.968	-1	-0.09	-12.36	
15	5-21	20K	18	+56.0	+1	0	56.020	+1	-0.10	-12.24	
16	5-22	20K	18	+56.0	-1	0	56.000	-1	-0.11	-12.00	
17	5-23	20K	18	+63.0	+1	0	63.040	+1	-0.09	-11.64	
18	5-26	20K	18	+63.0	-1	0	63.000	-1	-0.07	-11.52	
19	2-13	30K	10	+24.5	-1	0	24.500	-1	-0.01	-12.24	
20	2-37	20K	18	+45.5	-1	0	45.468	-1	-0.04	-11.88	
Average = -13.67											

* All gages were Kulite type.

TA NEST 3 - Time-of-Arrival (TOA) Measurements

Measurement Number	Gage Type ^a	Locations, ft			TOA, ms
		X	Y	Z	
1		0.0	+4.0	0.312	0.400
2		0.0	0.0	0.312	0.440
3		0.0	-4.0	0.312	0.405
4		9.0	0.0	0.312	0.825
5		18.0	+4.0	0.312	1.309
6		18.0	-4.0	0.312	1.266
7		27.9	+4.0	0.312	Failed
8		27.9	0.0	0.312	1.692
9		27.9	-4.0	0.312	1.712
10		35.9	+2.0	0.312	2.070
11		40.4	+4.0	0.312	2.309
12		40.4	0.0	0.312	2.291
13		40.4	-4.0	0.312	2.297
14		44.4	+2.0	0.312	2.408
15		47.9	0.0	0.312	2.661
16		50.9	+2.0	0.312	2.821
17		53.8	+4.0	0.312	2.975
18		53.8	0.0	0.312	2.973
19		53.8	-4.0	0.312	2.988
20		56.5	+2.0	0.312	3.124
21		59.2	0.0	0.312	3.273
22		61.7	+2.0	0.312	3.416
23		64.0	+4.0	0.312	3.552
24		64.0	0.0	0.312	3.569
25		64.0	-4.0	0.312	3.551
26		66.3	+2.0	0.312	3.683
27		68.5	0.0	0.312	3.819
28		0.0	+4.0	0.447	Failed
29		0.0	0.0	0.447	0.442
30		0.0	-4.0	0.447	0.489
31		9.0	+4.0	0.447	0.896
32		9.0	-4.0	0.447	0.895
33		18.0	0.0	0.447	1.258
34		27.9	+4.0	0.447	1.715
35		27.9	0.0	0.447	1.701
36		27.9	-4.0	0.447	1.731
37		40.4	0.0	0.447	2.290
38		47.9	+4.0	0.447	2.674
39		47.9	0.0	0.447	2.666
40		47.9	-4.0	0.447	2.687
41		53.8	0.0	0.447	2.981
42		59.2	+4.0	0.447	3.285
43		59.2	0.0	0.447	3.280
44		59.2	-4.0	0.447	3.296
45		64.0	0.0	0.447	3.559
46		68.5	+4.0	0.447	3.826
47		68.5	0.0	0.447	3.825
48		68.5	-4.0	0.447	3.825

^aAll gages were crystal type.

APPENDIX E

HEST LOCKUP CODE DESCRIPTION

The lockup impulse code is used to calculate HEST pressure and impulse histories for a given initial pressure, cavity, and overburden dimensions soil properties, as well as the ratio of specific heats (γ) of the detonation products. The code is small enough to run on the HP 9420A programmable calculator, and a BASIC version for the Tektronix 4051 is available. No provision is made for handling layered soils; the overburden and test bed materials are assumed uniform and homogeneous. The calculations are one-dimensional, and the three-dimensional properties of a HEST calculation are approximated. The detonation product/air mix in the cavity is assumed to have a uniform pressure distribution, and dynamic properties are neglected. The detonation product/air mix is assumed to be a "gamma law" gas with gamma held constant. The lockup code is typically used to design a HEST so that its pressure history matches a given nuclear waveform. This is done by varying cavity and overburden dimensions until the calculated HEST waveform most closely matches the desired nuclear waveform.

The code is also used in the analysis of data obtained from a HEST test. In this case, one inputs the appropriate soil model, as-built dimensions, etc., into the code and varies the initial pressure until the calculated HEST impulse-time trace most closely matches the given data trace. This initial pressure is called the Simulation Peak Pressure. This method of determining peak pressures is an alternative to using the peak pressure routine^a. In fitting a data trace with the lockup code the user determines the quality of the fit by inspection. Since these HESTs were designed with the lockup code, fitting data traces with the code yields information about the quality of the simulation. The lockup code should be used in the analysis of HEST test data whenever the results of that analysis are to be used as inputs in future HEST designs.

^aHampler, Howard M., and Earickson, Jeff A., *High-Pressure and Foam HEST Analysis*, CERF AST-10, Civil Engineering Research Facility, University of New Mexico, Albuquerque, New Mexico, publication pending.